FINAL DATA REPORT FIELD AND LABORATORY DATA COLLECTION PHASE OYSTER BAYOU MARSH RESTORATION PROJECT (CS-59)

CAMERON PARISH, LOUISIANA



OFFICES

Orlando, 8008 S. Orange Avenue, Orlando, Florida 32809, Phone (407) 855-3860
Bartow, 1525 Centennial Drive, Bartow, Florida 33830, Phone (863) 533-0858
Baton Rouge, 316 Highlandia Drive, Baton Rouge, Lousiana 70884, Phone (225) 752-4790
Cocoa, 1300 N. Cocoa Blvd., Cocoa, Florida 32922, Phone (321) 632-2503
Fort Myers, 9970 Bavaria Road, Fort Myers, Florida 33913, Phone (239) 768-6600
Miami, 2608 W. 84th Street, Hialeah, Florida 33016, Phone (305) 825-2683
New Orleans, 1305 Distributors Row, Suite 1, Jefferson, Louisiana 70123, Phone (504)835-2593
Port Charlotte, 740 Tamiami Trail, Unit 3, Port Charlotte, Florida 33954, Phone (941) 624-3393
Port St. Lucie, 460 Concourse Place NW, Unit 1, Port St. Lucie, Florida 34986, Phone (772) 878-0072
Sarasota, 2500 Bee Ridge Road, Sarasota, Florida 34239, Phone (941) 922-3526
Tallahassee, 3175 West Tharpe Street, Tallahassee, Florida 32303, Phone (850) 576-6131
Tampa, 3925 Coconut Palm Drive, Suite 115, Tampa, Florida 33619, Phone (813) 620-3389
West Palm Beach, 2200 North Florida Mango Road, Suite 101, West Palm Beach, Florida 33409, Phone (561) 687-8200

MEMBERS:
A.S.F.E.
American Concrete Institute
American Society for Testing and Materials
Florida Institute of Consulting Engineers



August 9, 2013 AAI File: 12-80-3741

Coastal Protection and Restoration Authority P.O. Box 44027 Baton Rouge, LA 70804

Attention: Ms. Kodi Collins, P.E.

Kodi.collins@la.gov

Final Data Report - Field and Laboratory Data Collection Phase Re:

Oyster Bayou Marsh Restoration Project (CS-59)

Cameron Parish, Louisiana

We have completed the field exploration and laboratory data collection phase of the Oyster Bayou Marsh Restoration Project (CS-59) project. A summary of the field exploration and laboratory testing results, along with our evaluation of the data and preliminary recommendations for selection of geotechnical design properties are provided in the attached Final Data Report. This work was authorized by acceptance of our work plan, AAI File No. 113-12-80-3741PR, dated August 7, 2012.

We will be pleased to discuss any questions you may have concerning this data report.

Sincerely,

ARDAMAN & ASSOCIATES, INC.

ROBERT E. ROUSSET, E.I.

ASSISTANT PROJECT ENGINEER

RER/RJW/gtp

(6) bound originals

License No. 36633 **PROFESSIONAL**

BRANCH MANAGER/PRINCIPAL ENGINEER

TABLE OF CONTENTS

TABLE OF CONTENTS	ł
SECTION 1. GENERAL PROJECT INFORMATION	L
1.1 Project Description	L
SECTION 2. FIELD EXPLORATION	
2.1 Permission and Access)
SECTION 3. LABORATORY TESTING	
3.1 Laboratory Testing Overview	
3.4.2 Torvane Index Strength Tests	
3.4.3 Consolidated-Undrained Shear Strength Tests	
APPENDIX A. BORING LOGS AND PROFILESA-1	
APPENDIX B. LABORATORY DATA PLOTSB-1	
APPENDIX C. CONSOLIDATION TEST RESULTS	
APPENDIX D. UNCONSOLIDATED UNDRAINED TRIAXIAL COMPRESSION TEST RESULTSD-1	
APPENDIX E. CONSOLIDATED-UNDRAINED SHEAR STRENGTH TEST RESULTS E-1	
APPENDIX F. SETTLING AND SLURRY CONSOLIDATION TEST RESULTS F-1	



FINAL DATA REPORT FIELD AND LABORATORY DATA COLLECTION PHASE OYSTER BAYOU MARSH RESTORATION PROJECT (CS-59)

CAMERON PARISH, LOUISIANA

Results and findings of the field exploration and laboratory testing phases of the Oyster Bayou Marsh Restoration project are provided herein. Boring locations, boring logs and generalized subsurface profiles, along with a description of terms and symbols used on the boring logs are provided in Appendix A. Laboratory testing data plots are included in Appendix B and laboratory testing results are presented in Appendices C through F.

SECTION 1. GENERAL PROJECT INFORMATION

1.1 Project Description

The Oyster Bayou Marsh Restoration project will consist of the creation of approximately 510 acres of saline marsh and nourishing 90 acres of existing saline marsh with hydraulically dredged material from the Gulf of Mexico. The project will also consist of construction of approximately 14,140 linear feet of earthen terraces throughout the proposed project area. Altered hydrology, drought stress, saltwater intrusion, and hurricane induced wetland losses have caused the area to undergo interior marsh breakup. USGS data between 1984 and 2011 predicts a land loss rate of -0.75 percent/year in the project area. The scope of work associated with the field and laboratory data collection phase of this project consisted of performing a total of 19 soil borings (B-01 through B-19) to depths ranging from 40 to 60 feet below the existing mudline at locations established by the Coastal Protection and Restoration Authority (CPRA).

Geotechnical field and index laboratory testing data for the proposed dredge material borrow site have already been obtained for CPRA by GeoEngineers under a different contract. These samples were delivered to our laboratory by GeoEngnieers on May 22, 2013. Results of index tests were reviewed and used to select representative samples for inclusion in preparation of three composite samples for settling column testing and slurry consolidation testing. The results of the settling and slurry consolidation tests are discussed in Sections 3.3.5 and 3.3.6, respectively, and are included in Appendix F.

1.2 Site Location and Description

The project site is located in Cameron Parish, Louisiana, east of Mud Lake, north of Highway 27, and approximately 4 miles west of Monkey Island. The site is a wetland area with the majority of its surroundings consisting of marsh. The water depth at the boring locations during the field exploration phase ranged from 0.25 to 1.42 feet, with an average water depth of approximately 0.9 feet. The site is bordered to the south by the Gulf of Mexico. Open water and marsh areas



border the site to the north, east, and west. An unnamed gravel road running north from Highway 27 was used for mobilizing and launching our airboat-mounted drilling equipment.

1.3 Geology

Geologically, the site is underlain by the Saline Marsh Deposits of the Holocene Age. These deposits consist of gray to brown to black clay and silt with moderate to high organic content. Further south the Saline Marsh is mixed with Cheniers consisting of white to light gray fine sand and shell fragments.

SECTION 2. FIELD EXPLORATION

2.1 Permission and Access

Prior to mobilizing to the site to establish the boring locations or conduct any portion of our fieldwork, landowners, as listed in the Scope of Services for Geotechnical Investigation and Engineering Services, Oyster Bayou Marsh Restoration, CS-59 document, were notified in the form of a letter from Ardaman and Associates, Inc. (AAI) to inform the parties involved of our geotechnical investigation operations. Through communication with the landowners and Ms. Kodi Collins with CPRA, permission was granted to access the site and conduct our geotechnical investigation at all of the boring locations.

2.2 Soil Borings

A total of nineteen borings were performed at locations designated by CPRA, as shown on Figure A-1, Boring Location Plan, in Appendix A. Boring locations B-01, B-02, and B-03 were performed within the proposed Terracing Area. Boring locations B-05 through B-16 were performed within the proposed Marsh Creation Area with the exception of B-09. Boring locations B-04, B-09, B-17, B-18, and B-19 were performed at designated locations outside the proposed boundaries of the Terracing and Marsh Creation Areas. The nineteen soil borings were performed between October 1 and October 10, 2012. As-drilled boring locations were determined in terms of Global Positioning System (GPS) UTM coordinates recorded at each boring location using a hand-held GPS device. Table 2.1 below presents the GPS coordinates at each boring location.

Water level readings were recorded every day during the field exploration phase from the nearest water elevation gauge location (29° 46′ 46.89″ N, 93° 34′ 20.77″ W) that was established by the surveyors prior to our geotechnical investigation. In addition, the water depth at each boring location was measured at the time of drilling. Elevations at the boring locations were calculated based on these water readings. Gauge water level, water depth readings, and calculated mudline elevations for each boring location are summarized in Table 2.1 below. This information is also included on the soil boring logs in Appendix A.

Boring locations B-01 through B-17 were performed using an airboat-mounted, rotary-type drilling rig. Borings locations B-18 and B-19 were performed on land using an ATV-mounted, rotary-type drilling rig. Borings were advanced using 4-inch diameter rotary wash methods to



12-80-3741

depths ranging from 40 to 60 feet below the existing mudline or ground surface. Discrete samples were obtained continuously within the upper 20 feet at all of the boring locations. Continuous sampling was performed to provide detailed information for near surface stratigraphy. Samples were obtained at five-foot intervals at depths greater than 20 feet. The boreholes were grouted upon completion in accordance with State regulations.

Table 2.1 Soil Boring Details

			GPS Co	ordinates	Water	Data	
Boring ID	Depth (ft)	Mudline Elevation* (ft, NGVD)	Latitude	Longitude	Water Elevation at Gauge Location (ft, NGVD)	Water Depth at Borehole (ft)	Project Area
B-01	40	-0.49	29°47′09.00″N	93°25′00.40″W	0.68	1.17	Terracing Area
B-02	45	-0.32	29°47′16.00″N	93°24′37.10″W	0.68	1.00	Terracing Area
B-03	40	-0.60	29°47′22.00″N	93°24′16.40″W	0.65	1.25	Terracing Area
B-04	40	-0.68	29°47′11.40″N	93°24′02.00″W	0.65	1.33	Other
B-05	40	-0.51	29°46′59.60″N	93°23′56.20″W	0.66	1.17	MCA
B-06	60	-0.77	29°46′52.20″N	93°24′06.30″W	0.65	1.42	MCA
B-07	42	0.57	29°46′56.40″N	93°24′43.40″W	0.90	0.33	MCA
B-08	40	-0.08	29°46′41.70″N	93°24′55.00″W	0.50	0.58	MCA
B-09	40	+0.03	29°46′35.10″N	93°25′03.70″W	0.70	0.67	Other
B-10	60	+0.17	29°46′39.90″N	93°24′27.90″W	0.50	0.33	MCA
B-11	40	+0.45	29°46′22.60″N	93°24′35.60″W	0.70	0.25	MCA
B-12	60	-0.17	29°46′29.70″N	93°24′04.30″W	0.66	0.83	MCA
B-13	40	-0.05	29°46′09.30″N	93°23′56.50″W	0.70	0.75	MCA
B-14	40	+0.20	29°46′23.30″N	93°23′37.70″W	0.70	0.50	MCA
B-15	60	-0.38	29°46′27.40″N	93°23′40.80″W	0.70	1.08	MCA
B-16	40	-0.13	29°46′41.70″N	93°23′31.40″W	0.70	0.83	MCA
B-17	60	-0.68	29°47′12.50″N	93°23′41.60″W	0.65	1.33	Other
B-18**	60	NA	29°46′05.50″N	93°24′24.10″W	NA	NA	Other
B-19**	40	NA	29°46′04.20″N	93°24′24.10″W	NA	NA	Other

^{*}Mudline elevations calculated based on gauge water levels and water depths at the boring locations.

** Land Borings.

MCA=Marsh Creation Area



In the cohesive and semi-cohesive soils, relatively undisturbed samples were secured using a 3-inch diameter, 30-inch long, thin-walled Shelby tube. In this sampling procedure, the borehole is advanced to the desired level, and the Shelby tube is lowered to the bottom of the boring. It is then pushed 24 inches into the soil in one continuous stroke.

Upon retrieval, the sample at the end of the tube was visually classified and then the sample was sealed in the tube with plastic caps and expandable disk-type seals. Each sample tube was labeled and placed vertically in a fabricated tube rack to minimize any disturbance to the sample during transport. All samples were transported to our Baton Rouge laboratory for extrusion and testing.

A total of 291 thin-walled tube samples and 4 bag samples were obtained during the field exploration program. Sample recovery lengths were measured in the field and upon extrusion in the laboratory. In general, sample recovery generally ranged from approximately 19 to 24 inches of recovery out of the total 24-inch sample stroke, with an average recovery of about 21.5 inches (i.e., average 90% recovery).

SECTION 3. LABORATORY TESTING

3.1 Laboratory Testing Overview

Periodically during and upon completion of our field exploration work, soil samples were transported to our Baton Rouge laboratory. The tube samples were stored in secure racks in an upright position and protected from vibration and the elements. The samples were removed from the sampling tubes in the laboratory using a specially fabricated hydraulic piston-type extruder.

In light of the very soft character of the samples, particularly those obtained from depths less than about 20 feet, sample extrusion was coordinated with specimen selection and testing to minimize sample disturbance by avoiding even short-term warping once outside the sampling tube. Selected samples that were not immediately tested were preserved with wax and placed in a humidity controlled storage room. In order to preserve representative portions for later consolidation and strength testing, the bottom 6-inch section of several tube samples (which typically exhibit the least sampling disturbance effects) were cut using a fine-toothed band saw and sealed in the sampling tube section. Then the remainder of the tube sample was extruded, classified and subjected to index and compressive strength testing. Hand-operated Torvane shear strength tests were also performed on the ends of the samples primarily to assess strength variability within the sample group. This procedure enabled evaluation of the corresponding classification and index strength data to guide selection of the most representative or potentially more critical samples for the more sophisticated consolidation and strength testing.

In order to avoid disturbance that might otherwise occur due to bonding of the sample to the inside of the galvanized steel sampling tube during the testing program period, a special



technique was used for extrusion of samples from the 6-inch cut sections. Specifically, a thin wire was carefully inserted along the edge of the sample and inside face of the tube and was then held taught to enable wire-cutting around the circumference of the sample prior to careful manual extrusion. This technique was developed and is standard practice in the geotechnical laboratory at the Massachusetts Institute of Technology (Germaine and Germaine, 2009).

An overview of the scope of the laboratory testing phase in terms of the type and number of tests performed to date is presented in Table 3.1 below. Results of the laboratory tests and their implication with respect to design material property selection are presented and discussed in the following sections of this report.

Table 3.1 Laboratory Testing Summary

Test Method	ASTM Reference	Number of Tests Performed
Unconsolidated Undrained (UU) Triaxial Compression Test	ASTM-D2850	160
Consolidation Test	ASTM-D2435	24
Atterberg Limit Determination	ASTM-D4318	164
Organic Content	ASTM-D2974	29
Moisture Content	ASTM-D2216	493
Grain Size Analysis	ASTM-(C136,D1140,D422)	68
Unit Weight Determination	ASTM-D2937	423
Specific Gravity Determination	ASTM-D854	24
Consolidated Undrained – Direct Simple Shear Strength Tests	ASTM D4767	2
Slurry Consolidation Tests	ASTM D2435 (mod.)	1
Settling Column Tests	USACE 1110-2-5027	3

3.2 Classification and Index Testing

Soil conditions encountered at all of the boring locations, with the exception of land Borings B-18 and B-19, generally consisted of very soft to soft clay (CH, per the Unified Soil Classification) and silty clay (CL) with organics, sand, and shells to depths ranging from about 16 to 20 feet below the mudline. Medium to very stiff clay (CH) or silty clay (CL) soils were encountered below depths of 16 to 20 feet, with occasional inter-bedded thin sandy clay (CL), silt (ML), and clayey sand (SC) layers. Soil conditions encountered at the two land boring locations, Nos. B-18 and B-19, were notably different. In particular, loose to medium dense sand (SP-SC) with clay and clayey sand (SC) was encountered to depth of 30 and 10 feet below the existing ground surface at boring locations B-18 and B-19, respectively. Below these depths, conditions were similar to those encountered at the other boring locations.

3.2.1 Visual Classification

Visual classification included description of soil color, consistency and type, and identification of structural conditions (layering, seams, etc.) and variations (organics, oxide inclusions, etc.).



Visual classifications for the soil samples obtained from the site are incorporated into the soil boring logs in Appendix A.

3.2.2 Moisture Content and Density

More than four hundred moisture content determinations (ASTM D2216) and 423 total unit weight determinations (ASTM D2937) were performed in conjunction with the sample extrusion process and preparation of test specimens. Total unit weights of the tube samples were computed based on sample volume and weight measurements taken after exclusion of any materials that appeared to have been disturbed during the sampling or extrusion process (occasionally encountered at the top of the tube sample). Two or more moisture content determinations were made for each extruded sample, and dry densities were computed for each sample. Considering that all samples were obtained from below water (excluding samples from borings B-18 and B-19), degrees of saturation were computed to confirm that the density and moisture content values correspond to near 100 percent saturation as a quality control measure. Moisture content and dry density values for each sample are included on the soil boring logs in Appendix A.

Variations in moisture content, total unit weight (wet density) and dry density versus depth below the mudline at all of the soil boring locations are illustrated on Figures B-1, B-2 and B-3, respectively (Appendix B). As expected, *in situ* moisture contents generally decreased with depth. With the exception of a few highly organic samples encountered near the mudline, moisture contents within the upper 16 feet below the mudline typically ranged from about 60 to 100 percent, with an average value of about 80 percent. Within the depth range from 16 to 20 feet, moisture contents generally ranged from about 20 to 80 percent. Moisture contents of samples obtained from depths below 20 feet typically ranged from about 20 to 45 percent.

As can be seen in Figure B-2, total unit weight (or wet density) values generally increased with depth, as expected. Total unit weights of samples obtained from the upper 16 feet below the mudline typically ranged from about 80 to 110 pounds per cubic foot (pcf), with an average value of about 96 pcf. Samples obtained from depths greater than 16 feet were generally higher, ranging from about 95 to 130 pcf.

Dry densities of the tube samples and strength test specimens were computed based on measured total unit weights and moisture contents. The variation in dry density with depth for the marsh area samples is shown on Figure B-3. Samples obtained from the upper 16 feet below the mudline generally displayed dry densities ranging from about 40 to 65 pcf. Dry density values within the depth interval from 16 to 20 feet were higher but more variable, ranging from about 50 to 110 pcf. Samples obtained from depths greater than 20 feet tended to be more consistent and displayed a slight decreasing trend with depth. Dry density values within the depth interval from 20 to 34 feet generally ranged from about 80 to 110 pcf. Below the 34-foot depth, dry densities were slightly lower and generally ranged from about 70 to 90 pcf.



3.2.3 Specific Gravity

Specific gravity determinations were performed on samples corresponding to those selected for one-dimensional laboratory consolidation testing. The specific gravity of samples tested ranged from 2.62 to 2.78, with an average value of 2.72.

3.2.4 Organic Content

A total of 29 organic content determinations (ASTM D 2974) were performed on selected samples. The results of organic content tests are presented on the soil boring logs in Appendix A, and are plotted versus depth below the mudline on Figure B-4 (Appendix B). Organic contents generally ranged from about 2 to 10 percent, with the higher values corresponding to samples obtained within about 4 feet of the mudline.

3.2.5 Atterberg Limits

A total of 164 Atterberg limit determinations (ASTM D4318) were performed on selected samples to assist in soil classification and to enable correlation to pertinent clay behavior properties. The Atterberg limit data consist of measured liquid limit (LL) and plastic limit (PL) values from which the plasticity index (PI = LL - PL) is derived. The individual test data are included on the boring logs in Appendix A. The test results are also presented in terms of a plasticity chart on Figure B-5 and variation with depth on Figures B-6 and B-7 (Appendix B). As expected, the data indicate that the marsh deposits down to depths of about 16 feet below the mudline predominantly consist of highly plastic materials classifying as CH-type soils in accordance with the Unified Soil Classification System. Samples obtained between depths of about 16 and 38 feet predominantly consist of less plastic clays classifying as CL-type soils. At depths greater than about 38 feet, liquid limit values increased to above 50%, indicative of CH-type soils.

The Liquidity Index (LI) is a parameter that characterizes the *in situ* moisture content of a sample in relation to its liquid and plastic limit values (LI= [MC-PL]/PI). Clay soils having high liquidity indices, i.e., approaching or even greater than 1.0, have *in situ* water contents that are near to or above their liquid limit, which is characteristic of very soft and compressible "normally consolidated" conditions. As can be seen on Figure B-8, these type conditions are prevalent in the marsh deposits from the mudline down to a depth of about 14 to 16 feet, where liquidity index values range from about 0.7 to 1.4. Samples obtained at depths greater than about 16 feet generally displayed liquidity index values less than 0.5, which suggests slightly overconsolidated conditions and hence higher shear strength and lower compressibility.

3.2.6 Particle Size Distribution

A total of 27 particle size analysis tests with hydrometer (ASTM D422) and particle size analysis tests (%" through #200 Sieve) and 41 fines content determinations (ASTM D 1140) were performed on selected samples. The test results, in terms of percent fines (i.e., percent by dry weight finer than the U.S. No. 200 sieve size, 0.074 mm, or silt and clay fraction) are included on



the soil boring logs in Appendix A. Percentages of gravel, sand, silt, and clay size particles based on results of the particle size analyses tests are summarized in Figure B-9 in Appendix B.

3.3 Consolidation Tests

A total of 24 incremental consolidation tests (ASTM D 2435) were included in the laboratory testing program to enable assessment of stress history and determination of one-dimensional stress-deformation and time-rate of consolidation characteristics of the marsh clay deposits that will dictate post-construction settlement of the terrace berms.

Considering the very soft and compressible character of the marsh clay samples in light of the index data discussed above, the laboratory consolidation tests were generally performed using a reduced load increment ratio, LIR, on the order of 0.5 (versus the customary increment ratio of 1.0 where loads are doubled in each increment). The use of a lower LIR improves resolution of the compression curve and provides more data within the low effective stress range around the *in situ* and final design stresses beneath the proposed terrace berms. The use of the lower LIR does, however, extend the test duration since the number of load increments normally required to complete a test increases by a factor of two. Each test typically included one unload-reload sequence.

During each load increment, the accumulation of vertical displacement with time is measured. In general, each load increment was sustained for a period of 24 hours. At times, the increment duration was increased to assess long-term drained creep behavior. The vertical displacement versus time data was evaluated using the conventional log-time and square-root time curve fitting techniques to determine the end of primary consolidation (i.e., the point in time at which dissipation of load-induced excess pore water pressures in the sample had dissipated and drained creep ensued for each load increment). The individual test results, in terms of vertical strain versus effective vertical stress, are presented in Appendix C. (Individual load increment time curves will be included in the final report.)

Typical laboratory consolidation test results, considered in terms of vertical strain, ε_v (%; at the end of primary consolidation), versus vertical effective stress, σ'_{vc} (tons/ft²; log scale), may be simply characterized as being composed of recompression and virgin compression. The flatter recompression portion of the ε_v versus log σ'_{vc} curve occurs at vertical effective stresses lower than the preconsolidation pressure, σ'_p to which the specimen had historically been subjected. The steeper virgin compression portion of the ε_v versus log σ'_{vc} response occurs at vertical effective stresses greater than the maximum past pressure, σ'_p . In the case of the marsh deposits, particularly within about 14 feet of the mudline, the preconsolidation is "apparent", and results largely from post-deposition drained creep.

3.3.1 Compression Characteristics

The compression ratio, CR, is defined as the slope of the virgin compression portion of the $\epsilon_{\rm v}$ versus log $\sigma'_{\rm vc}$ curve and can be used to predict the magnitude of consolidation settlements for normally consolidated foundation clays. Compression ratios for the very soft marsh deposit



samples tested from depths less than about 14 to 16 feet below the mudline, generally range from 0.2 to 0.4, with an average value of 0.31. Samples obtained from depths greater than about 16 feet generally displayed lower CR values, averaging about 0.24. The compression index, C_c , characterizes the slope of the void ratio, e, versus $\log \sigma'_{vc}$ curve, and is equal to $(1+e_o)$ x CR where e_o is the initial specimen void ratio. Site-specific correlations between the virgin compression parameters CR and C_c and various index properties are shown in Figure B-10.

The slope of the recompression portion of the laboratory consolidation curve is used to estimate primary consolidation settlement magnitudes for stress increments resulting in final stress levels less than the preconsolidation pressure. Because the initial recompression behavior in the laboratory test can be influenced by sample disturbance (sampling stress relaxation, etc.), an unload-reload sequence is typically included to enable better assessment of in situ recompression behavior. The recompression ratio, RR, is defined as the slope of the recompression portion of the $\varepsilon_{\rm v}$ versus log $\sigma'_{\rm vc}$ curve. Recompression ratios for samples, obtained from depths less than about 14 to 16 feet below the mudline within very soft marsh deposits, generally range from 0.025 to 0.045, with an average value of 0.034.

The coefficient of compressibility, m_{ν} , is a parameter that characterizes the compression modulus in one-dimensional primary consolidation. The relationship between m_{ν} and vertical effective stress ratio for samples tested to-date is shown on Figure B-11.

The continued accumulation of vertical strain with time subsequent to the end of primary consolidation is referred to as secondary consolidation (or drained creep). This component of clay compression behavior is important to estimating long-term settlements (and to the overall coastal subsidence situation). The coefficient of secondary compression, $C_{\alpha\epsilon}$, quantifies the creep rate in terms of strain per log cycle of time after the end of primary consolidation. This parameter is derived from the individual load increment time curves generated during the consolidation tests. It is generally acknowledged that the ratio between the coefficient of secondary compression and primary compression ratio (i.e., increment "CR" being the tangential slope of the ϵ_{ν} versus log $\sigma'_{\nu c}$ curve at a given stress level) tends to be a constant value for a given material (Mesri and Castro, 1987). This behavior is relied upon for estimating long-term creep settlement behavior in the numerical models designated for use by CPRA in the engineering phase of this project. The relationship between $C_{\alpha\epsilon}$ and CR for samples tested todate is illustrated in Figure B-12 (Appendix B).

3.3.2 Preconsolidation Pressure

Any elements within the natural ground clay having a preconsolidation pressure equal to the *in situ* vertical effective stress (i.e., $\sigma'_{vc} = \sigma'_{p}$) is considered to be normally consolidated. Elements with *in situ* vertical effective stresses less than the maximum past pressure are considered to be overconsolidated (the higher past stresses are most likely associated with post-deposition drained creep and desiccation related to vegetation within the upper 14 to 16 feet at the subject site). These two stresses define the stress history of a clay element which, in turn, strongly influences its undrained shear strength and future compression behavior when loaded.



Determination of the maximum past pressure is, therefore, critical to the evaluation. This determination involves estimating the vertical effective stress at which the transition from recompression to virgin compression occurs. Since the actual ε_{v} versus $\log \sigma'_{vc}$ curves measured in the laboratory do not consist simply of the two linear portions as discussed above, several techniques are conventionally used to provide an estimate of the maximum past pressure. The Casagrande construction (Casagrande, 1936) and strain energy methods (Becker et al., 1987) were used in our evaluation of the laboratory data.

Estimated maximum past pressure, σ'_p , values are included on the individual test summary plots in Appendix C and are summarized versus depth on Figure B-13 (Appendix B). The data indicate very slight degrees of overconsolidation (i.e., $\sigma'_p > \sigma'_{vo}$). Overconsolidation ratios, σ'_p / σ'_{vo} , typically ranged from about 1.5 to 10.

3.3.3 Coefficient of Consolidation

The coefficient of consolidation, c_v, is a parameter that quantifies the time-rate of consolidation and is dependent on, among other things, the material type and stress history. Coefficients of consolidation were computed using square-root and logarithm of time curve fitting techniques for each load increment applied during the consolidation tests. The relationship between the laboratory measured coefficient of consolidation (taken as the arithmetic average of the two curve fitting techniques) and the applied effective stress is presented for each test on the figures in Appendix C and are summarized on Figure B-14 in Appendix B.

3.3.4 Coefficient of Permeability

The coefficient of consolidation is inversely proportional to the coefficient of compressibility, m_{ν} , discussed above, and directly proportional to the coefficient of permeability, k_{ν} . Hence, the vertical coefficient of permeability, as a function of void ratio, can be derived from results of laboratory consolidation tests. The relationship between vertical coefficient of permeability, k_{ν} , and void ratio, e, based on results of consolidation tests are shown on Figure B-15 (Appendix B).

3.3.5 Settling Column Tests

Three representative composite samples were generated using discrete samples obtained from a total of 21 soil borings performed within the proposed borrow area by GeoEngineers in April 2013. Based on statistical evaluation of provided laboratory classification and index test data and review of general stratigraphy reflected on the supplied borrow area boring logs, it was decided that three composite samples would be prepared to represent materials from the three characteristic soil profiles typical of the borrow site. These three profile types, along with representative index properties, are summarized in the table below:



Composite I.D.	Borings Included	Soil Type	Depth Range (ft)	Moisture Content (%)	Liquid Limit (%)
Type 1	C-01-2 C-07-1	СН	0-8	108	113
Type 1	C-10-1 C-11-1	CL	8 – 10	40	38
Type 2	C-04-1 C-05-1	СН	0-8	108	102
Type 2	C-06-1 C-08-1	CL	8 - 15	35	35
	C-12-1 C-15-1	СН	0-8	106	104
Type 3	C-16-1 C-18-1	CL	8 – 12	38	38
	C-19-1	СН	12 - 20	55	55

Approximately 6-inch long portions of selected 2-foot core samples obtained from depths down to an average of 10 feet below the mudline were combined and mixed to create three composite samples. After mixing, each composite sample was split into three replicates (one for testing, one for archive storage, and one for CPRA use if requested). The remaining discrete borrow area samples were re-wrapped and preserved. The composite samples were sealed in air-tight plastic containers, and one of each type was shipped to Ardaman's Corporate Laboratory in Orlando, Florida for testing.

Laboratory settling test were performed in 20-cm diameter graduated plexi-glass settling columns. Test samples were mixed with synthesized marsh water having a salinity, in terms of total dissolved solids, of 10.5 g/l. Initial solids contents of the settling test samples ranged from about 13 to 13.5 percent, with corresponding initial total suspended solids concentrations ranging from 142 to 154 g/l. The slurry was mixed with a hand-held stirrer to provide a homogeneous sample, and remove any segregation of particles which occurred during placement of the slurry into the column. The columns were covered with clear plastic wrap to prevent evaporation of the supernatant fluid during the test period.

The settling tests consisted of visually monitoring the height of the sediment-water interface with time over a period of 28 days. The test results, in terms of interface height versus time are included in Appendix F. The initial slurry height in the cylinders at the start of the tests ranges from 150 to 154 cm. The initial settling velocities (i.e., the initial slope of the settled height versus time curve) ranged from 0.025 to 0.05 cm/minute. This more rapid "zone settling" behavior, prevailed during the first 30 to 36 hours of the test. Significant slower "compression settling" then commences and continued until the end of the 28-day test.



Final settled sediment heights ranges from 53 to 75 cm, with corresponding final solids contents ranging from 28 to 32 percent (total suspended solids concentrations of 225 to 400 g/l). Upon completion of the monitoring period, a series of 150 ml samples were extracted from the settled sediment at 5 to 10 cm depth intervals for moisture content determinations. Results of these tests, which reflect the variation in moisture content and density within the approximately 2 feet thick settled sediment sample, are plotted in Appendix F. These data were used to develop unit weight profiles characteristic of near-surface settled dredge deposits that were then used to compute void ratio versus effective vertical stress relationships for the very near-surface marsh creation deposits. These relationships, along with results of the slurry consolidation test described in the following section, will be incorporated in self-weight march consolidation settlement analyses.

3.3.6 Slurry Consolidation Tests

A one-dimensional incremental slurry consolidation test was performed on a sample prepared from the dredge borrow area Type 1 composite. The test was performed using specially designed and fabricated equipment with a counterbalance pulley system (to counteract a portion of the normal load associated with the top loading piston) that is similar to a conventional one-dimensional consolidation device except that the equipment used allows for evaluation of the consolidation behavior at stresses as low as 0.001 kg/cm2. For this test, the specimen is created and then incrementally loaded within a 10.2-cm diameter by 60-cm tall settling column to produce a specimen height at the end of settling of approximately 10 to 15 cm. After gravity settling is substantially complete, the specimen is loaded one-dimensionally under stresses of 0.001 to 0.13 kg/cm2 using a load increment ratio of 1.

The change in specimen height with time under each load was monitored and evaluated to characterize the one-dimensional compressibility, consolidation and drained creep properties of the sediment. Results of the slurry consolidation test are included in Appendix F.

3.4 Strength Tests

The strength characteristics of the marsh deposits are important for geotechnical engineering analyses, particular related to stability of the terrace berms and associated excavations.

Unconsolidated-Undrained Triaxial Compression Tests

A total of 160 unconsolidated-undrained (UU) triaxial compression tests (ASTM D2850) were performed on specimens trimmed from selected samples. Results of these strength tests are included on the soil boring logs in Appendix A. Individual UU test stress-strain curves are included in Appendix D. Undrained shear strengths from the UU compression tests are plotted versus depth in Figure B-16 (Appendix B).

3.4.2 Torvane Index Strength Tests

Hand-operated torvane (TV) index strength tests were performed in conjunction with the sample extrusion process. These test results are considered to be index strengths in that the



absolute value of the measured undrained shear strength is generally not considered adequately reliable for use in design. The test results, however, are useful in identifying soil strength variability and trends with respect to depth, material type, etc. A series of laboratory miniature vane (LV) shear strength tests were also performed on selected samples. Measured torvane and laboratory vane strengths, along with shear strengths measured in the UU compression tests, are presented versus depth in Figure B-17 (Appendix B). As can be seen, the TV and LV index test results are generally consistent with undrained shear strengths and the UU strengths derived from the compression tests.

3.4.3 Consolidated-Undrained Shear Strength Tests

Two consolidated-undrained (CK_oU) direct simple shear (CKoUDSS) strength tests were performed on selected samples consolidated in the laboratory under various vertical effective consolidation stresses. One test was performed at a vertical effective stress significantly greater than the in-situ preconsolidation pressure in order to determine normally consolidated undrained strength ratio, s_u/ o'_{vc}. The other test was performed on a specimen that was first consolidated under a vertical effective stress greater than the in-situ preconsolidation pressure and then unloaded to achieve an OCR of 3.0 to establish the relationship between strength ratio and overconsolidation ratio in accordance with the SHANSEP (Stress History and Normalized Soil Engineering Properties) design methodology (Ladd & Foott, 1974). These tests were used, along with the UU, TV, and LV strength data discussed above, to select final undrained shear strength profiles for use in design stability analyses, and to develop shear modulus values for use in undrained settlement calculations.

Undrained shear strength profiles are estimated in accordance with SHANSEP according to the following normalized undrained shear strength, s_u / σ'_v , equation:

$$s_u / \sigma'_v = C \cdot OCR^m$$

Where: OCR = overconsolidation ratio = $\sigma'_{vm} / \sigma'_{v}$

 $C = s_u / \sigma'_v$ for OCR = 1.0 (i.e., normally consolidated) m = experimentally determined exponent coefficient

Results of the CKoUDSS tests indicated SHANSEP strength parameters C=0.29 and m=0.85. These values are higher than normally expected for inorganic highly plastic clays (where C=0.24 and m=0.70 are more typical), which may reflect somewhat elevated organic contents in the samples selected for testing. An undrained shear strength profile computed according to the SHANSEP methodology and using somewhat more conservative parameters C=0.24 and m=0.70 is plotted alongside the current UU and TV strength test data on Figure B-17. As can be seen, the computed strength profile based on normalized clay behavior is consistent with the lower bound of the measured data. Considering the observed variability in measured shear strength data above the lower bound strength envelope, a somewhat higher design shear strength profile was developed for use in stability analysis.



SECTION 4. REFERENCES

- Becker, D. E., Crooks, J. H. A., Been, K., and Jefferies, M. B. (1987), "Work as a Criterion for Determining In Situ and Yield Stresses in Clays", Canadian Geotechnical Journal, Vol. 24, No. 4, pp 549-564.
- Casagrande, A. (1936), "The Determination of the Preconsolidation Load and its Practical Significance", Proceedings, First International Conference on Soil Mechanics and Foundation Engineering, Cambridge, Vol. 3, pp 60-64.
- Germaine, J., and Germaine, A. (2009). "Geotechnical Laboratory Measurements for Engineers." Hoboken, New Jersey: John Wiley and Sons, Inc.
- Ladd, C. C. and Foott, R. (1974), "New Design Procedure for Stability of Soft Clays," ASCE, JGGE, Vol. 100, No. G57, pp 763-786.
- Mesri, G. and Castro (1987), "C α /Cc Concept and KO During Secondary Compression". ASCE, JGGE, 113(3), pp 230-247.



APPENDIX A. BORING LOGS AND PROFILES

This Appendix contains the following:

- Figure A-1 Boring Location Plan
- Description of Terms & Symbols Used on Soil Boring Logs
- Soil Boring Logs
- Soil Boring Profiles



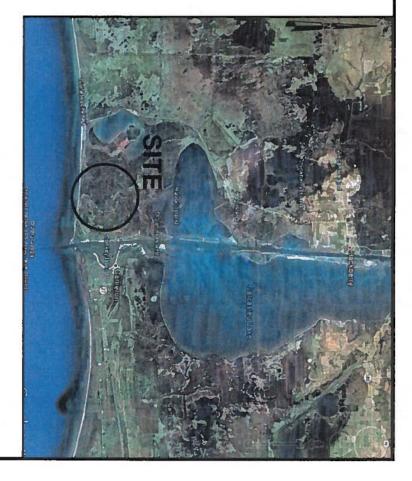
NOT TO SCALE

Confidential Information: Privileged & Confidential Work Product



NOTE:
BORING LOCATIONS ARE APPROXIMATE.

BORING LOCATION PLAN



VICINITY MAP

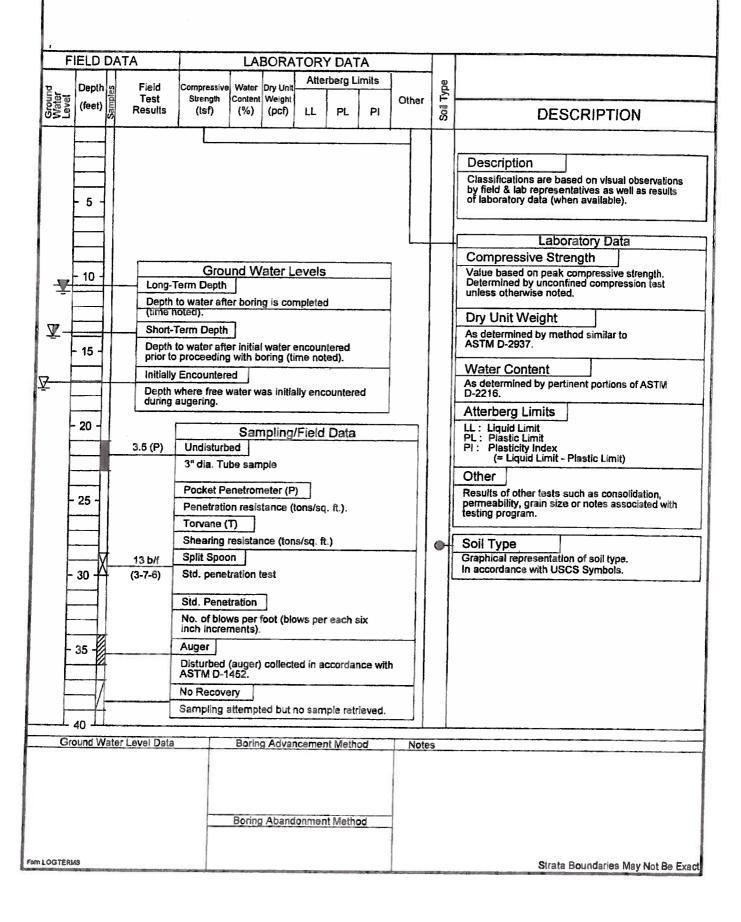
REFERENCE: SITE IMAGE BY GOOGLE.

RESTORATION PROJECT OYSTER BAYOU MARSH CAMERON PARISH, LOUISIANA

COASTAL PROTECTION AND RESTORATION AUTHORITY
BATON ROUGE, LOUISIANA

A-1	03-04-13	12-80-3741 03-04-13
Figure No.:	Date:	File No.:
RER	GTP	R. ROUSSET
Checked by:	Drawn by:	Project Engineer:
Jefferson, LA	Batan Rouge, LA	B.
ociates, Inc.	Ardaman & Associates, Inc.	Are
A		

DESCRIPTION OF TERMS AND SYMBOLS USED ON SOIL BORING LOG



LOG OF SOIL BORING B-01



File:

12-80-3741

Date:

10/3/12

Logged by: B. Singleton

Driller:

D. Tyler

CPRA Baton Rouge, LA

Sheet 1 of

Baton Rouge Geotechnical Laboratory
AASHTO Accredited Laboratory , LELAP Certificate No. 02052,
USACE Validated

Rig:

Airboat

Strata Boundaries May Not Be Exact

F	FIELD	DATA		L	ABORA	ATO			Valida	ted		Location: Lat. 29° 47′ 9"
		60	i ve		100.1		berg L		, no		ype	Long. 93° 25' 0.4"
Ground Water	Depth (feet)	Field Test	press engti	Water Content	Dry Unit Weight				Percent Passing #200 Sieve	Other	Soil Type	Surface Elevation: -0.49 (ft., NAVD)
Level	(icet)	Results	Compressive Strength (tsf)	(%)	(pcf)	LL	PL	PI	Pe Pa #200		Š	Description
		_ 0.0 (P)	0.19 t=1.0	86		104	33	71	95	ORG,		Very soft brown and gray CLAY (CH) w/ shells and trace organics
		0.0 (P)		95 81	48 48							and trace organics
		5.5 (. /	0.06	••								
	- 5 -	_ 0.0 (P)	t=2.0	71 81	58 53	59	17	42		ORG₂		
		0.0 (P)		78	53							
			0.17	73								
		0.0 (P)	t=4.0	87 80	53 52	73	22	51				
	- 10 -	0.0 (P)		61	61							
		F 0.0 (D)	0.07	54	60	70	4.7			000		
		_ 0.0 (P)	t=6.0	69 67	60 55	78	17	61		ORG₃		
	-15-	0.0 (P)		63 57	60							
		0.25 (P)	0.40 t=7.0	133	36	188	48	140		ORG₄		Soft gray ORGANIC CLAY (OH)
		0.75 (D)	1.51	228	24							
		_ 0.75 (P)	t=8.0	18 19	120 108							Stiff gray SILTY CLAY (CL) w/ trace sand
	- 20 -											Very stiff gray SANDY CLAY (CL) w/ organics
								ı				
l		0.75 (P)	2.18 t=10.0	21	107	47	12	35	69			
	- 25 -	0.73 (F)		22	104	2	18		09			
		0.75 (P)		27	100							
		- 0.75 (P)		21	100							
	-30-								Some Saltone.			Medium dense gray CLAYEY SAND (SC) w/ trac
												silt
		1.75 (P)	5.75 t=14.0	24	101				22	GSH		
	- 35 -	1.75 (P)		26	92							
ŀ												Stiff brown and gray CLAY (CH) w/ silty sand layers
ļ			1.46	20	0.0	FO	4-	40				
}		1.0 (P)	t=16.0	32 31	88 86	59	17	42				
	-40-	Water Level Da	la .	TE	Boring Ac	vance	ment l	Method	1	Note	es.	Boring completed at 40 ft.
	/ater E	4" Nom. Dia. Short Flight Auger: 0 to 6 ft. 4" Dia. Rotary Wash: 6 to 40 ft.									Inconeral P H: Hy G ₁ = 1 G ₂ = 4	3.6% Confidential Information
Borehole grouted with cement/									ORG ₃ = 3.6% Confidential Information. Privileged & Confidential Work Product			
												VVORK Product

LOG OF SOIL BORING B-02



File: Date: 12-80-3741 10/3/12

Logged by: B. Singleton

Driller:

Rig:

D. Tyler Airboat

CPRA Baton Rouge, LA

Sheet 1 of 2 Baton Rouge Geotechnical Laboratory
AASHTO Accredited Laboratory, LELAP Certificate No. 02052,
USACE Validated

FIELD DATA LABORATORY DATA Location: Lat. 29° 47' 16" Long. 93° 24' 37.1" Compressive Strength (tsf) Percent Passing #200 Sieve Atterberg Limits Surface Elevation: -0.32 (ft., NAVD) Depth Field Ground Dry Unit Weight (pcf) Water Other Soil (feet) Test Content LL PL Level (%) Ы Results Description 0.0 (P) **119** 41 Very soft gray CLAY (CH) w/ trace organics and 88 0.05 58 68 70 21 49 89 t=2.0 0.0 (P) 95 97 53 ORG. 0.09 0.0 (P) 58 65 19 46 46 GSS 70 Very loose gray CLAYEY SAND (SC) w/ shell 5 t=2.0 fragments _ 0.0 (P) 63 66 Very soft gray CLAY (CH) w/ shell fragments 57 0.11 0.0 (P) 75 56 76 20 56 t=4.0 73 55 0.13 10 0.0 (P) 59 65 **72** 18 54 t=5.0 61 0.0 (P) 0.25 0.0 (P) 56 69 **75** 19 56 95 **GSH** t=6.0 15 53 66 57 0.0 (P) 0.18 0.25 (P) 50 74 47 13 34 Very soft gray SILTY CLAY (CL) t=8.0 47 69 20 Stiff to very stiff gray SILTY CLAY (CL) 1.75 (P) 25 2.38 19 110 t=12 0 2.0 (P) 19 112 30 3.0 (P) 23 108 35 Stiff gray CLAY (CH) w/ silt layers NR **4**0 **Continued Next Page** Ground Water Level Data **Boring Advancement Method** 4" Nom. Dia. Short Flight Auger: t: Unconsolidated, Undrained Triaxial Compression Test Lateral Pressure = psi 0 to 6 ft. Water Elevation at Gauge 4" Dia. Rotary Wash: GSH: Hydrometer Particle Size Analysis Location = 0.68' 6 to 45 ft. GSS: Particle Size Analysis

Water Depth at Borehole = 1'

LOGOTR GDT

Boring Abandonment Method Borehole grouted with cement/ bentonite upon completion

 $ORG_1 = 5.2\%$

Confidential Information. Privileged & Confidential Work Product

Strata Boundaries May Not Be Exact

LOG OF SOIL BORING B-02

File: Date:

12-80-3741

ite: 10/3/12

Logged by: B. Singleton Driller: D. Tyler

Sheet 2 of 2

CPRA Baton Rouge, LA

Baton Rouge Geotechnical Laboratory
AASHTO Accredited Laboratory , LELAP Certificate No. 02052,

Rig:

Airboat

Baton Rouge, LA	AASHTO Accredited Laboratory, LEL USACE Validat	AP Certificate No. 02052,
FIELD DATA	LABORATORY DATA	Location: Lat. 29° 47' 16"
	Atterberg Limits	த Long. 93° 24' 37.1"
Ground Depth G Field	Water Dry Unit 3 is o	Other Other Control Co
Ground Depth Water Level (feet) Level (Feet) Results (St.)	Water Content (%) Weight (pcf) LL PL PI 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Description
M 4 b/f		Stiff gray CLAY (CH) w/ silt layers
1-2-2	1	
	54 18 36	
2.0 (P) 2.00 t=18.0	31 90	
45	_ 30_ _86 _	Boring completed at 45 ft.
		Boring completed at 45 ft.
	1	
	1 1 1	
-50-	1	
I		
-55-		
I		
-60-		
65-		
-70-		
I		
I I		
	1	
-75-	1 1 1 1 1 1	
,		
 		
Water Elevation at Gauge Location = 0.68' Water Depth at Borehole = 1'		
Ground Water Level Data	Boring Advancement Method	Notes t: Upconsolidated Undrained Triavial Compression Test
	4" Nom. Dia. Short Flight Auger: 0 to 6 ft.	t: Unconsolidated, Undrained Triaxial Compression Test Lateral Pressure = psi
	4" Dia. Rotary Wash: 6 to 45 ft.	
Water Depth at Borehole = 1'	0 to 40 it.	
	Boring Abandonment Method	Confidential Information: Privileged & Confidential
	Borehole grouted with cement/	Work Product
	bentonite upon completion	
-		Strata Boundaries May Not Be Exact

LOG OF SOIL BORING B-03



File: Date:

12-80-3741 10/5/12

Logged by: B. Singleton

Driller: D. Tyler

CPRA Baton Rouge, LA Sheet 1 of 1

Baton Rouge Geotechnical Laboratory
AASHTO Accredited Laboratory, LELAP Certificate No. 02052,
USACE Validated

Rig:

Airboat

Strata Boundaries May Not Be Exact

	FIELD C	DATA		L/	ABORA	ATOF		ATA	Vallua			Location: Lat. 29° 47′ 22" Long. 93° 24' 16.4"
	se		sive			Atterl	berg L	imits	int ng eve	'	Тур	Surface Elevation: -0.60 (ft., NAVD)
Ground Water Level	Depth de (feet)	Field Test Results	Compressive Strength (tsf)	Water Content (%)	Dry Unit Weight (pcf)	LL	PL	PI	Perce Passir #200 Si	Other	Soil Type	Description
<u> </u>		0.0 (P)	0.06 t=1.0	66 87	62 53	68	17	51	98			Very soft gray CLAY (CH)
		0.0 (P)	0.10 t=2.0	51 43	72 76	43	16	27		ORG ₁		Very soft gray SILTY CLAY (CL) w/ shells
	- 5 -	0.0 (P)		43	75		1					
		0.0 (P)	0.18 t=3.0	63 51	65 68	45	16	29				
		0.25 (P)								ļ		
	-10-	0.0 (P)		64 71 71	56 59 60	74	17	57	96	GSS		Very soft gray CLAY (CH) w/ trace shell fragments
		0.25 (P)		74	56				ļ			
	- 15 -	 [1.75 (P)	 	74	54				 			Stiff gray SILTY CLAY (CL) w/ sand pockets
		2.0 (P)	1.41	23	104	44	14	30				
		2.0 (P)	t=7.0 1.51	23	105	49	14	35	75			
	-20-	_ 2.0 (P)	t=8.0	22 24	104		į					
		_								}		
	- 25	2.0 (P)		24	97							
		1.75 (P)		24	00				98		M	Loose tan and gray SILT (ML)
	-30-		 	_31	86			1				Medium to stiff light gray CLAY (CH)
			1.06									
		1.25 (P)	1.06 t=14.0	34	87 86	57	19	38				
	35	-										
					}							
		. 75 (D)		41	84							w/ sand, 38-40 ft.
	L ₄₀ _	1.75 (P)						1		I No	otes	Boring completed at 40 ft
	Water El Location		auge	0 to	Boring A Nom. Dia 6 ft. Dia. Rota 40 ft.	. Shor	t Fligh			t: La G:	Unce teral SS: F	onsolidated, Undrained Triaxial Compression Test l Pressure = psi Particle Size Analysis = 2.1%
	Water De 1.25'	epth at Borel	hole =									Confidential Information:
			Por	Boring Abandonment Method Borehole grouted with cement/							Privileged & Confidential Work Product	
				ber	ntonite u	ipon c	ompl	etion	C110			Strata Boundaries May Not Be Ex

LOG OF SOIL BORING B-04



File:

12-80-3741

Date:

10/6/12 Logged by: B. Singleton

Driller:

D. Tyler Airboat

CPR/ Bato		ge, LA	<u>.</u>			Accredi	ted Lai	ge Geo borator JSACE	y , LE Valida	al Labo LAP Cer	ratory tificate	e No. 02052,
F	FIELD	DATA			ABORA						e e	Location: Lat. 29° 47' 11.4" Long. 93° 24' 2"
Ground	Depth	sejo Fie	essiv ngth	Water	Dry Unit		berg L	imits	sing Sieve	Othor	Soil Type	Surface Elevation: -0.68 (ft., NAVD)
Water	(feet)	Fie Tes Resu	st 🖺	Content (%)	Weight (pcf)	LL	PL	PI	Perc Pas:	Other	Soi	Description
		_ 0.0 (F	3)	126 79	40							Very soft gray CLAY (CH) w/ trace organics and shell fragments
		0.0 (F	o.09 t=2.	5 64	65	57	16	41	ì	ORG₁		
	- 5 -	0.0 (F	2)	74 63	53							
		0.0 (F	0.09 t=3.		53 51	78	19	59		:		
	40	0.0 (f	t-4.	0 60	64 58	64	16	48	97 86	ORG ₂		
	-10-	0.0 (F	?)	87 65 66	61							
		0.0 (F	O.1 t=6.	79 0 85	53 47	93	20	73		ORG ₃		
	-15-	0.0 (2)	87 85	46							Very soft gray SILTY CLAY (CL)
		1.0 (I	O.1 t=7.		99	32	14	18	1			
		1.5 (O.1 t=8.		107	26	15	11				
	- 20 -		1.7									
	-25-	2.25	(P) t=10	.0 21	108	32	18	14	59			Stiff gray SANDY CLAY (CL)
	- 30 -			30	89							Stiff tan and gray CLAY (CH) w/ silt layers
	- 35 -	2.0 (1.9 t=14		84	69	24	45				
6												
		1.75	(P)	39	80_							
	Ground Water Level Data Boring Advancement Method								od	Not		Boring completed at 40 ft.
<u>↓</u> \	4" Nom. Dia. Short Flight Auger: 0 to 6 ft.									Lat OR OR	teral G ₁ = G ₂ =	nsolidated, Undrained Triaxial Compression Test Pressure = psi 2.1% 2.7% 6.3% Confidential Information: Privileged & Confidential
\ \times \times \ \ti				Boring Abandonment Method Borehole grouted with cement/ bentonite upon completion								Privileged & Confidential Work Product Strata Boundaries May Not Be Exac

LOG OF SOIL BORING B-05



File: Date:

12-80-3741

10/8/12 Logged by: B. Singleton

Driller: D. Tyler

CPRA Baton Rouge, LA

1.17'

Baton Rouge Geotechnical Laboratory

AASHTO Accredited Laboratory, LELAP Certificate No. 02052,

USACE Validated

Rig:

Airboat

Confidential Information:

Privileged & Confidential

Work Product

Strata Boundaries May Not Be Exact

·			\ <u>\</u>			1000			JSACE	Valida	ted		Location: Lat. 29° 46' 59.6"
	FIELD) L	DATA		L/	ABORA			AIA		ı	e l	Long. 93° 23' 56.2"
Ground Water	Depth (feet)	amples	Field Test	Compressive Strength (tsf)	Water Content		Atter	berg L PL	imits.	ercent passing 00 Sieve	Other	Soil Type	Surface Elevation: -0.51 (ft., NAVD) Description
Level	ļ	S	Results	8	(%)	(pcf)				# 2		222	•
	<u> </u>		0.0 (P)										Very soft gray CLAY (CH) w/ trace organics
	<u> </u>		0.0 (P)		85	51							
	- 5 -		_ _ 0.0 (P)	0.07 t=2.0	92	50	87	22	65	97	ORG₁		
			0.0 (P)		91 79	49					GSS		w/ shells at 6-10 feet
		The state of	0.0 (P)	0.14 t=4.0	86 84	52	101	25	76	8			
	-10-		0.0 (P)		88	49					Ė		
			_ 0.0 (P)	0.20 t=6.0	79	55	63	17	46		ORG ₂		
	-15-		_ 0.0 (P) -		92 98	51							Medium to stiff brown and gray CLAY (CH) w/ silty sand
			1.25 (P)	0.67 t=7.0	28 29	93 98	52	16	36	8			
		ı	_ 1.5 (P)	1.34 t=8.0	21 24	108 98	51	14	37	5			
	- 20 -		-			30							
	-	(Included)	_ 2.25 (P)		20	105				55			Stiff gray SANDY CLAY (CL)
	- 25 -		-0	0.92	32	91	50	18	32	99			Medium to stiff gray CLAY (CH) w/ silt layers
	-30-		2.25 (P)	t=12.0	30	93	30	10	32	99			
	- 35 -		- 1.25 (P) -		37	84							
	-40-		1.0 (P)	1.32 t=16.0	41	83 75	84	26	58	100			Boring completed at 40 ft
	Ground	W	ater Level Dat	ta		Boring Ad					Not		nsolidated, Undrained Triaxial Compression Test
1.0 (P)							r .	Lat GS OR	eral i S: Pa	Pressure = psi article Size Analysis 6.6%			

Boring Abandonment Method

Borehole grouted with cement/ bentonite upon completion

LOG OF SOIL BORING B-06



File: 12-80-3741

Date: 10/6/12

Date: 10/6/12 Logged by: B. Singleton

Airboat

Driller: D. Tyler

CPRA Baton Rouge, LA Sheet 1 of 2

Baton Rouge Geotechnical Laboratory

AASHTO Accredited Laboratory, LELAP Certificate No. 02052,

USACE Validated

Rig:

_

		_								Valida	ted		Location: Lat. 29° 46' 52.2"		
	FIEL	D [ATA		L.	ABORA						e	Long. 93° 24' 6.3"		
Ground	D	les	Field	ssive gth	Water	Dry Unit	Atter	berg L	imits	ent ing jeve	ļ	Soil Type	Surface Elevation: -0.77 (ft., NAVD)		
Water Level	(feet		Test Results	Compressive Strength (tsf)	Content (%)	Weight (pcf)	LL	PL	PI	Perc Pass #200 3	Other	Soi	Description		
_			_ 0.0 (P)			40							Very soft gray CLAY (CH)		
		-1	0.0 (P)	0.11	89 95	48 50	97	25	72		ORG₁				
		1	_	t=2.0 0.06	l 										
	- 5	-1	_ 0.0 (P)	t=2.0	99	47	98	24	74				w/ shells at 4-12 feet		
			0.0 (P)							ļ					
		-11	0.0 (P)	0.15	90 83	42 55	95	28	67						
	-10		_ 0.0 (1)	t=4.0					"	ļ					
			_ 0.0 (P)		92	47									
		-8	0.0 (P)	0.09 t=6.0	97	47	103	29	74		ORG ₂				
		8	_ _ 0.75 (P)	1-0.0	35	-							Stiff gray SANDY CLAY (CL)		
	-15	-1	-		18	111							Sun gray SANDT CLAT (CL)		
			2.5 (P)	1.41 t=7.0	18 24	103	49	14	35	69					
		j.	- - 0.0 (D)												
	- 20		2.0 (P)						-				OVER THE PROPERTY OF THE PROPE		
	<u> </u>	-				l							Stiff gray CLAY (CH) w/ silt layers		
			= 2.75 (P)												
		-	= 1.75 (P)	1.54 t=10.0		104 105	57	14	43						
	- 25	_		10.0	26	103									
		-		1.32	ļ	 			 		-	1833	Stiff gray SILTY CLAY (CL) w/ sand		
			1.5 (P)	t=12.0	31	90	29	19	10						
	-30				29	89					•				
					ļ		ļ		ļ						
	\vdash	0	=3					1			l		Stiff gray CLAY (CH) w/ silt layers		
	- 35		0.75 (P) -												
	<u> </u>	\dashv						ļ							
		1	L												
			2.25 (P)		39		77	23	54	ļ					
	L-40		/ater Level Da	ıta		Boring A	dvano	emen	Meth	od .	l No	tes	Continued Next Page		
	C. 00		L0101 0a		4" N	lom. Dia					t:	Unco	onsolidated, Undrained Triaxial Compression Test		
			evation at Ga	auge		ia. Rota	ry Was	sh:			OF	RG, =	Pressure = psi 5.2%		
- 1	Location = 0.65' 6 to 60 ft. Water Depth at Borehole =										$ORG_2 = 3.0\%$				
•	1.42'					Boring Abandonment Method						Confidential Information, Privileged & Confidential			
					Bor	Boring Abandonment Method Borehole grouted with cement/ bentonite upon completion						Work Product			
					Den	nonite u	hou c	ompl	ELIOFI				Strata Boundaries May Not Be Exa		

LOG OF SOIL BORING B-06



File:

12-80-3741

Date: 10/6/12 Logged by: B. Singleton

Driller: D. Tyler

CPRA Baton Rouge, LA Sheet 2 of 2

Baton Rouge Geotechnical Laboratory
AASHTO Accredited Laboratory LELAP Certificate No. 02052,

Rig:

Airboat

Bato		_							JSACE	Valida		Location: Lat. 29° 46' 52.2"			
F	IELC	D (ATA		L/	ABORA						9	Long. 93° 24' 6.3"		
Ground Water Level	Depth (feet)	Samples	Field Test Results	Compressive Strength (tsf)	Water Content (%)	Dry Unit Weight (pcf)		berg L PL	PI	Percent Passing #200 Sieve	Other	Soil Type	Surface Elevation: -0.77 (ft., NAVD) Description		
		#		0	35	81							Stiff gray CLAY (CH) w/ silt layers		
	-45-		1.25 (P)	1.13 t=18.0	28 26	93 93	32	13	19				Stiff gray SILTY CLAY (CL) w/ sand and shells		
	- 50 -		0.75 (P) -	1.68 t=20.0	40 38	82 84	66	22	44				Stiff gray CLAY (CH) w/ silt layers		
	- 55 -		1.0 (P)	1.51 t=22.0	38 41	83 76	63	20	43	100	l l				
	- 60 -		- _ 0.75 (P) 	1.73 t=24.0	47 43	_7 <u>6</u> _	78	21	57				Design asymptoted at 60 ft		
		1											Boring completed at 60 ft.		
		<u> </u>													
	-65-	$\left\ \cdot \right\ $									ļ				
		$\left\ \cdot \right\ $													
]													
	- 70 -	11								ļ					
		11			ļ										
	- 75	┧ [
		$\ \ $													
		7													
	80-			<u> </u>	<u> </u>		<u> </u>			<u> </u>	<u> </u>	ļ	<u> </u>		
	Ground Water Level Data Boring Advancement Method 4" Nom. Dia. Short Flight Auger: 0 to 6 ft. 4" Dia. Rotary Wash: 6 to 60 ft.									t:	t: Unconsolidated, Undrained Triaxial Compression Tes Lateral Pressure = psi				
1.42' Boring Abandonment Method Borehole grouted with cement/								•	Confidential Information: Privileged & Confidential Work Product						
					Bor ben	ehole gi tonite u	routed pon c	with omple	ceme	ent/	t/				
													Strata Boundaries May Not Be Exa		

LOG OF SOIL BORING B-07



File: Date:

12-80-3741

Airboat

10/1/12 Logged by: B. Singleton

Driller: D. Tyler

Sheet 1 of 2

CPRA Baton Rouge, LA

Baton Rouge Geotechnical Laboratory
AASHTO Accredited Laboratory , LELAP Certificate No. 02052,
USACE Validated

Rig:

F	FIELD) [ATA		L	ABORA	ATOF			Valida	iou_		Location: Lat. 29° 46' 56.4" Long. 93° 24' 43.4"		
		es		ssive jth				berg L	imits	ant ng leve		Soil Type	Surface Elevation: 0.57 (ft., NAVD)		
Ground Water Level	Depth (feet)	Sаmp	Field Test Results	Compressive Strength (tsf)	Water Content (%)	Dry Unit Weight (pcf)	LL	PL	PI	Percent Passing #200 Sieve	1	"	Description		
			0.0 (P)	0.37 t=2.0	187 84	51	106	30	76	94	ORG,		Very soft to soft gray CLAY (CH) w/ silt		
			 _ 0.0 (P) _	0.08 t=1.0 0.05	84 104 91	52 30 49	114 109	27 24	87 85	48	GSН		w/ shells and sand layers at 2-12 feet		
	- 5 -		_ _ 0.0 (P)	t=2.0 0.17 t=3.0	114 88 78	52 60	91	25	66	89 64	GSS				
			_ 0.0 (P)	0.02 t=3.0	62 71	63 58	85 68	20 19	65 49		ORG,				
	-10-		0.0 (P)	0.16 t=6.0 0.17	89 66 73	50 64 56	71	19	52	10 97	GSS				
			C 0.0 (P)	t=6.0 0.18	64 64	65 53	62	16	46						
		100	0.0 (P)	t=5.0 0.26 t=8.0	82 81 88	55 51 51	104	24	80						
	-15-		C 0.25 (P)	0.26 t=14.0	87 80	53			ļ						
			0.75 (P)	0.21 t=28.0	77 47	55 68 75	95	21	74						
	- 20 -		= 2.0 (P) =	0.24 t=7.0 0.07 t=8.0	45 27 28	90	118	28	90						
	- 25 -		1.5 (P)	1.87 t=10.0	22 21	108 103	45	12	33				Stiff gray SILTY CLAY (CL)		
			- - 1.5 (P)				:	:							
	-30		- 1.5 (1)		23	101		; ;							
			1.25 (P)	1.19 t=14.0		100	44	13	31						
	- 35		C 0.75 (P)		22	104									
			L 0.73 (F)		25	92			<u> </u>						
	Ground Water Level Data Boring Advancement Method											tes	Continued Next Page		

Water Elevation at Gauge Location = 0.90' Water Depth at Borehole =

4" Nom. Dia. Short Flight Auger: 0 to 12 ft.

4" Dia. Rotary Wash: 12 to 42 ft.

Boring Abandonment Method

Borehole grouted with cement/ bentonite upon completion

t: Unconsolidated, Undrained Triaxial Compression Test Lateral Pressure = psi GSS: Particle Size Analysis

GSH: Hydrometer Particle Size Analysis

ORG₁ = 9.8% ORG₂ = 4.1% ORG₃ = 3.9%

Confidential Information: Privileged & Confidential Work Product

Strata Boundaries May Not Be Exact

0.33

LOG OF SOIL BORING B-07



File: Date: 12-80-3741

te: 10/1/12

Logged by: B. Singleton

Driller:

D. Tyler

CPRA Baton Rouge, LA Sheet 2 of 2

Baton Rouge Geotechnical Laboratory

AASHTO Accredited Laboratory, LELAP Certificate No. 02052,

Rig:

Airboat

Bato	n Ro	uge	, LA		P	ASHTO A	Accredi	ited Lai	borator JSACE	y , LEI Valida	.AP Çer led	AP Certificate No. 02052, id				
	FIELD DATA				LABORATORY DATA								Location: Lat. 29° 46' 56.4"			
	9		avissenge Courter (%) Water Content (%) Water Content (%) Water Content (%) Atterberg Limits Atterberg Limits Page 2002 #								Soil Type	Long. 93° 24' 43.4"				
Ground	Depti	ple	Field	ress ingt	Water	Dry Unit Weight			-	cen saing	Other	Ē	Surface Elevation: 0.57 (ft., NAVD)			
Ground Water Level	(feet	Sarr	Test Results	Omp Stre (t	Content (%)	Weight (pcf)	LL	PL	PI	Per Pas	•	So	Description			
		N		ŭ						#		NOV	Stiff gray SILTY CLAY (CL)			
	<u> </u>	-	2.0 (P)										Sull gray SILTY CLAT (CL)			
					_ 24	_102_						YVX	Boring completed at 42 ft.			
1		11										ļ				
l	-45															
	73															
		41			ļ						i					
		-11	ß is					1		İ						
		+) 									}				
	-50	11]										
l		11														
]	98													
	L	╝	3]					
	- 55	4										ļ				
1		┨╏	0						İ							
	-	\dashv					İ				:					
		1	10													
	-60															
ł	_ 60			:			1			ļ						
ı		ا ـ) 			İ			Į							
ı		\dashv														
1	<u> </u>	-														
	-65	-				ļ		Ì								
I		7				1			Ì							
i								ļ		1		1				
]				ŀ										
	- 70	_				1										
1		4								ļ						
1		\dashv			ĺ											
	-	\exists				[
1	7.	1				1					1		1			
1	- 75															
2																
		\downarrow														
		\dashv														
	[⊥] 80				<u> </u>		<u> </u>		<u> </u>	<u> </u>	<u> </u>					
	Grou	nd V	Vater Level Da	ta		Boring A					No	tes				
	4" Nom. Dia. Short Flight Auger: 0 to 12 ft.															
¥ \	Water Elevation at Gauge Location = 0.90' 4" Dia. Rotary Wash							sh:								
Ŷ,	Water		pth at Boreh	'-"	J 7£ 11.					Confidential Information: Privileged & Confidential Work Product						
(0.33'				Boring A	hando	nmen	Meth	od							
2					Bor	Boring Abandonment Method Borehole grouted with cement/										
3					ben	bentonite upon completion										
												Strata Boundaries May Not Be Exa				

LOG OF SOIL BORING B-08



File: Date: 12-80-3741

Privileged & Confidential

Work Product

Strata Boundaries May Not Be Exact

10/2/12 Logged by: B. Singleton

Driller:

D. Tyler

CPRA Baton Rouge, LA

Sheet 1 of 1 Baton Rouge Geotechnical Laboratory
AASHTO Accredited Laboratory, LELAP Certificate No. 02052,
USACE Validated

Rig:

Airboat

	FIELD	DATA		L	ABOR	ATO			Valida	ieu		Location: Lat. 29° 46' 41.7" Long. 93° 24' 55"		
		S	isive th			Atter	berg L	imits	nt gr eve		Lype	Surface Elevation: -0.08 (ft., NAVD)		
Ground Water Level	Depth (feet)	Results	Compressive Strength (tsf)	Water Content (%)	Dry Unit Weight (pcf)	LL	PL	PI	Perce Passir #200 Si	Other	Soil Type	Description		
_		_ 0.0 (P)		44 67	!		1887-196 					Very soft gray CLAY (CH) w/ sand and shells		
	-	0.0 (P)	Ì	56	67									
	—	- 0.0 (1 /	0.03	81	50									
	- 5 -	0.0 (P)	t=2.0	89 72	48	85	25	60	69 86					
		0.0 (P)		63 88	56									
	<u> </u>	0.0 (P)	0.18 t=4.0	75 78	57	103	28	75	90	GSS		Very soft gray CLAY (CH)		
	-10-		1-4.0	74	48				1					
		0.0 (P)	0.10	85	47									
		0.0 (P)	t=6.0	54 86	71 45	64	18	46				w/ silt pockets at 12-14 feet		
	-15-	0.0 (P)		55	70									
	13		0.10	87	50	00	22	60	76	GSS				
	<u> </u>	0.0 (P)	t=7.0	71	57	82	22	60	76	GSS		w/ shells at 16-20 feet		
	⊢	1	0.07 t=8.0	85 82	48 54	93	25	68	ļ			w/ stiells at 10-20 feet		
	-20-		1-0.0	64	62									
	20-		-				ļ		<u> </u>					
	-											Medium gray and tan SILTY CLAY (CL)		
		2.5 (P)	0.73	25	100	39	13	26						
	- 25 -	2.5 (F)	t=10.0	40	80	39	'3	20	3	1				
	25													
	-		İ			ļ						1		
	1	F	0.62 t=12.0	28	99	38	13	25	1					
	30-	3.5 (P)	12.0	20	103									
	-30-													
	-													
					1				18					
	-35-	0.75 (P)			<u></u>				0.0000000000000000000000000000000000000		***	1		
											,,,,,	Loose gray CLAYEY SAND (SC)		
		11									77 97 V			
	-	0.75 (P)	2.82	18	112	29	17	12	48					
	40-		t=16.0	26	100									
		l Water Level D	ata		Boring A	dvanc	ement	Metho	od	No		Boring completed at 40 ft		
					4" Nom. Dia. Short Flight Auger:							nsolidated, Undrained Triaxial Compression Test		
		Elevation at G	auge		ia. Rotai	ry Was	sh:			Lateral Pressure = psi GSS: Particle Size Analysis				
		on = 0.50' Depth at Bore	hole =	6 to	6 to 40 ft.									
	0.58'											Confidential Information:		
Boring Abar								Meth	od			Privileged & Confidential		

Borehole grouted with cement/ bentonite upon completion

CPRA

Baton Rouge, LA

LOG OF SOIL BORING B-09



Baton Rouge Geotechnical Laboratory
AASHTO Accredited Laboratory, LELAP Certificate No. 02052,

File:

12-80-3741

Date:

10/4/12 Logged by: B. Singleton

Driller:

D. Tyler

Rig:

Airboat

Strata Boundaries May Not Be Exact

	FIELD)ATA	<u> </u>	1	ABOR	ATO			Valida	ted		Location: Lat. 29° 46' 35.1"		
			0				berg L				be 'pe	Long. 93° 25′ 3.7″		
Ground	Depth ☐	Field	ressi ngth	Water	Dry Unit		berg L	imits	cent sing Siev	Other	Soil Type	Surface Elevation: 0.03 (ft., NAVD)		
Vater Level	Depth (feet)	Test Results	Compressive Strength (taf)	Content (%)	Weight (pcf)	LL	PL	PI	Per Pas #200	Other	တိ	Description		
		0.0 (P)	0.22 t=1.0	61	62	97	26	71				Very soft gray CLAY (CH) w/ silt		
		_ 0.0 (P)	0.16 t=2.0	73 87	52 51	104	27	77	98					
	- 5 -	0.0 (P)												
		0.0 (P)	0.17 t=3.0	85 87 88	48 53 48	75	21	54	94	GSS		w/ shells at 6-12 feet		
		0.0 (P)		!										
	-10-	0.0 (P)	0.06 t=5.0	84 85	52 48	99	27	72						
		0.0 (P)		84	55									
	- 15 -	0.0 (P)	0.18 t=6.0	79 84	55 49	95	25	70						
		C 0.0 (P)		48 79	59							w/ sand layers at 16-18 feet		
		0.0 (P)	0.89 t=8.0	22 24	104 106	35	12	23				Medium gray SILTY CLAY (CL) w/ sand		
	- 25 -	3.25 (P)	2.08 t=10.0	24	109 100	40	14	26				Stiff to very stiff tan and gray SILTY CLAY (CL)		
	-30-	2.0 (P) 2.0 (P)	1.58 t=14.0	29 35	88	39	20	19	100					
	- 35 -			32	85				100		2383	Stiff gray CLAY (CH) w/ shells		
		1.5 (P)		39		80	24	56		ORG.				
	40	- (, ,		40	73									
		Vater Level Da	ıta	T	Boring A	dvanc	ement	Metho	d	Nol		Boring completed at 40 ft		
L	Vater Ele .ocation Vater De 0.67'	0 to 4" D	4" Nom. Dia. Short Flight Auger: 0 to 6 ft. 4" Dia. Rotary Wash: 6 to 40 ft.							nsolidated, Undrained Triaxial Compression Test Pressure = psi article Size Analysis 3.5% Confidential Information:				
					Boring A					Privileged & Confidential				
					ehole gr tonite u				ent/			Work Product		

LOG OF SOIL BORING B-10



File: 12-80-3741

Date: 10/2/12

Privileged & Confidential

Work Product

Strata Boundaries May Not Be Exact

Logged by: B. Singleton **Driller:** D. Tyler

CPRA Baton Rouge, LA Sheet 1 of 2

Baton Rouge Geotechnical Laboratory
AASHTO Accredited Laboratory, LELAP Certificate No. 02052,
USACE Validated

Rig:

Airboat

FIELD DATA					L/	ABORA	ATOF	RY D				, a	Location: Lat. 29° 46' 39.9" Long. 93° 24' 27.9"			
		88		ssive			Atter	berg L	imits	ng eve		Soil Type	Surface Elevation: 0.17 (ft., NAVD)			
round Nater Level	Depth (feet)	Ѕатр	Field Test Results	Compressive Strength (tsf)	Water Content (%)	Dry Unit Weight (pcf)	LL	PL	PI	Perce Passii #200 Si	Other	Soil	Description			
			0.0 (P)							"			Very soft gray CLAY (CH)			
		I	0.0 (P)	0.18 t=2.0	88 88 57	47 53 62	87	21	66							
	- 5 -		- _ 0.0 (P)	0.06 t=2.0	56	63 59	93	23	70	96	GSS		w/ shells at 4-8 feet			
			0.0 (P)		64 79 64											
	- 10 -		- _ 0.0 (P) -	0.18 t=4.0	72 93 87	52 50 49	94	22	72							
			0.25 (P) 0.0 (P)		91	47	į									
	45	L. L.	- - - 0.25 (P)	0.24	86 75	45 55	76	21	55							
	15 -		-	t=6.0 0.10	68 28	57 100	51	15	36				w/ silt at 16-20 feet			
			_ 0.5 (P) - 1.0 (P)	t=7.0	ι=7.0	L-7.0	L-7.0	38	81							
	- 20 -		_ 1.0 (1)		27	98										
	- 25 -		- _ 0.75 (P) -	0.56 t=10.0	28 29	97 90	45	14	31				Soft to medium gray SILTY CLAY (CL)			
	-30-		- 1.25 (P)		22	101	-	1								
	- 35 -		3.0 (P)	2.18 t=14.0	23 24	104 99	51	16	35				Stiff tan and gray CLAY (CH) w/ sand			
	40-		-		33	95							Continued Next Page			
Ground Water Level Data Boring Advancement Method									No							
<u> </u>	Locati	on:	vation at Ga = 0.50' pth at Borel	0 to 4" D	4" Nom. Dia. Short Flight Auger: 0 to 6 ft. 4" Dia. Rotary Wash: 6 to 60 ft.						t: Unconsolidated, Undrained Triaxial Compression Test Lateral Pressure = psi GSS: Particle Size Analysis Confidential Information.					

Boring Abandonment Method

Borehole grouted with cement/ bentonite upon completion

0.33

LOG OF SOIL BORING B-10



File: Date: 12-80-3741

Date: 10/2/12 Logged by: B. Singleton

Driller:

D. Tyler

CPRA Baton Rouge, LA Sheet 2 of 2

Baton Rouge Geotechnical Laboratory

AASHTO Accredited Laboratory, LELAP Certificate No. 02052,

LISACE Validated

Rig:

Airboat

						V.011107		l	JSACE	Valida	ted		Leasting Let 200 46120 0			
l	FIELD DATA				L/	ABOR	ATO	RY D	ATA	1		9	Location: Lat. 29° 46' 39.9" Long. 93° 24' 27.9"			
Ground	Depti	ples	Field	Compressive Strength (tsf)	Water	Dry Unit Weight	Atter	berg L	imits.	cent ising Sieve	Other	Soil Type	Surface Elevation: 0.17 (ft., NAVD)			
Ground Water Level	(feet)	San	Test Results	Comp Stre (t	Content (%)	Weight (pcf)	LL	PL	PI	Per Pas #200		os	Description			
30		-X	25 b/f _ 5-13-12		12					18			Medium dense brown and gray CLAYEY SAND (SC)			
	-45	-X	-		23					59			Stiff brown and gray SANDY CLAY (CL)			
	- 50	Sec. 10	2.0 (P)		26								Stiff brown and gray CLAY (CH) w/ silt layers			
			-	1.42	52	70							our provincing gray of the (orly in our layers			
	- 55		0.75 (P)	t=22.0	43	73	73	21	52							
15			- - 1.5 (P)	1.55 t=24.0	1	85	57	19	38							
	- 60				_ 39	_77				 -			Boring completed at 60 ft.			
i i	- 65	-														
	- 70								1							
		1														
8	- 75															
<u></u>																
	⊥ ₈₀ .	L			Ь	<u> </u>	L	<u> </u>	<u></u>	<u></u>	Not	<u> </u>				
_ [Water Locat	Ele	vation at Ga 0.50'	auge	4" N 0 to 4" D	Boring Advancement Method 4" Nom. Dia. Short Flight Auger: 0 to 6 ft. 4" Dia. Rotary Wash: 6 to 60 ft.							nsolidated, Undrained Triaxial Compression Test Pressure = psi			
	Water 0.33'	Dе	pth at Boreh	10le =	Bore	Boring Abandonment Method Borehole grouted with cement/ bentonite upon completion							Confidential Information: Privileged & Contidential Work Product			
								,			Strata Boundaries May Not Be Ex					

LOG OF SOIL BORING B-11



File:

12-80-3741

Date:

10/4/12 Logged by: B. Singleton

Driller:

D. Tyler

CPRA Baton Rouge, LA Sheet 1 of 1

Baton Rouge Geotechnical Laboratory
AASHTO Accredited Laboratory, LELAP Certificate No. 02052,
USACE Validated

Rig:

Airboat

Strata Boundaries May Not Be Exact

								_	Validat	led		Location: Lat. 29° 46' 22.6"		
F	FIELD	DATA		<u>L/</u>	ABOR						e e	Long. 93° 24' 35.6"		
Ground Water Level	Depth (feet)	Field Test Results	Compressive Strength (tsf)	Water Content (%)	Dry Unit Weight (pcf)		berg L PL	imits PI	Percent Passing #200 Sieve	Other	Soil Type	Surface Elevation: 0.45 (ft., NAVD) Description		
<u>Z</u>		0.0 (P)	ŏ	55	62							Very soft gray CLAY (CH) w/ silt and sand layers		
		0.0 (P) 0.0 (P)		61 77	64	93	25	68	77			w/ organics at 0-4 feet		
	- 5 -	0.0 (P)	0.12 t=3.0	62 70 83 80	58 51 53	92	24	68						
	-10-	0.0 (P) 0.0 (P)	0.15	77	56 53	95	27	68						
		0.0 (P)	t=5.0	82	52		-							
	- 15-	0.25 (P)	0.12 t=6.0	61	64	74	22	52			2000	Medium gray SILTY CLAY (CL) w/ sand		
		_ 1.5 (P) - _ 1.0 (P)	0.78 t=8.0	22 30	94 105	44	15	29				Medium gray SILTY CLAY (CL) W/ Sailu		
	- 25 -	0.5 (P)		24	91				22	GSH	1	Loose gray CLAYEY SAND (SC)		
	-30-	5 b/f 1-4		23	98				6			Loose tan and gray SAND (SP-SC) w/ clay		
	- 35 -	_ 0.5 (P)		20	92							Stiff gray SILTY CLAY (CL)		
	40-	_ 2.25 (P)	1.21 t=16.0		89 85	47	20	27						
		Water Level D	ata	T	Boring /	Advanc	emen	Meth	od		otes	Boring completed at 40 ft		
	Locatio Water [Elevation at G n = 0.70' Depth at Bore	0 to	4" Nom. Dia. Short Flight Auger: 0 to 6 ft. 4" Dia. Rotary Wash: 6 to 40 ft.							t: Unconsolidated, Undrained Triaxial Compression Test Lateral Pressure = psi GSH: Hydrometer Particle Size Analysis			
1	0.25'			Boring Abandonment Method							Confidential Information: Privileged & Confidential			
				Bor	rehole g ntonite (route upon c	d with compl	cem etion	ent/			Work Product		

LOG OF SOIL BORING B-12



File:

12-80-3741

Date:

10/8/12

Logged by: B. Singleton

Driller:

D. Tyler

Airboat

CPRA Baton Rouge, LA Sheet 1 of 2

Baton Rouge Geotechnical Laboratory
AASHTO Accredited Laboratory, LELAP Certificate No. 02052,
USACE Validated

Rig:

	CICI F		ΑΤΛ		- 1	NBOB/	\TO!			Valida	ted		Location: Lat. 29° 46' 29.7"			
	FIELD DATA		9		ABORA	ATORY DATA Atterberg Limits					be.	Long. 93° 24' 4.3"				
Ground Water Level	Depth	poles	Field	ressi angth	Water	Dry Unit		berg L	.iiiiita	cent ssing Siev	Other	Soil Type	Surface Elevation: -0.17 (ft., NAVD)			
Water Level	(feet)	San	Test Results	Compressive Strength (tsf)	Content (%)	Weight (pcf)	LL	PL	PI	Per Pas #200		ဖြ	Description			
<u>-14</u> -			0.0 (P)										Very soft gray CLAY (CH)			
		H	0.0 (P)	0.19	77 87	56 53	83	27	56			///,				
		ı	_ 0.0 (1)	t=2.0	83	50	00	~'								
	- 5 -		0.0 (P)													
	-		0.0 (P)	0.22	90 79	50 57	95	25	70							
			-	t=3.0 0.08	71	56			-							
			0.0 (P)	t=4.0	93 90	49 44	102	28	74		ORG,					
	-10-	H	0.0 (P)		90	44										
		1	-	0.16	90	51				ļ						
	-		_ 0.0 (P)	t=6.0	76 77	57 56	82	22	60				w/ sand layers at 12-14 feet			
	-15-		1.25 (P)	0.20 t=6.0	32	91	32	15	17				Very soft tan and gray SILTY CLAY (CL)			
			_ 1.25 (P)		36 40	84										
		ı	-		26	101										
			2.75 (P)	1.92 t=8.0	26 22	106	55	13	42		ORG		Stiff tan and gray CLAY (CH) w/ silty sand layers			
	- 20 -	H	_		22	104					-					
		11									ļ					
			-													
	-		_ 3.0 (P)		28	90										
	- 25 -	П	-													
		$\left\{ \right\}$				1			•							
		Ť.	- _ 1.75 (P)	1.36	27	99	59	17	42	88						
	-30-			t=12.0	29 30	89	36	21	15	99			Stiff tan and gray SILTY CLAY (CL)			
		$\ $			30											
		Ц	_				1				ļ					
	ļ		2.25 (P)		34	86										
	-35-	ſ	-		34	00										
	<u> </u>	-														
<u> </u>	<u> </u>		75 /0\	1.14		79	90	29	61	 			Stiff tan and gray CLAY (CH) w/ silt layers			
	40-		2.75 (P)	t=16.0		19	30	79	01		<u></u>		Continued Next Page			
	Ground Water Level Data Boring Advancement Method								No t:		nsolidated, Undrained Triaxial Compression Test					
	4" Nom. Dia. Short Flight Auger: 0 to 6 ft. 4" Dia. Rotary Wash:								La	Lateral Pressure = psi						
$\bar{\Delta}$	Locati	on	= 0.66'	_		60 ft.	y vva	sil.			ORG, = 2.6% ORG ₂ = 2.6%					
	Water 0.83'	De	pth at Boreh	nole =							Confidential Information: Privileged & Confidential					
							outed with cement/						Work Product			
						bentonite upon completion						Objects Described Mars Not 25 Free L				
L											1		Strata Boundaries May Not Be Exact			

LOG OF SOIL BORING B-12



File:

12-80-3741

Date: 10/8/12 Logged by: B. Singleton

Driller: D. Tyler

CPRA Baton Rouge, LA Sheet 2 of 2

Baton Rouge Geotechnical Laboratory
AASHTO Accredited Laboratory, LELAP Certificate No. 02052,
USACE Validated

Rig:

Airboat

Strata Boundaries May Not Be Exact

										Valida	ted	1	Location: Lat. 29° 46' 29.7"
	FIELD	0	ATA		<u>L/</u>	ABORA						e l	Lorg. 93° 24' 4.3"
	<u> </u>	68	5 1 - 1 - 1	ssive gth	l		Atter	berg L	imits	ent ing ieve		Soil Type	Surface Elevation: -0.17 (ft., NAVD)
Ground Water Level	(feet)	Samp	Field Test Results	Compressive Strength (tsf)	Water Content (%)	Dry Unit Weight (pcf)	LL	PL	PI	Perc Pass #200 S	Other	Soi	Description
		⇈			39	80							Stiff tan and gray CLAY (CH) w/ silt layers
]									Ì		
		H	- 1.25 (P)	1.92 t=18.0	33	89	54	21	33		! 		
	-45-		. 1.25 (P) - -	[-10.0	37	85					ļ		
	45	┨		İ		Ì					Į		
		11		1.48		ļ							
		30	- _ 0.75 (P)	t=20.0		76	85	25	60	99			
	- 50 -	H	-		43	81					ł		
		1			Ì								
			_	1.99	43	78	69	22	47				
			1.25 (P)	t=22.0	31	85			''		1		
	- 55 -	П	_		"		l.		Ì				
	ļ	4											
	-		-	}									
	- 60 -		0.5 (P)		45	76	<u> </u>	ļ		ļ			Daving appleted at 60 ft
	-	4	ı										Boring completed at 60 ft.
		1											r
	-	-								Ì		1	
	-65	1									1		
		7											
		+											
	-70										1		
		$\frac{1}{2}$											
		1											
]								Ì			
	- 75	+											
						ļ.							
		-		i				ŀ					
		1											
		nd V	Vater Level D	ata		Boring						otes	It had the desired Triming Commencing Trade
-	Water Locati	Ele	evation at G = 0.66'	auge	0 to	Nom. Dia 6 ft. Dia. Rota 60 ft.			nt Aug	er:	t: L:	Unc atera	onsolidated, Undrained Triaxial Compression Test I Pressure = psi
1	Water 0.83'	De	pth at Bore	hole =									Confidential Information: Privileged & Confidential
	2.20					Boring /					7		Work Product
4					I Bo	rahala c	ıraııta	d with	1 cem	ent/			

Borehole grouted with cement/ bentonite upon completion

LOG OF SOIL BORING B-13



File: 12-80-3741 Date: 10/9/12 Logged by: B. Singleton

Airboat

Driller: D. Tyler

CPRA Baton Rouge, LA

Sheet 1 of 1 Baton Rouge Geotechnical Laboratory AASHTO Accredited Laboratory, LELAP Certificate No. 02052, USACE Validated

Location: Lat. 29° 46' 9.3"

Rig:

F	IELD	DATA			L/	ABORA	ATOF		_	Validat			Location: Lat. 29° 46' 9.3" Long. 93° 23' 56.5"
		ss.	-	sive			Atter	berg L	imits	nt ig eve		Jype	Surface Elevation: -0.05 (ft., NAVD)
Ground Water Level	Depth (feet)	Fi To Res	eld est sults	Compressive Strength (tsf)	Water Content (%)	Dry Unit Weight (pcf)	LL	PL	PI	Percent Passing #200 Sieve	Other	Soil Type	Description
		0.0	(P)				90	25	65				Very soft gray CLAY (CH)
		0.0		0.09	74 80	56 55	107	24	83				
		- 0.0	(٢)	t=2.0	79	49	101	_4					
	- 5 -	0.0	(P)		70 105								
		0.0	(P)	0.06	88 95	48 48	104	23	81				with shells at 6-8 feet
1		L		t=3.0	90	46	1		i.				
		0.0	(P)		57	63			 				
	-10-	0.0	(P)	0.08 t=5.0	80	53	105	25	80				
		F	(D)	1-0.0	80	51							
	<u> </u>	0.0	(P)		88	52							
	-15-	0.0	(P)	0.07 t=6.0	92	49	105	26	79				
1		0.0	(P)	!	81	51							
				0.09	83	56							
		1.2	5 (P)	t=8.0	42 48	78 76	52	15	37				with sheils at 18-20 feet
	- 20 -				10	'			1			188	Medium to stiff tan and gray SILTY CLAY (CL)
1		P											
		- 4.0	(D)	1.70 t=10.0	22	103	46	13	33	84			with sand at 23-30 feet
	- 25 -	1.0	(P)		20	108		ļ					
	-					İ							
8				0.83	00	92	24	46	40	96			
		2.0	(P)	t=12.0	ຸວບ	91	34 55	16 22	18 33		ORG	3,	Medium to stiff tan and gray CLAY (CH) w/ silt
S8	-30-				31	3'							layers
1					3								
1		F	·= (D)										
	-35-	2.2	5 (P)		30	89							
_		{											
8/8/13		╙		2.52		-							Very stiff tan and gray CLAY (CH)
3	-	2.7	5 (P)	t=16.0		87 84	77	28	49				
ARD LOGOT OTR 12-80-3/41 GPJ LOGOTH GPJ 80873	L 40-	Water	Level Da	ıta	1	Boring A	dvano	emen	t Meth	od		otes	Boring completed at 40 ft.
2						lom. Dia							onsolidated, Undrained Triaxial Compression Test Pressure = psi
<u> </u>			on at Ga	auge	4" [6 ft. Dia. Rota	ry Wa	sh:					= 2.5%
200 000 000 000 000 000 000 000 000 000	Water	on = 0.7 Depth a	ս [.] ıt Borel	nole =	6 10	40 ft.							Confidential Information:
25 25	0.75'					Boring A	bando	nmen	t Meth	od	\exists		Privileged & Confidential Work Product
0000						ehole g				ent/			VVOIK FIDUUGE
RO L					Del	tG	٠,٠٠١ د	p1	J., (7)				Strata Boundaries May Not Be Exact

LOG OF SOIL BORING B-14



Date: 10/10/12 Logged by: B. Singleton

12-80-3741

Airboat

Driller: D. Tyler

Sheet 1 of 1

CPRA Baton Rouge, LA Baton Rouge Geotechnical Laboratory
AASHTO Accredited Laboratory , LELAP Certificate No. 02052,
USACE Validated

Rig:

File:

	FIELD		ΔΤΛ		1 /	ABORA	\TOE			Validat	led		Location: Lat. 29° 46' 23.3"
		П	<u> </u>	9				berg L				be/	Long. 93° 23' 37.7"
Ground	Depth	saldi	Field	ressi ingth sf)	Water	Dry Unit	Atten	Del g L	.iiiiis	cent sing Siev	Other	Soil Type	Surface Elevation: 0.20 (ft., NAVD)
Ground Water Level	(feet)	San	Test Results	Compressive Strength (tsf)	Content (%)	Weight (pcf)	LL	PL	PI	Per Pas #200	Other	တိ	Description
= 1		200	0.25 (P)	Ů									Very soft gray CLAY (CH)
				0.06	79	53			۱		000		
	<u> </u>	H	0.25 (P)	t=2.0	63	60 58	108	34	74	99	GSS		
			0.0 (P)	0.04	69 91	48	107	27	80		ORG.		
	- 5 -	H	_ 0.0 (1)	t=2.0	76	52							
			0.0 (P)		94								
			• •	0.04	57 75	55							
			0.0 (P)	t=4.0	70	59	94	22	72				
	-10-	H	0.0 (P)		77 67	49							
			-		93	56			ļ		i		
		۱	0.0 (P)	0.06 t=6.0	80 88	51	98	28	70				
			- -	1-0.0	85	47							
	15-		_ 0.0 (P)										
	-	H	0.0 (P)	0.20	86	55	82	25	57				
	-		_ 0.0 (1)	t=7.0	80	51				ļ			
			0.0 (P)	0.22 t=8.0	39	85	38	18	20				Very soft gray SILTY CLAY (CL) w/ trace sand
	- 20 -	Щ			40	72	<u> </u>					2000	
		$\ \ $											Very soft gray CLAY (CH)
	-	$\ $							Ì				
		H	0.25 (P)	0.39 t=10.0	69	57	95	21	74				
	- 25 -			1-10.0	71	55	<u>L</u> _		ļ	ļ	ļ		
		$\{ \ $											Very soft gray SILTY CLAY (CL) w/ trace organics
		$\ \ $		Ì]				l	388	
		Ħ	0.0 (P)		69			Ì					
	-30-		-	<u> </u>	41 55	62	<u> </u>			ļ	ļ	100	
	50	$\ \ $								1			Stiff gray SILTY CLAY (CL) w/ trace sand
	<u> </u>	$\ \cdot \ $						1					
	<u> </u>		- - 4 5 (D)	1.35		00	40	20	29	92			
	35-		1.5 (P) 2.5 (P)	t=14.0		98 95	49	20	29	<u> </u>	<u> </u>	388	
		41								1			Stiff brown and gray CLAY (CH) w/ silt layers
		$\{ \ \ $											
	 		-	1.39 t=16.0	39	84	78	24	54				
	L ₄₀ -		-	1-10.0	31	86		<u> </u>					
		d W	ater Level Da	ta	_	Boring A	dvanc	ement	Meth	od		tes	Boring completed at 40 ft
						lom. Dia. 6 ft.	Short	Fligh	t Auge	er:			nsolidated, Undrained Triaxial Compression Test Pressure = psi
			vation at Ga	auge	4" D	ia. Rotai	ry Was	sh:			GS	SS: F	Particle Size Analysis
_			= 0.70¹ pth at Borel	nole =	6 to	40 ft.					0	τG ₁ =	5.4%
	0.50'					Boring A	banda	nmor	Moth	nd	4		Confidential Information:
						ehole gi					1		Privileged & Confidential Work Product
						tonite u							
													Strata Boundaries May Not Be Exa

LOG OF SOIL BORING B-15



File: 12-80-3741

Date: 10/9/12

Logged by: B. Singleton

Airboat

Strata Boundaries May Not Be Exact

Driller: D. Tyler

CPRA Baton Rouge, LA Sheet 1 of 2

Baton Rouge Geotechnical Laboratory

AASHTO Accredited Laboratory, LELAP Certificate No. 02052,

USACE Validated

Rig:

										Valida	led		Location: Lat. 29° 46' 27.4"
	FIELD	DATA			L/	ABORA						e e	Long. 93° 23' 40.8"
Cd	Donth	sala Fiel		assive gth	Water	Doy I Init	Atter	berg L	imits	ent sing Sieve	Other	Soil Type	Surface Elevation: -0.38 (ft., NAVD)
Ground Water Level	(feet)	Tes Resu	st ¦	Compressive Strength (tsf)	Content (%)	Dry Unit Weight (pcf)	LL	PL			Other		Description
		0.0 (F	(د	0.17 t=1.0	79	54	105	30	75		ORG₁		Very soft gray CLAY (CH) w/ organics
		0.0 (F	ا (ح		83	55							
		- 0.5 (1	′	0.08	103	44							
	- 5 -	0.0 (F	P)	t=2.0	86 92	49 46	111	31	80	!	ORG ₂		
ļ		0.0 (F	P)	0.16	61	65	72	19	53		ORG:		
				t=3.0 0.17	80	52					ļ		
		0.25	(P)	t=4.0	87	52	102	24	78				
	-10-	0.0 (P)		89								
		.		0.17	74 81	52		05	0.5	00			
	-	0.0 (I	P)	t=6.0	92 74	50 50	90	25	65	98			
	-15-	0.0 (1	P)	0.13 t=6.0	97	49	95	24	71	l			
	- 13-	0.0 (1	D)	1-0.0	80 68	50			}				
		• • • • •	' '		36	70							
		1.5 (P)	0.11 t=8.0	52 40	79	56	17	39	75	GSS		w/ sand at 18-20 feet
	- 20 -			-	36	80	-	 	┼	-			Stiff gray CLAY (CH) w/ sand
		11					ŀ				ļ		oun gray out (erry mount
		╙		1.07	22	104	54	15	39	77			
	ļ	3.25	(P)	t=10.0	21	105	54			''	1		
	- 25 -	Ī			-								
		1											
		 	D \							99			
	-30-	1.0 (P)		29	88					ļ		
		-		Ì									
		┧╽		1.08		<u> </u>		<u> </u>					
		2.0 ((P)	t=14.0	0 31		59	23	36		ORG	4	Stiff tan and gray CLAY (CH) w/ silt layers
ļ	-35-				29	86							
		1											
		₩			1								
	10	2.25	(P)		38	80				7.55			
	-1-40- Groun	d Water Le	vel Da	ita		Boring /	Advanc	emen	t Meth	od		tes	Continued Next Page
						Nom. Dia	. Shor	t Fligh	t Aug	er:	La	iteral	onsolidated, Undrained Triaxial Compression Test Pressure = psi
$\bar{\Delta}$		Elevation on = 0.70		auge	4" [Dia. Rota 60 ft.	ıry Wa	sh:					Particle Size Analysis : 12.4%
	Water	Depth at		nole =	610	ou II.					0	RG2 =	8,0% 3.3% Confidential Information:
	1.08'					Boring /	Abando	onmen	t Meth	od			:1.5% Privileged & Confidential
Σ						rehole g ntonite (ent/			Work Product
					Dei	.come (۰،۱۰۰۰ د	- J. 11P1	55.011				Strata Boundaries May Not Be Exac

LOG OF SOIL BORING B-15



Date: 10/9/12 Logged by: B. Singleton Driller: D. Tyler

12-80-3741

Airboat

Strata Boundaries May Not Be Exact

Sheet 2 of 2

CPRA Baton Rouge, LA Baton Rouge Geotechnical Laboratory
AASHTO Accredited Laboratory, LELAP Certificate No. 02052,
USACE Validated

Rig:

File:

Dato		90				.Adilio		L		Valida	ed		Location: Lat. 29° 46' 27.4"
	FIELD	ם (ATA		L/	BOR	ATO	RY D	ATA			9	Location: Lat. 29 46 27.4 Long. 93° 23' 40.8"
	L	68	5 1.1.1	ssive gth		D 1 124		berg L	imits	ent ing ieve		Soil Type	Surface Elevation: -0.38 (ft., NAVD)
Ground Water Level	(feet)	Samp	Field Test Results	Compressive Strength (tsf)	Water Content (%)	Dry Unit Weight (pcf)	LL	PL	PI	Perc Pass #200 \$	Other	Soi	Description
		I											Stiff tan and gray CLAY (CH) w/ silt layers
		$\ \cdot\ $								<u>'</u>			
	-	Ħ	1.0 (P)	1.63 t=18.0	47	79	90	26	64				
	-45-		• •		26 39	82		1					
	ļ.,	┨╏		1									
		$\ \ $		1							ļ		
			1.75 (P)								ļ		
	-50	H	-		32	92				1	1		
		d											
		Ц	_	1.60	ļ								
			1.0 (P)	t=22.0	35 38	87 84	57	20	37		ļ		
	-55		-					İ					
]											
		Н	-			ļ							
	-60		1.0 (P)		44	81		<u> </u>		<u></u>			
	- 60	1											Boring completed at 60 ft.
	-	+									ļ		
		1									ļ		
	-65	4						ļ					
	-	\dashv				1							
		1								1			
		4											
•	70	\dashv	}	1									
		4											
	 	1									1		
	- 75]									ļ		
	-	\dashv											
	-	1			İ						1		
		1	<u></u>		<u> </u>						L		
	Grou	nd V	Vater Level D	ata	40.3	Boring .					No t:	otes Unc	onsolidated, Undrained Triaxial Compression Test
				.	0 to	Nom. Dia		_	it Aug	CI.	La	atera	I Pressure = psi
Δ	Locat	ion	evation at G = 0.70'		4" [6 to	Dia. Rota 60 ft.	ary Wa	isn:					
2	Water 1.08'	. De	epth at Bore	ehole =									Confidential Information:
					_	Boring					7		Privileged & Committeenties! Work (Product)
2					pe	rehole g ntonite	groute upon	comp	letion	HILL			
					1						1		Strata Boundaries May Not Be Exac

LOG OF SOIL BORING B-16



Date: 10/10/12
Logged by: B. Singleton
Driller: D. Tyler

12-80-3741

Airboat

Strata Boundaries May Not Be Exact

Sheet 1 of 1

CPRA Baton Rouge, LA Baton Rouge Geotechnical Laboratory
AASHTO Accredited Laboratory, LELAP Certificate No. 02052,
USACE Validated

Rig:

File:

	FIELD	DATA	1	L/	ABORA	ATOR						Location: Lat. 29° 46' 41.7" Long. 93° 23' 31.4"
		s a	ssive			Attert	erg Li	mits	ng eve		Soil Type	Surface Elevation: -0.13 (ft., NAVD)
Ground Water Level	Depth (feet)	Field Test Results	Compressive Strength (tsf)	Water Content (%)	Dry Unit Weight (pcf)	LL	PL	ΡI	Perce Passi #200 S	Other	Soil	Description
<u> </u>		_ 0.0 (P)										Very soft gray CLAY (CH) w/ trace organics
		0.0 (P)	0.21 t=2.0	105 91 97	47 49 45	119	29	90		ORG₁		
	- 5 -	0.0 (P)	0.05 t=2.0	118	41	118	26	92	1			w/ shells at 4-8 feet
		0.0 (P)		116 90 90	53					E		
	10	0.0 (P)	0.11 t=4.0	89	50	100	25	75	67			w/ sand pockets at 9-10 feet
	-10-	0.0 (P)		94	49			<u>'</u>				
		0.0 (P)	0.10 t=6.0	80	55	79	22	57				
	15-	0.0 (P)		78	56							
		1.5 (P)	0.93 t=7.0	26	98	34	13	21				Medium gray SILTY CLAY (CL)
	-20-	1.0 (P)	0.73 t=8.0	33	89	57	15	42				Medium gray CLAY (CH) w/ silt
		- - -										
	- 25 -	2.25 (P)	1.68 t=10.0	24 24	99 99	44	17	27	88	ORG	2	Stiff gray SILTY CLAY (CL) w/ sand layers
		1.25 (P)										
	-30		2,35									Very stiff tan and gray CLAY (CH) w/ silt layers
3	- 35	2.0 (P)	t=14.0		88	67	25	42	100			
	40	2.25 (P)		41	78							Boring completed at 40 ft
	Groun	d Water Level	Data	4" 1	Boring A				•	No t:	Unc	onsolidated, Undrained Triaxial Compression Test
⊻	Locati	Elevation at o	_	0 to	Nom. Dia o 6 ft. Dia. Rota o 40 ft.		_	ı Auge	51.	La	ateral RG₁ =	: 10.1% - 1.7%
2	Water 0.83'	Depth at Bor	enole =		Boring	Abondo	nmen	t Math	od	_		Confidential Information: Privileged & Confidential
<u> </u>				Bo bei	rehole g ntonite	route	d with	cem				Work Product

LOG OF SOIL BORING B-17



 File:
 12-80-3741

 Date:
 10/5/12

 Logged by:
 B. Singleton

Driller: D. Tyler

Airboat

CPRA Baton Rouge, LA Sheet 1 of 2

Baton Rouge Geotechnical Laboratory

AASHTO Accredited Laboratory, LELAP Certificate No. 02052,

USACE Validated

Rig:

F	IELD	DATA		L/	BOR	ATOF		ATA	Valida			Location: Lat. 29° 47' 12.5" Long. 93° 23' 41.6"
	9	2	ssive			Atter	berg L	imits	ent ing ieve		Soil Type	Surface Elevation: -0.68 (ft., NAVD)
Ground Water Level	Depth (feet)	Field Test Results	Compressive Strength (tsf)	Water Content (%)	Dry Unit Weight (pcf)	LL	PL	PI	Percent Passing #200 Sieve	Other	Soil	Description
_		0.0 (P)	0.12 t=1.0	91	50	75	22	53	}			Very soft to soft gray CLAY (CH)
		0.0 (P)	0.05 t=2.0	124	38	119	29	90	99			
	- 5 -	0.0 (P)		81	52							
		0.0 (P)	0.09 t=3.0	84	54	62	20	42				
	\vdash	_ 0.0 (P)	t-0.0	69				ļ		!		
	-10-	ļ:		57 63	64							
	\vdash	0.0 (P)	0.28 t=5.0	102	48	96	23	73	ļ			
		0.0 (P)										
		F		92	49					ļ		
	-15-	0.5 (P)	0.13 t=6.0	92	50	94	23	71				
		2.5 (P)	1.01	25	103	48	16	32				Stiff gray SILTY CLAY (CL)
	\vdash	-	t=7.0			l	l					
	20	2.25 (P)				45	14	31				
		2.0 (P)							95			w/ sand and silt layers at 23-30 feet
	- 25 -				ļ							
		ļ										
		0.75 (D)			1	38	16	22				
		0.75 (P)		29	86	36	'0	22				
	-30-											Medium to stiff tan and gray CLAY (CH) w/ silt layers
												layers
		2.75 (P)		34					in the second			
	-35-	- \ \	1	33	84							
				1								
			1.32				1					
		1.75 (P)	t=16.0	37	83	72	27	45	0	ORC	j1	
	Ground	Water Level Da	ıta	1	Boring /	Advanc	emen	t Meth	od	No.	otes	Continued Next Page
	Water E Locatio	levation at Ga n = 0.65'	auge	0 to 4" E	lom. Dia 6 ft. Dia. Rota 60 ft.	. Shor	t Fligh			t:	Unce	onsolidated, Undrained Triaxial Compression Test I Pressure = psi = 3.0%
	Water [1.33'	Depth at Borel	nole =									Confidential Information:
				Bor	Boring /	route	d with	ı cem		-		Privileged & Confidential Work Product
				Der	tonite i	ibon c	ompi	GUUII				Strata Boundaries May Not Be Exa

LOG OF SOIL BORING B-17



Date: 10/5/12
Logged by: B. Singleton
Driller: D. Tyler

12-80-3741

Airboat

Sheet 2 of 2

CPRA Baton Rouge, LA

Baton Rouge Geotechnical Laboratory
AASHTO Accredited Laboratory, LELAP Certificate No. 02052,
USACE Validated

l contion: | at 20° 47' 12 5"

File:

Rig:

F	IELD	D	ATA		L/	ABOR/	TOF	_	ATA	Validat			Location: Lat. 29° 47' 12.5" Long. 93° 23' 41.6"
	0	les	Field	ssive gth n	Water	Dry Unit	Atter	berg L	imits	ent sing Sieve	Other	Soil Type	Surface Elevation: -0.68 (ft., NAVD)
Ground I Water Level	(feet)	Samp	Test Results	Compressive Strength (tsf)	Content (%)	Weight (pcf)	LL	PL	PI	Perc Pass #200	Other	Soi	Description
	- 45 -		1.0 (P)		54	65							Medium to stiff tan and gray CLAY (CH) w/ silt layers
				1.37 t=20.0	43	75	l I						
	- 50 -	100	0.75 (P) -	1-20.0	41	76							
	- 55 -	Section 2	- _ 1.0 (P) -		35	80							
		3 1 1	_ _ 1.0 (P)	0.98 t=24.0	38	83	68	24	44				
	- 60 -	Π				†- <u>'-</u> '-		† 		†			Boring completed at 60 ft.
		1											
		1						ļ					
,	- 65	1											
		1											
	- 70 -					ļ							
	[/o	-										i,	
		1										ļ	
	75												
	-	1											
5		-											
		1					<u> </u>	<u>L</u> .					
		nd V	Vater Level D	ata	A" I	Boring A					t:	otes Unc	onsolidated, Undrained Triaxial Compression Test
	Locati Water	on	evation at G = 0.65' epth at Bore		0 to	o 6 ft. Dia. Rota 60 ft.			Aug	J.	L	atera	I Pressure = psi Confidential Information:
	1.33'					Boring					\dashv		Privileged & Confidential Work Product
					Bo be	rehole g ntonite (pon (a with compl	n cem letion	env			Strata Boundaries May Not Be Exac

LOG OF SOIL BORING B-18



File: Date: 12-80-3741

10/4/12

Privileged & Confidential

Work Product

Strata Boundaries May Not Be Exact

Logged by: M. Henderson **Driller:**

D. Anthony

Ardco K-1000

CPRA Baton Rouge, LA Sheet 1 of 2

Baton Rouge Geotechnical Laboratory
AASHTO Accredited Laboratory, LELAP Certificate No. 02052,
USACE Validated

Rig:

Location: Lat. 29° 46' 5.5"

Ī	FIELD) [ATA		L/	ABORA	TOF	RY DA	AŢA				Location: Lat. 29° 46° 5.5° Long. 93° 24' 24.1"
		68		ssive				oerg Li	mits	ent ing ieve		Soil Type	Surface Elevation: N/A (ft., NAVD)
Ground Water Level	Depth (feet)	Samp	Field Test Results	Compressive Strength (tsf)	Water Content (%)	Dry Unit Weight (pcf)	LL	PL	PI	Percent Passing #200 Sieve		<u>.</u>	Description
			_ 0.5 (P) -		10 22	112				33	GSH		Loose gray CLAYEY SAND (SC) w/ shells and gravel
		Service State	0.5 (P)	0	16 20	80				7	GSH		Loose tan and gray SAND (SP-SC) w/ clay and shells
	- 5 -		0.0 (P)			[1			! 		
		1000	_ 0.0 (P)		10	101							
<u></u>			0.0 (P)										
<u>v</u> .	10	190	0.0 (P)							16	GSH		Loose to medium dense brown and gray CLAYEY SAND (SC) w/ silt
			0.5 (P)		23	97							
	-15		0.5 (P)							36	GSH		w/ trace shell fragments 10 to 16 ft.
			0.5 (P)		40 41 25	83							-w, trace shering ments to to to the
	_		0.5 (P)		33	90							
	-20		<u> </u>		19	109							
			4.0 (P)	2.00 t=10.0	21	109	33	17	16	20			
	- 25												
			0.5 (P)							23	GSI	1	
	-30		5.5 (.)		28	88		-			 		Stiff gray SILTY CLAY (CL) w/ sand layers
		-		1.03			40	47	00				
	25		1.0 (P)	t=14.		89 84	46	17	29	80			
	-35	\dashv											Stiff tan SILTY CLAY (CL) w/ silt layers
			-										
L	<u></u>		2.0 (P)		29	90	<u> </u>	<u></u>	<u> </u>			22	Continued Next Page
			Water Level D	ata		Boring	Advan	cemen	l Meth	od	N-	otes	
∇			ter first enc		0 to	Nom. Dia o 6 ft. Dia. Rota o 60 ft.			it Aug	er:	11:	atera	onsolidated, Undrained Triaxial Compression Test al Pressure = psi Hydrometer Particle Size Analysis
					10								Confidential Information.

Boring Abandonment Method

Borehole grouted with cement/ bentonite upon completion

CPRA

Baton Rouge, LA

LOG OF SOIL BORING B-18



Sheet 2 of 2

Baton Rouge Geotechnical Laboratory
AASHTO Accredited Laboratory, LELAP Certificate No. 02052,

File:

12-80-3741

Date: 10/4/12

Driller:

Logged by: M. Henderson D. Anthony

Rig:

Ardco K-1000

FIELD DATA LABORATORY DATA LOcation: Lat. 29° 46' 5.5" Long. 93° 24' 24.1"	1
50.1g. 55 17 17 17 18 18 18 18 18 18 18 18 18 18 18 18 18	
Atterberg Limits E B S Surface Elevation: N/A (ft., NA	VD)
Ground Depth Ground (feet) Test Level Results Results Ground (feet) Results Ground (feet) Results Ground (feet) Content	
Stiff gray CLAY (CH)	
1.70 t=18.0 45 75 90 26 64	
1.0 (P) t=18.0 43 71	
1.0 (P)w/ shells	
50 41 76	
1.76 36 85 57 20 37	8
1 15 (P) t=22.0 30 30 31 25 31	
55 - 37 81	
1.5 (P)	
1.5 (P)	
Boring completed at 60 ft.	
-65-	
70-	
-75-	
1,000	
80 Ground Water Level Data Boring Advancement Method Notes to Unpage olidated Undrained Triaxial	
A" Nom Dia Short Flight Auger L. Uniconsolitated, Orlandined Trianian	Compression Test
6 to 60 ft.	
© Confidential In Boring Abandonment Method Privileged & Co	
Borehole grouted with cement/ Work Pro	
bentonite upon completion Strata Bounda	ries May Not Be Exac

LOG OF SOIL BORING B-19



File:

12-80-3741

Date: 10/4/12

Logged by: M. Henderson

Driller:

D. Anthony

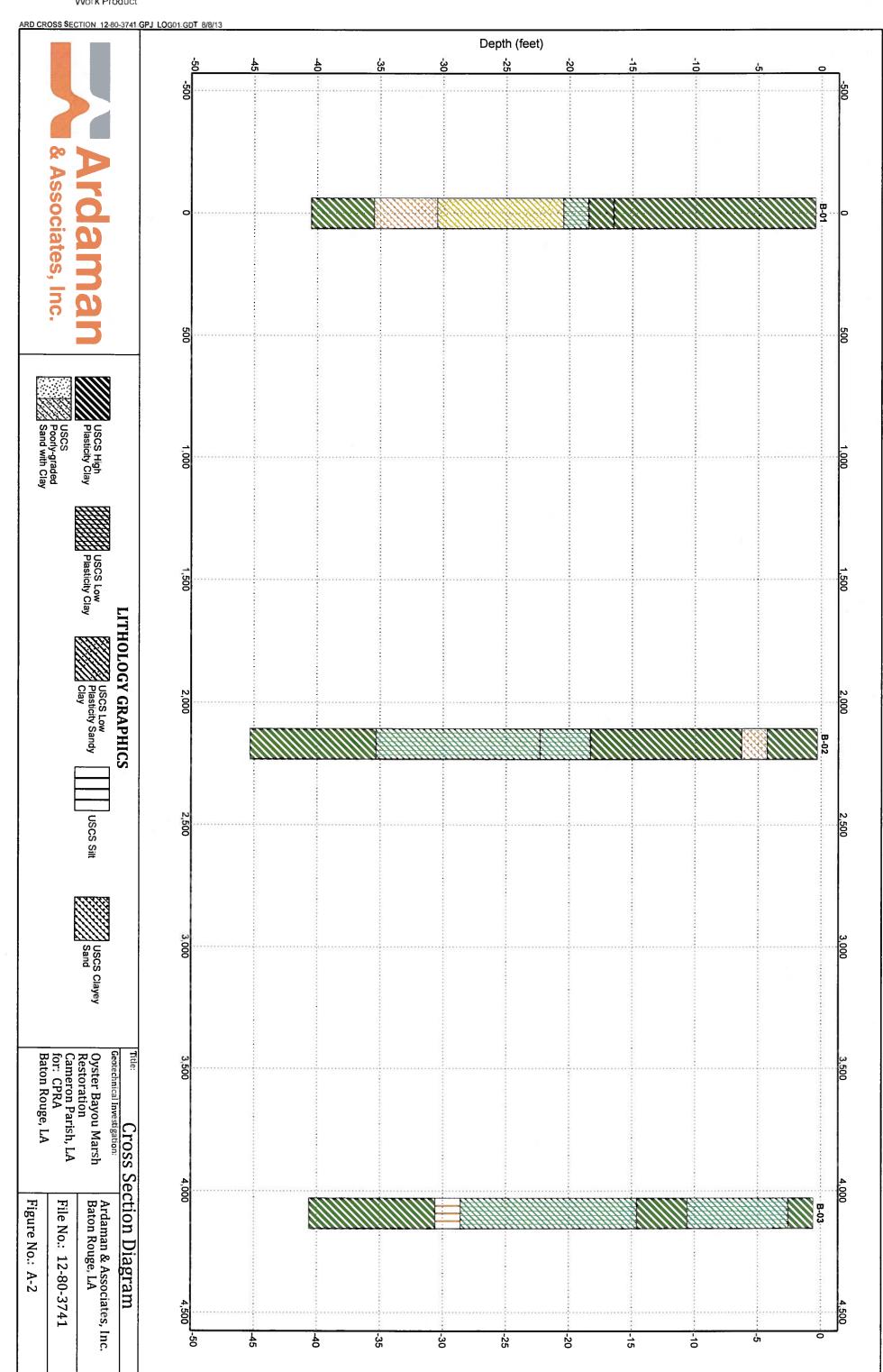
CPRA Baton Rouge, LA

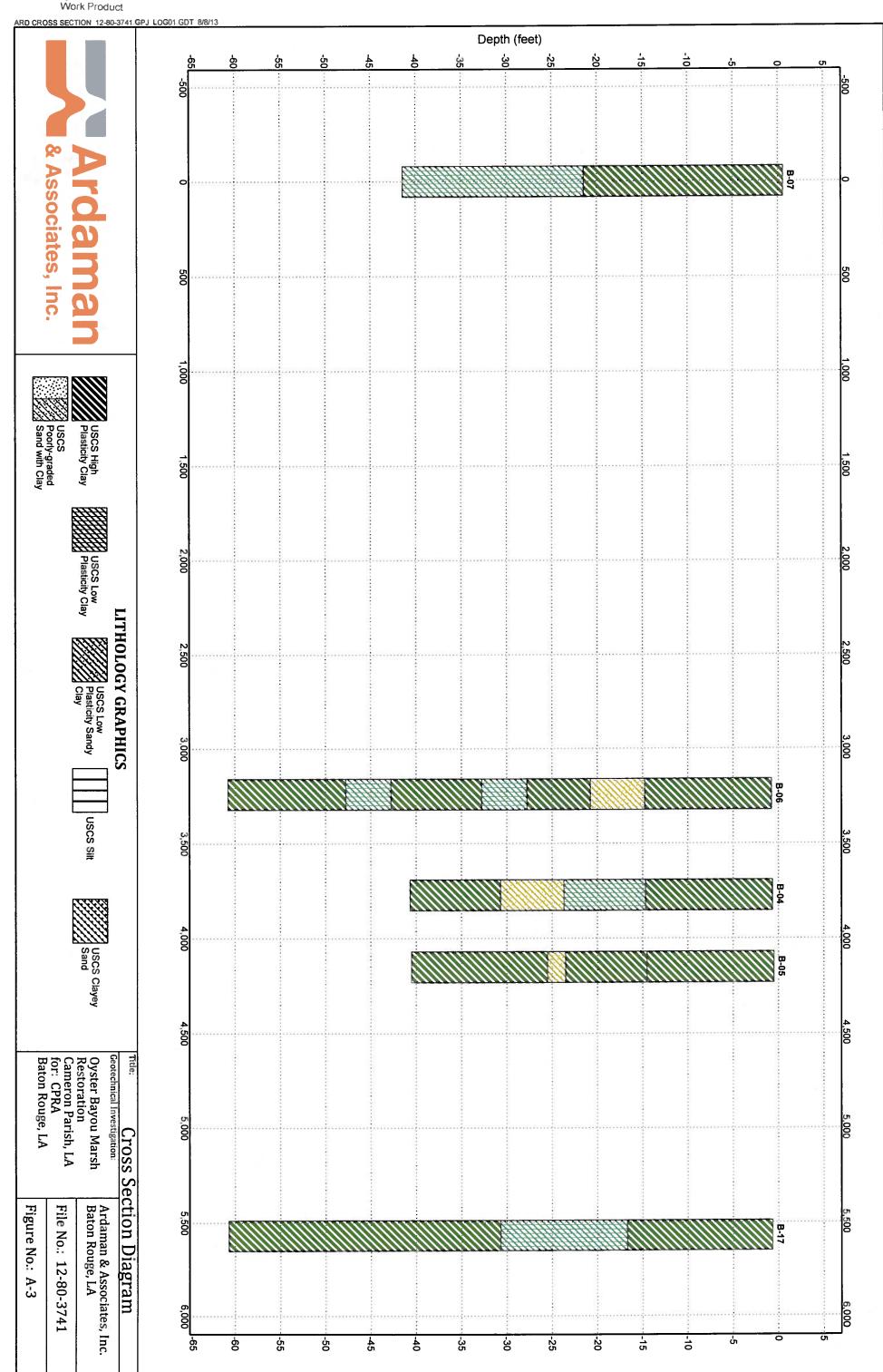
Sheet 1 of 1 Baton Rouge Geotechnical Laboratory
AASHTO Accredited Laboratory, LELAP Certificate No. 02052,
USACE Validated

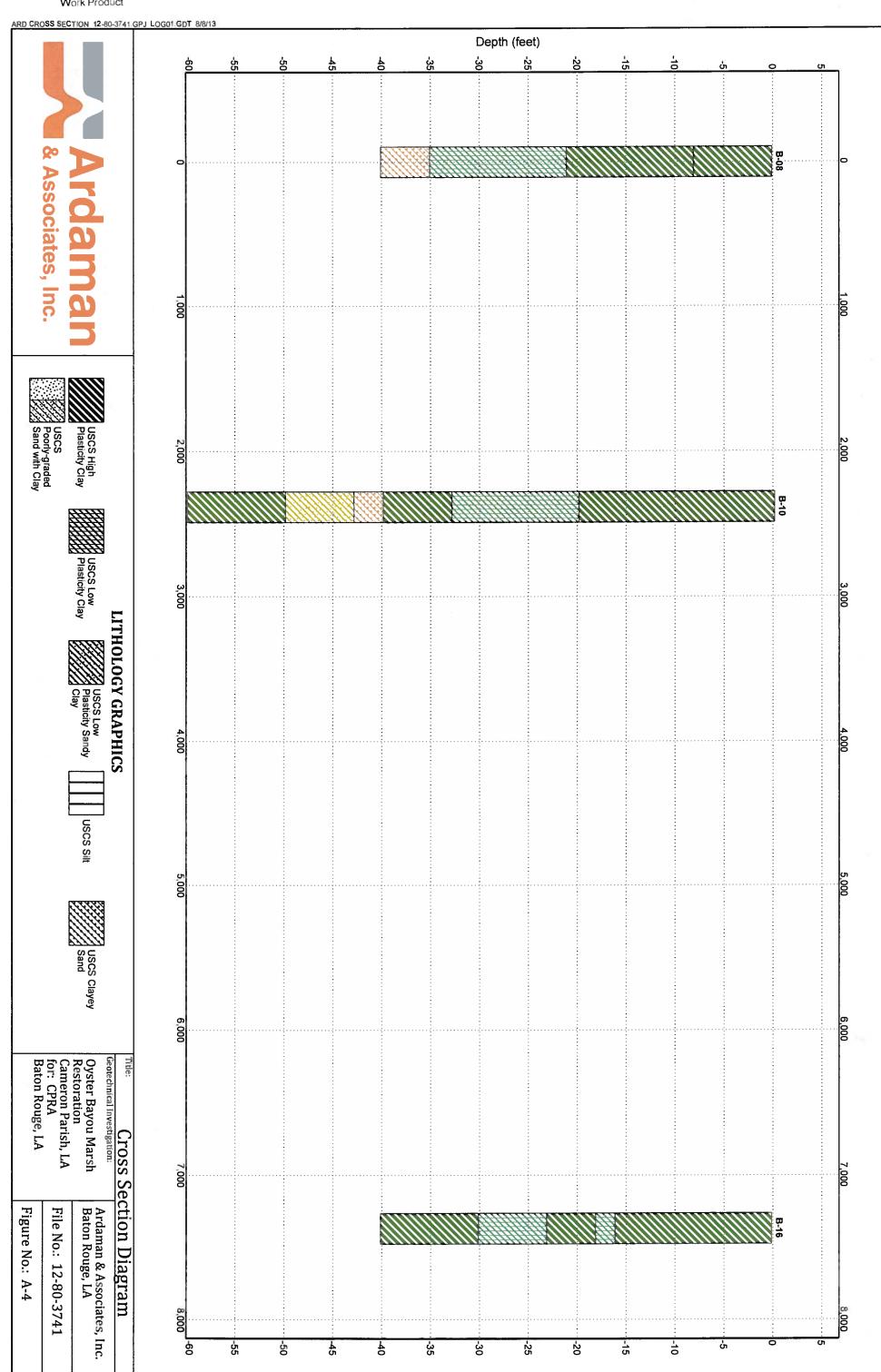
Rig:

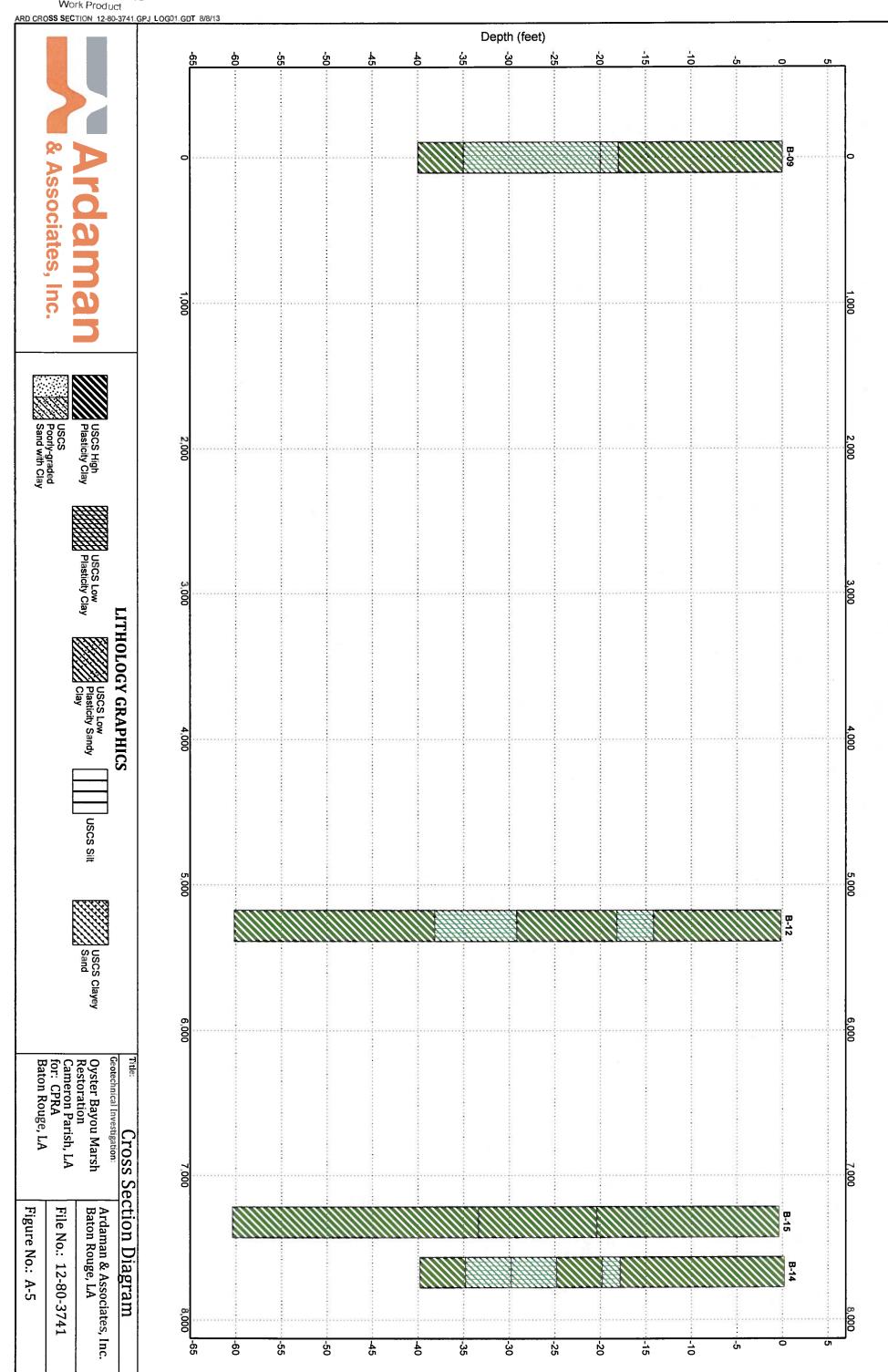
Ardco K-1000

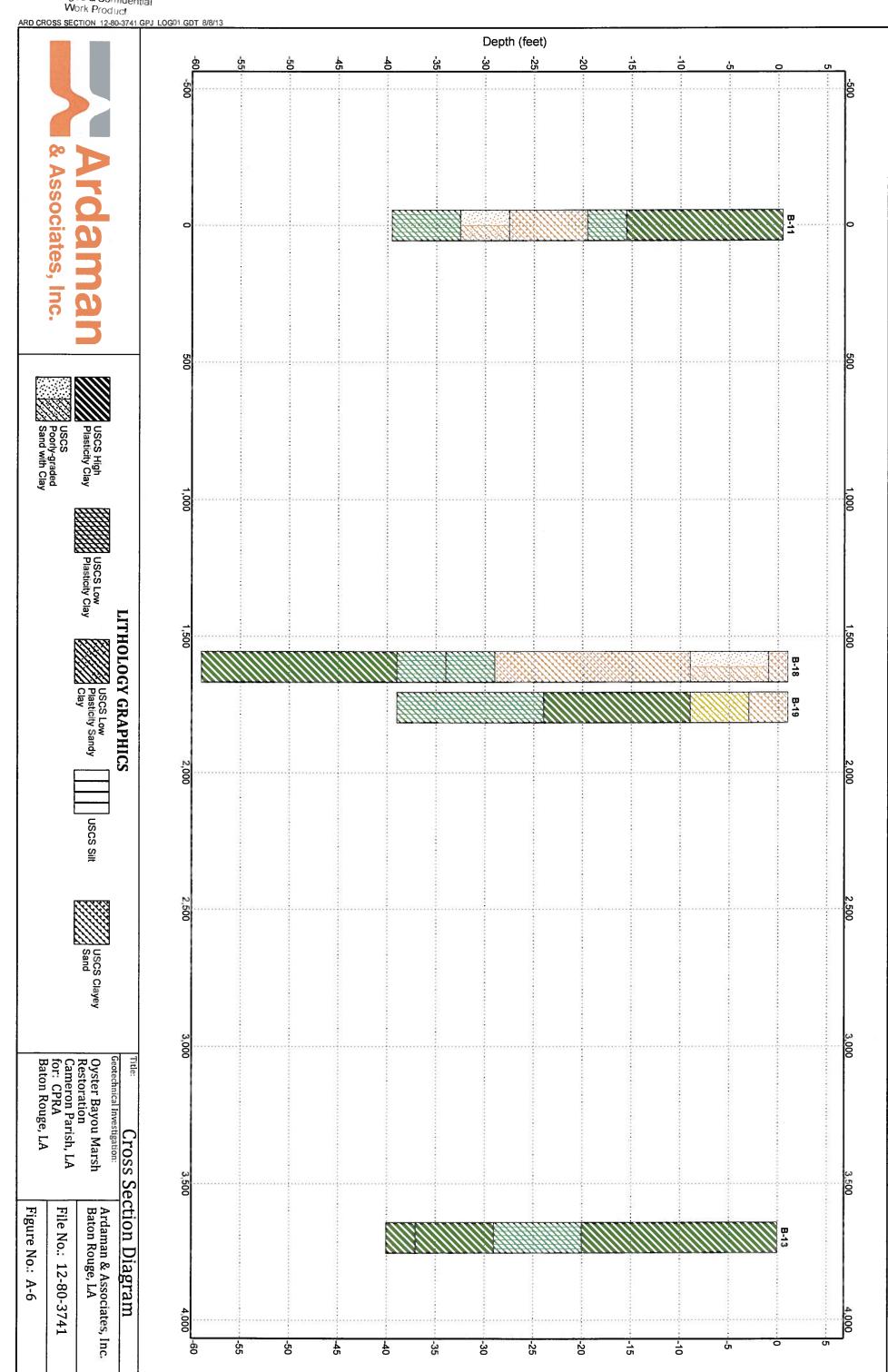
	5.0	_			_	177.27	. = 0 -			Validat	ed		Location: Lat. 29° 46' 4.2"
	FIELD	D	ATA		L/	ABORA						ec e	Long. 93° 24' 24.1"
Ground	Depth	salo	Field	essiv ngth f)	Water	Dry Unit		berg L	imits	sing Sieve	Other	Soil Type	Surface Elevation: N/A (ft., NAVD)
Water Level	(feet)	Sampl	Test Results	Compressive Strength (tsf)	Content (%)		LL	PL	PI	Percent Passing #200 Sieve	Other	So	Description
			0.5 (P)			40.5							Loose white and tan CLAYEY SAND (SC) w/
-		ŀ	-		12	105			i				Silvino
Ā			0.25 (P)							13	GSH		
	- 5 -	ı	0.25 (P)	0.21 t=2.0	30	90	45	16	29	56			Very soft gray SANDY CLAY (CL) w/ silt
		۱	0.0 (P)	2.0	34								
		ı	- -		64						ľ		
	-	35	0.0 (P)	0.06 t=4.0	66	62	65	18	47	67			
	10-		0.25 (P)	0.10	60	64	68	19	49				Very soft gray CLAY (CH)
		30	0.25 (P)	t=5.0									w/ shells at 12-14 feet
			_ 0.20 (,)						į.		!		
	-15-		0.25 (P)				94	26	68				
	-	۱	0.0 (P)		72					ļ	1		
			<u>-</u>		84 78	54			İ				
			0.0 (P)	0.12 t=8.0	77	53	98	19	79	91	ı		
	20-		-										
]			ļ								
		F	0.0 (P)		40			ļ			ļ		
	- 25 -		_		24 32	91	ļ		ļ	-	ļ	1000	Stiff to very stiff tan and gray SILTY CLAY (CL) w/
	-	4									Ì		trace sand layers
			_								1		
			1.0 (P)	2.55 t=12.0	\ ZU	109	40	16	24				
	30-		-		20	104							
		1											
		1	<u></u>			!							
	-35-		1.5 (P)		28	92	İ						
		4											
	-	1	:	1.92	ľ								
			[0.75 (P)	t=16.0	0 32	89	43	19	24				
	<u> </u>				30	84			14-45		I No	tes	Boring completed at 40 ft
==	Groun	a V	Vater Level Da	ıta	4" 1	Boring A Nom. Dia					t:	Unce	onsolidated, Undrained Triaxial Compression Test
Ā	Free w	vat	er first enco	untered	i 4"[4 ft. Dia. Rota 40 ft.	ry Wa	sh:			GS	iteral SH: I	l Pressure = psi Hydrometer Particle Size Analysis
						Boring /	hond	n proce	• Mossis	od			Confidential Information:
Ţ						rehole g	route	d with	cem				Privileged & Confidential Work Product
					ber	ntonite i	ibou c	ompl	etion				Strata Boundaries May Not Be Exa
													Strata Boundaries May Not Be Exa

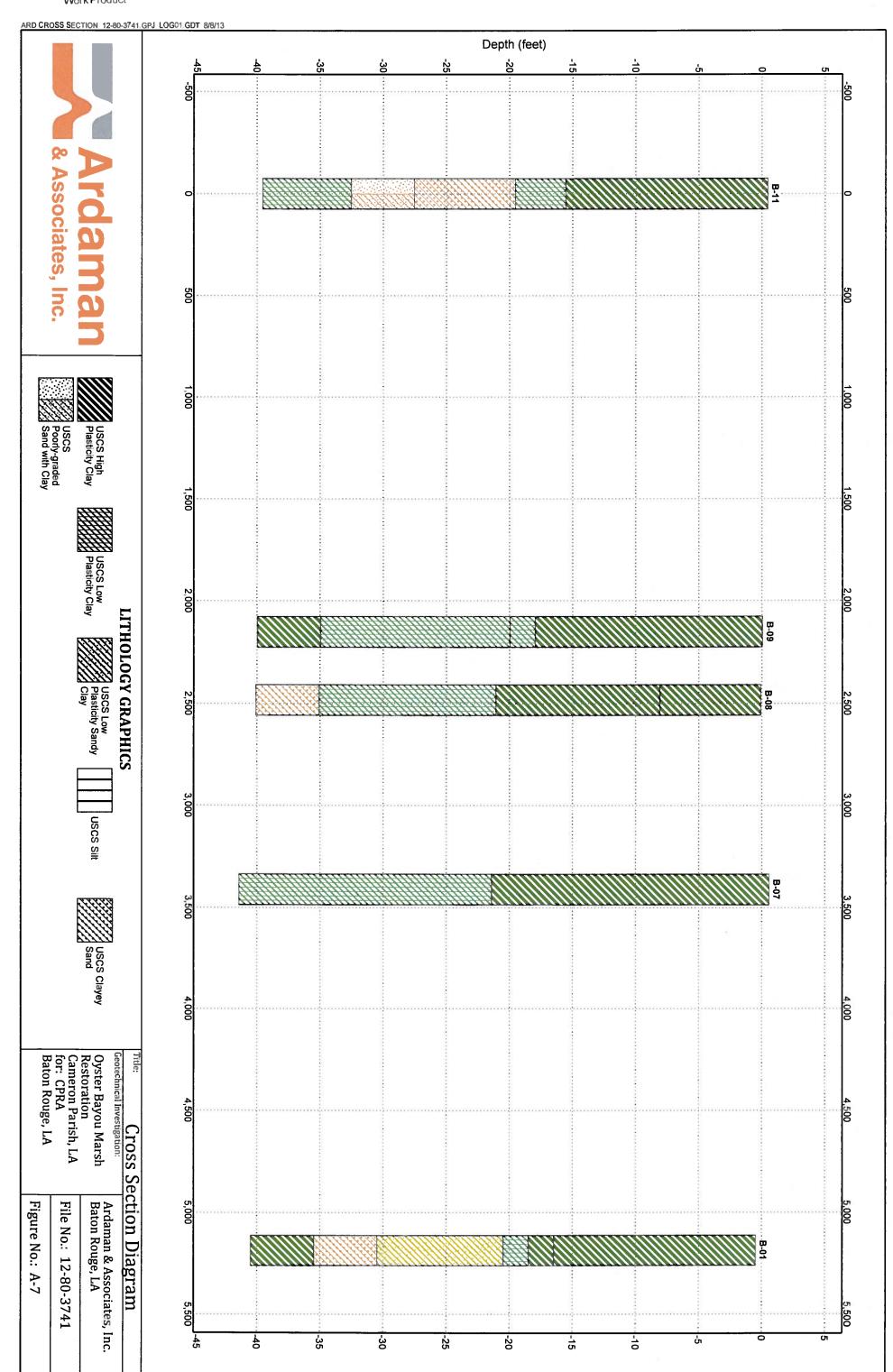


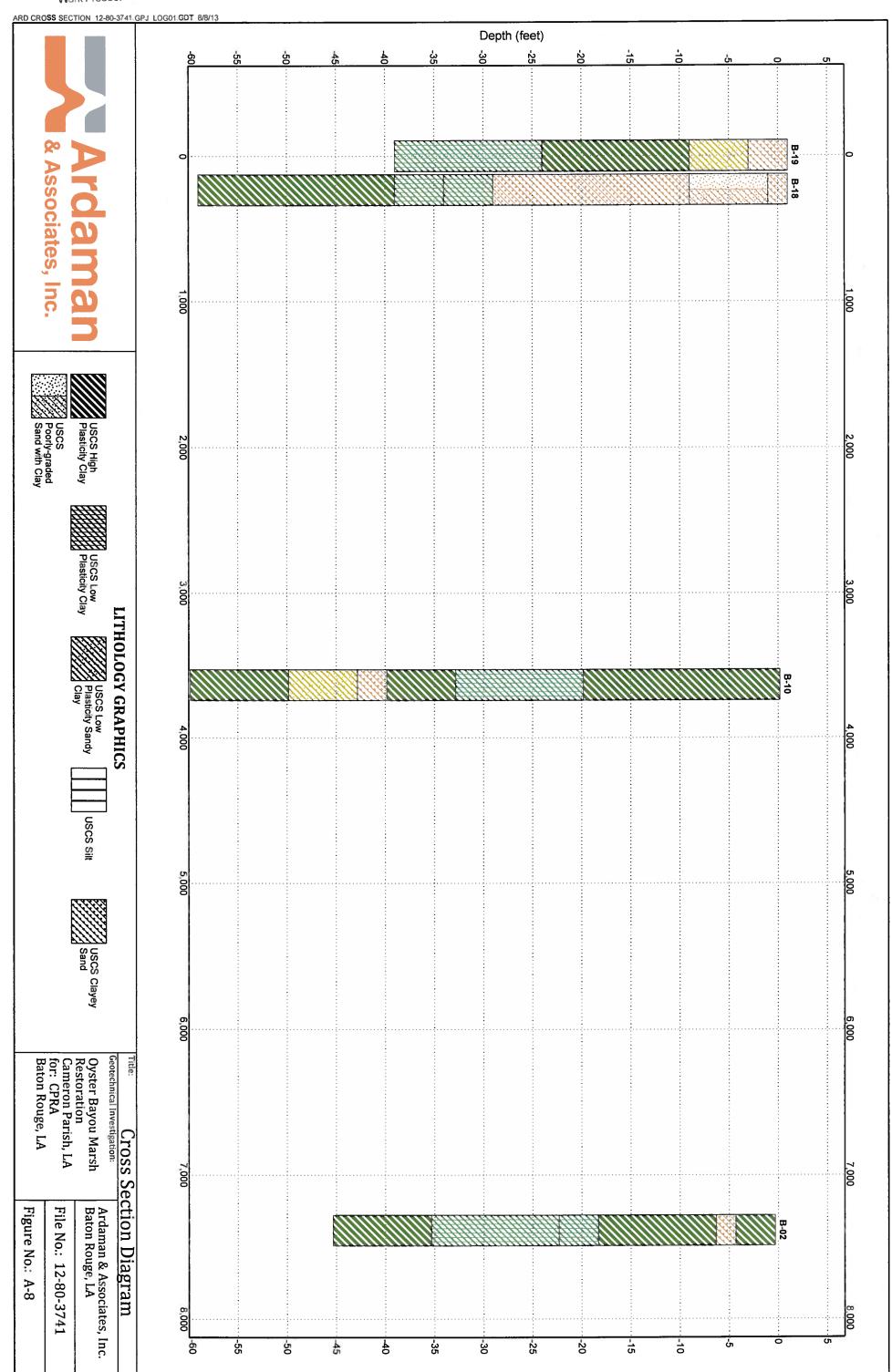


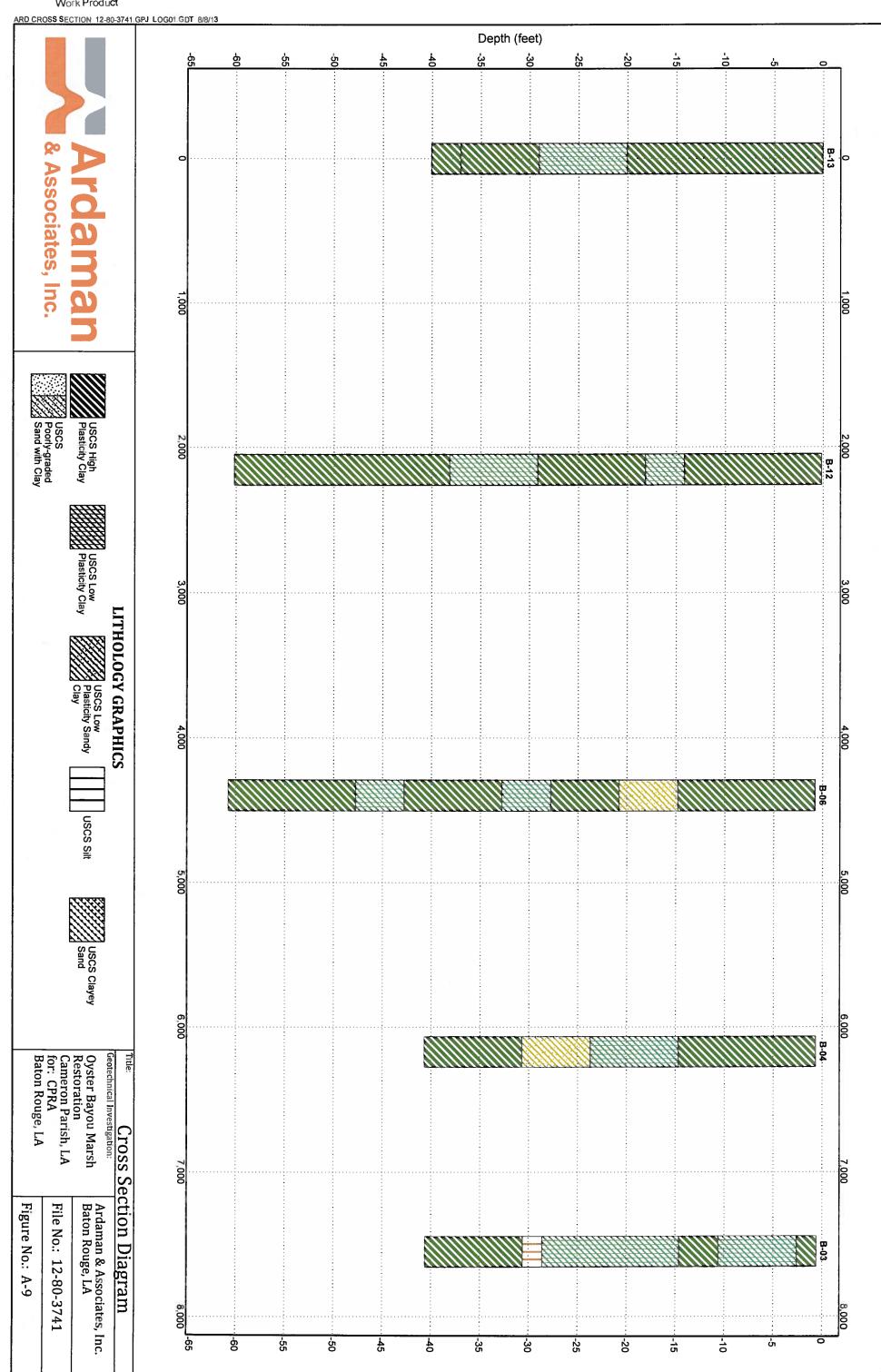


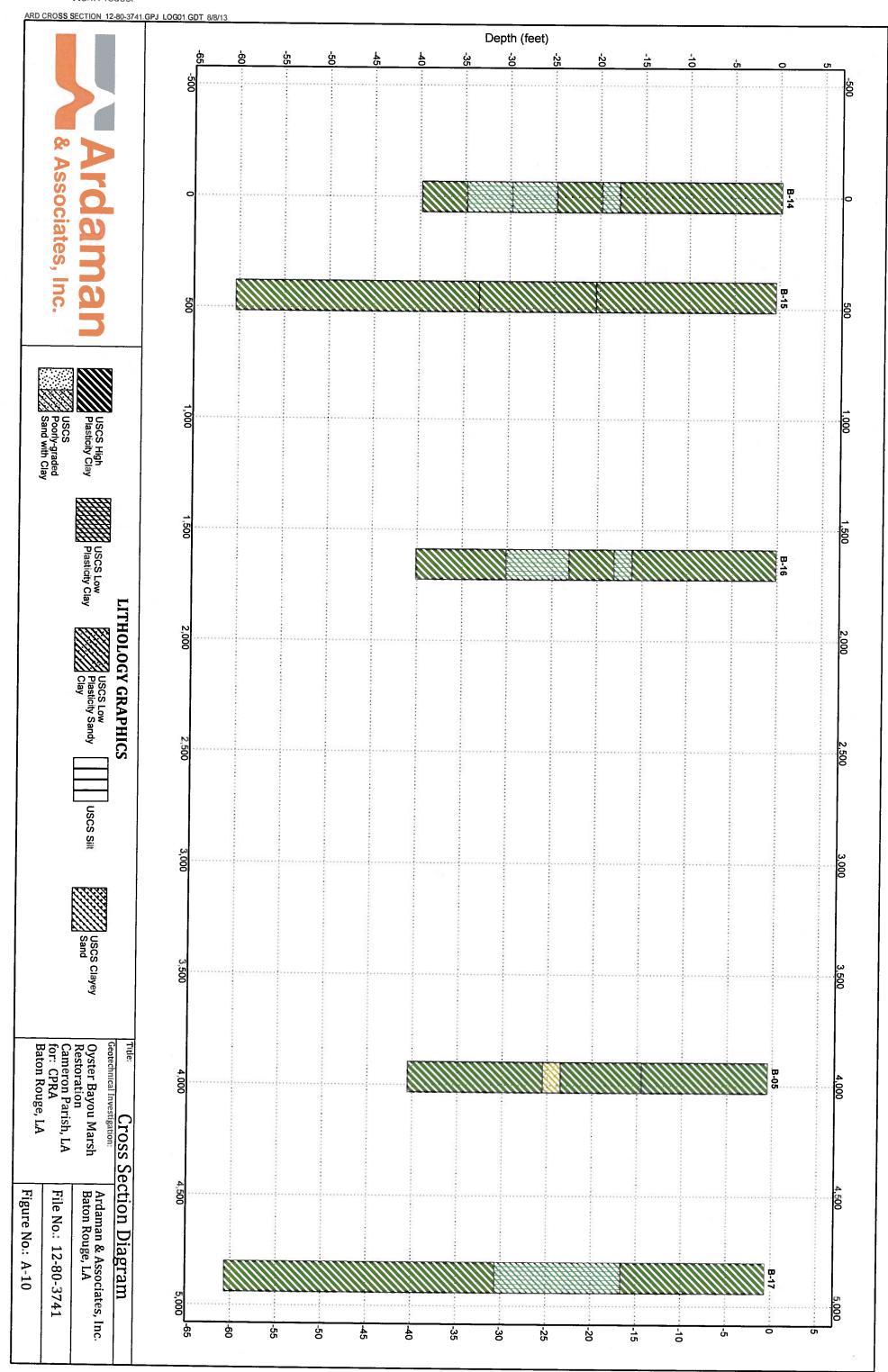












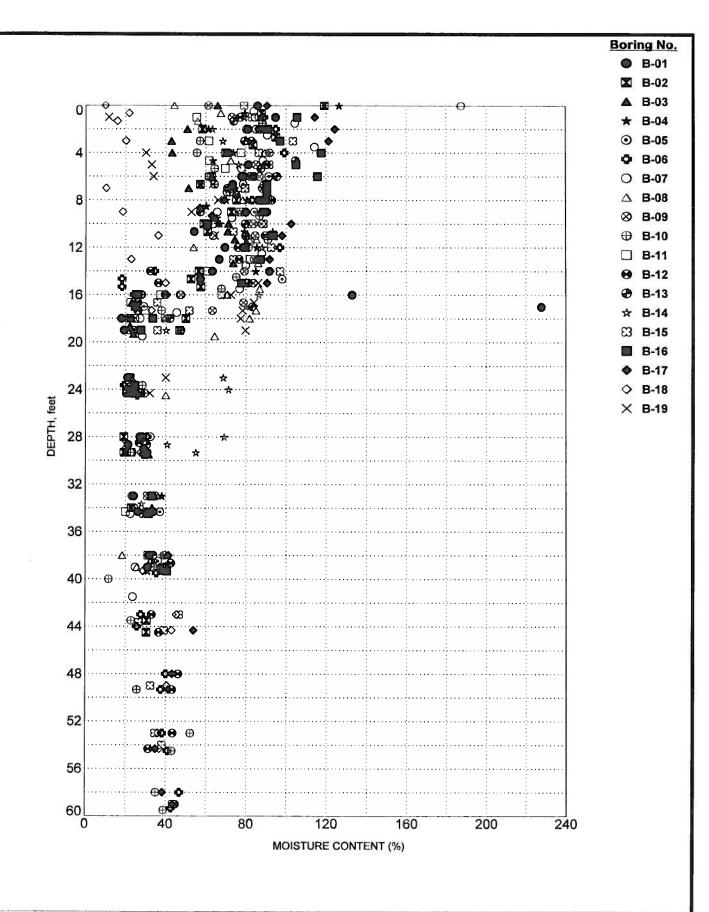
APPENDIX B. LABORATORY DATA PLOTS

This Appendix contains the following:

- Figure B-1 Moisture Content vs Depth
- Figure B-2 Wet Density vs. Depth
- Figure B-3 Dry Density vs. Depth
- Figure B-4 Organic Content vs. Depth
- Figure B-5 Plasticity Chart
- Figure B-6 Liquid Limit vs. Depth
- Figure B-7 Plasticity Index vs. Depth
- Figure B-8 Liquidity Index vs. Depth
- Figure B-9 Hydrometer Particle Size Analyses Results
- Figure B-10 Correlations between Compressibility and Index Properties
- Figure B-11 Coefficient of Compressibility vs. Stress Ratio
- Figure B-12 C_{αε} vs. CR
- Figure B-13 Stress History Profiles
- Figure B-14 Coefficient of Consolidation vs. Stress Ratio
- Figure B-15 Vertical Coefficient of Permeability vs. Void Ratio
- Figure B-16 UUC Shear Strength vs. Depth
- Figure B-17 Vertical Effective Stress and Undrained Shear Strength vs. Depth



Ardaman & Associates, Inc.



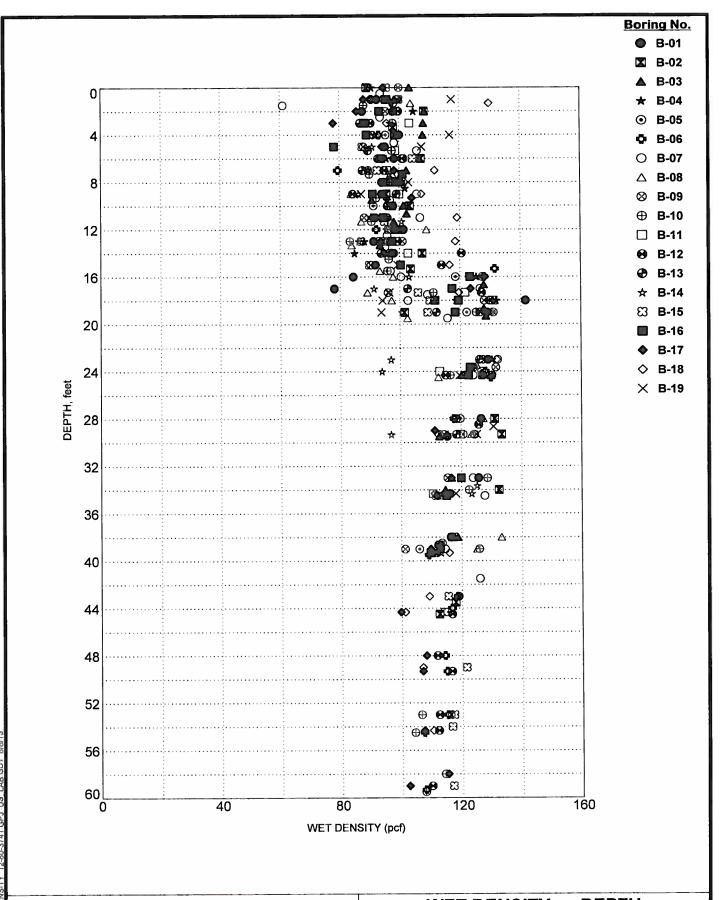


MOISTURE CONTENT vs DEPTH

Project: Oyster Bayou Marsh Restoration

Client: CPRA

AAI Project Number: 12-80-3741 Figure No.: B-1





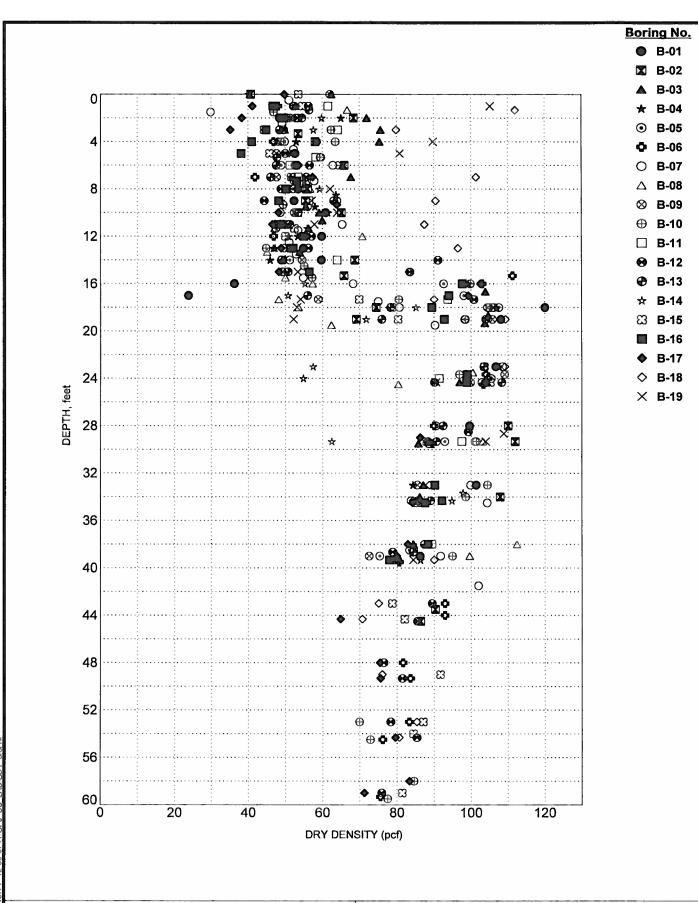
WET DENSITY vs DEPTH

Project: Oyster Bayou Marsh Restoration

Client: CPRA

AAI Project Number: 12-80-3741

Figure No.: B-2



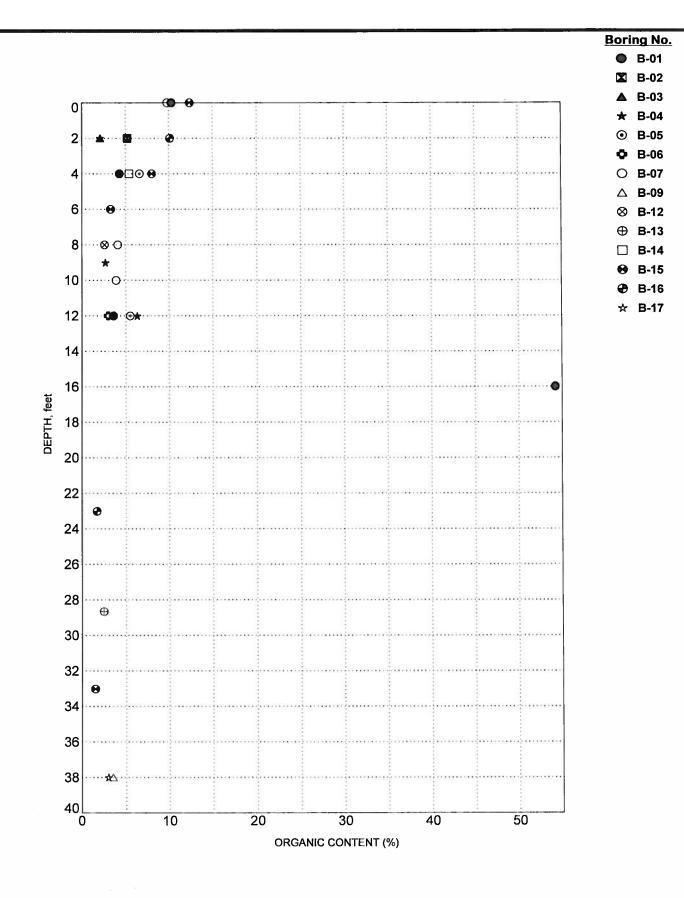


DRY DENSITY vs DEPTH

Project: Oyster Bayou Marsh Restoration

Client: CPRA

AAI Project Number: 12-80-3741 Figure No.: B-3





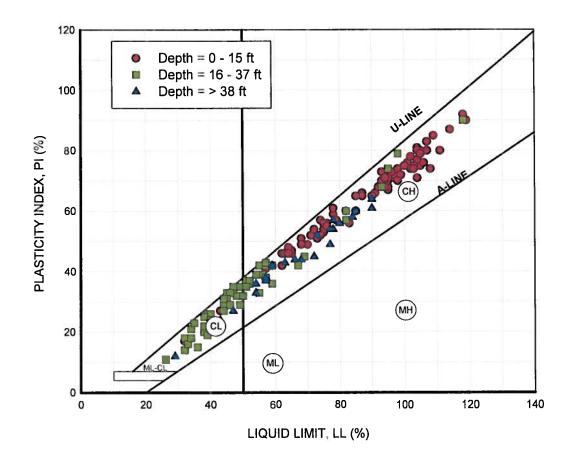
ORGANIC CONTENT vs DEPTH

Project: Oyster Bayou Marsh Restoration

Client: CPRA

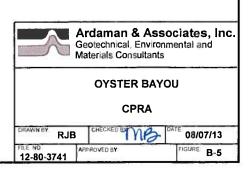
AAI Project Number: 12-80-3741

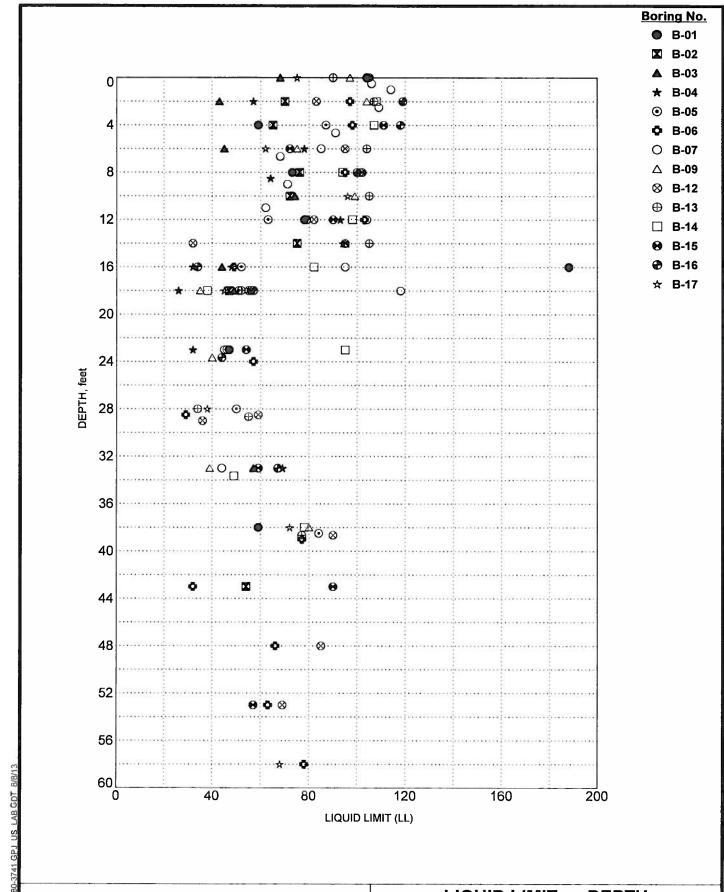
Figure No.: B-4



PLASTICITY CHART

Confidential Information: Privileged & Confidential Work Product





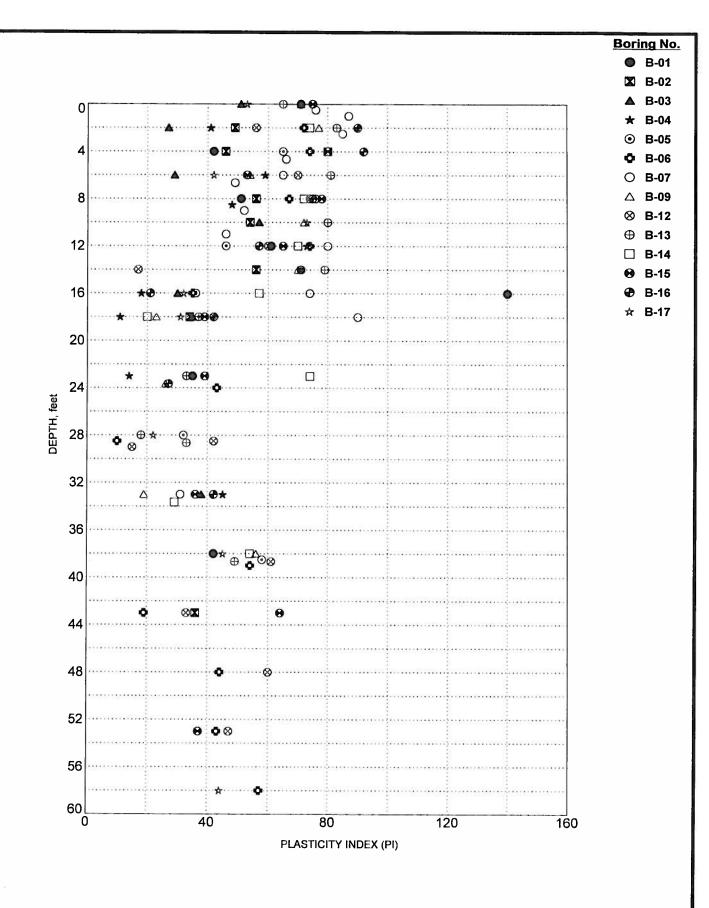


LIQUID LIMIT vs DEPTH

Project: Oyster Bayou Marsh Restoration

Client: CPRA

AAI Project Number: 12-80-3741 Figure No.: B-6



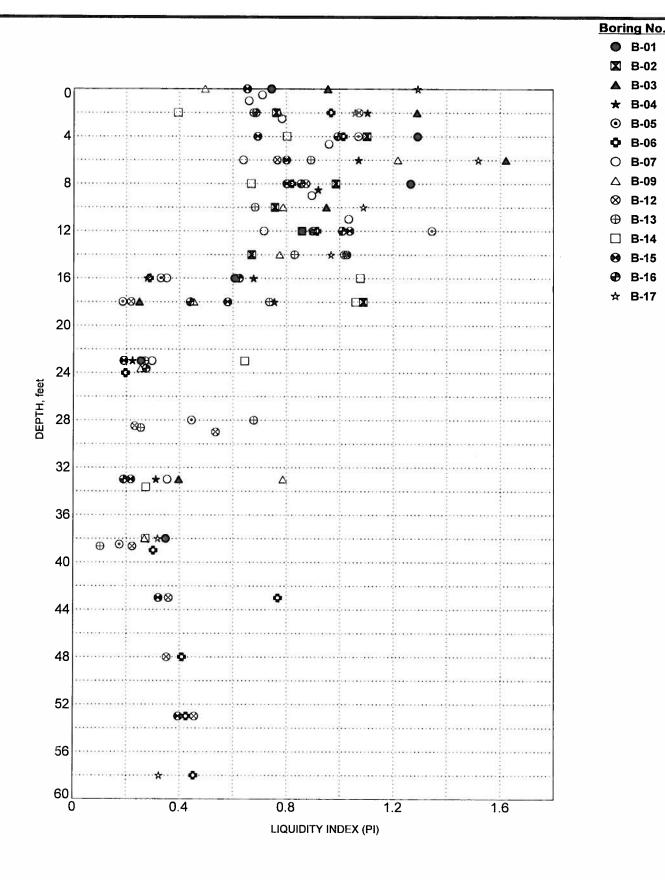


PLASTICITY INDEX vs DEPTH

Project: Oyster Bayou Marsh Restoration

Client: CPRA

AAI Project Number: 12-80-3741 Figure No.: B-7





LIQUIDITY INDEX vs DEPTH

Project: Oyster Bayou Marsh Restoration

Client: CPRA

AAI Project Number: 12-80-3741

Figure No.: B-8

B-01 ■ B-02 B-03

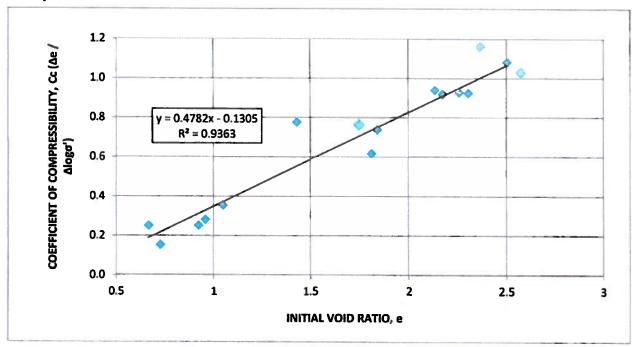
B-04 B-05 B-06 O B-07 B-09 ⊗ B-12 ⊕ B-13 □ B-14

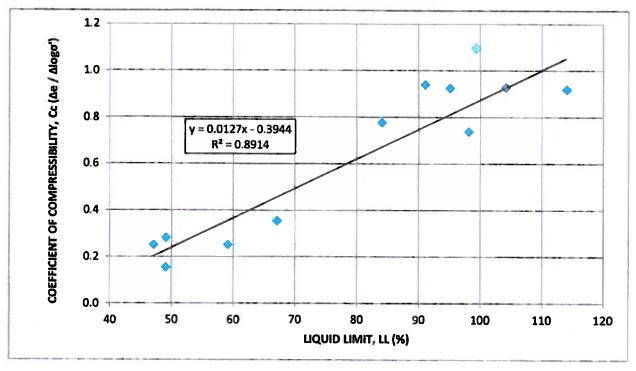
⊕ B-16 **☆** B-17

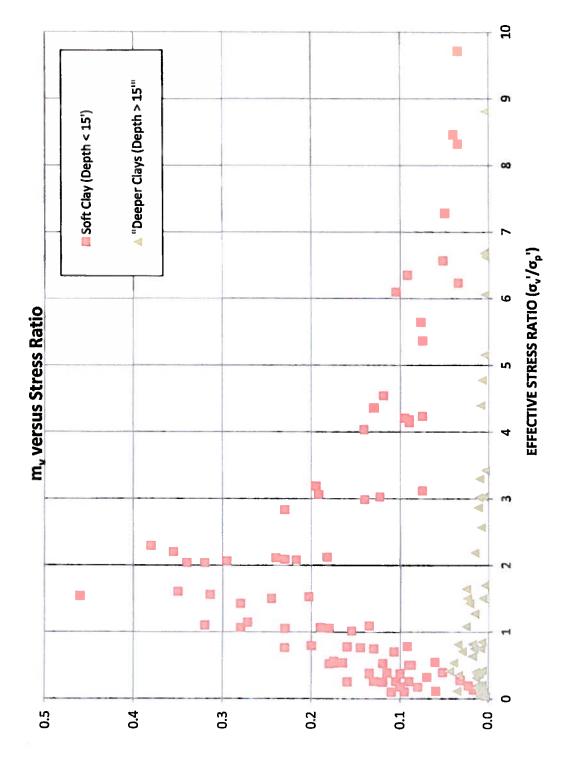
Figure B-9 Hydrometer/Sieve Particle Size Analyses Results

DOFING ID	Sample Depth	% Gravel	% Sand	% Silt	% Clay
B-01	33-35	0	78	7	15
B-02	2-4	0	11	29	09
B-02	4-6	0	53		47
B-02	14-16	0	2	52	43
B-03	0-2	0	2	34	64
B-03	10-12	0	4	5	96
B-04	8-10	0	8	32	65
B-05	4-6	0	3	6	97
B-05	23-25	0	45	14	41
B-07	2-4	0	52	12	36
B-07	4-6	21	15	9	64
B-07	8-10	0	06	1	10
B-08	4-6	0	31	18	51
B-08	8-10	5	5	6	90
B-08	16-18	1	23	7	76
B-09	8-9	0	9	6	94
B-10	4-6	0	4	6	96
B-11	23-25	0	78	9	16
B-12	28-30	0	1	∞	91
B-12	48-50	0	1	15	84
B-14	2-4	0	1	6	66
B-15	18-20	0	25	7	75
B-18	0-2	10	57	19	14
B-18	2-4	7	98	3	4
B-18	10-12	2	81	8	6
B-18	14-16	5	59	16	20
B-18	28-30	0	77	13	10
B-18	33-35	0	20	48	32
B-19	2-4	7	81	4	8
B-19	4-6	0	44	25	31
B-19	8-10	0	34	46	71

Client: CPRA Project: Oyster Bayou AAI Project No.12-80-3741







COEFFICIENT OF COMPRESSIBILITY, m_{ν} (1/tsf)

316 Highlandia Drive Baton Rouge, LA 70810 225-752-4790 (phone) 225-752-4878 (fax)

Confidential Information, Privileged & Confidential Work Product

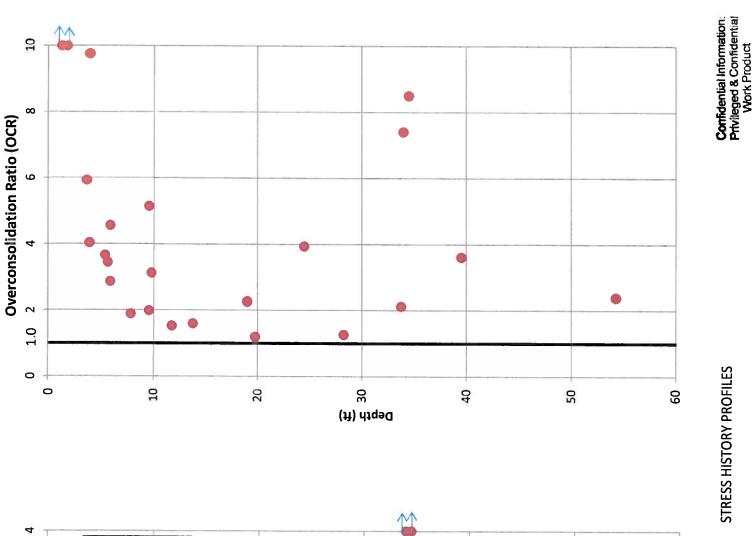
0.60 0.50 0.40 CR ($\Delta\epsilon_{\nu}/\Delta\log\sigma'$) Cas versus CR 0.20 0.10 0.00 0.000 $C_{ac}\left(\Delta\epsilon/\Delta\log t\right) \\ \begin{array}{c} 0.012 \\ 0.002 \\ 0.003 \end{array}$ 0.020 0.016 0.004 Confidential Intermation Privileged & Comfidential Work Product

Client: CPRA Project: Oyster Bayou AAI Project No. 12-80-3741

Figure B-12

Ardaman & Associates, Inc.

316 Highlandia Drive Baton Rouge, LA 70810 225-752-4790 (phone) 225-752-4878 (fax)



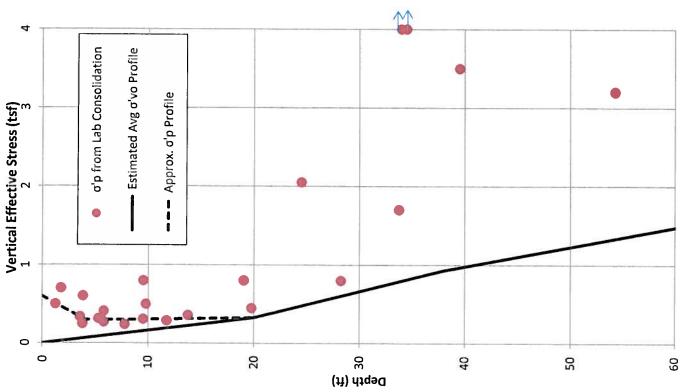


Figure: B-13

STRESS HISTORY PROFILES

AAI Project No. 12-80-3741 Project: Oyster Bayou

Client: CPRA

Project: Oyster Bayou AAI Project No.12-80-3741 Client: CPRA

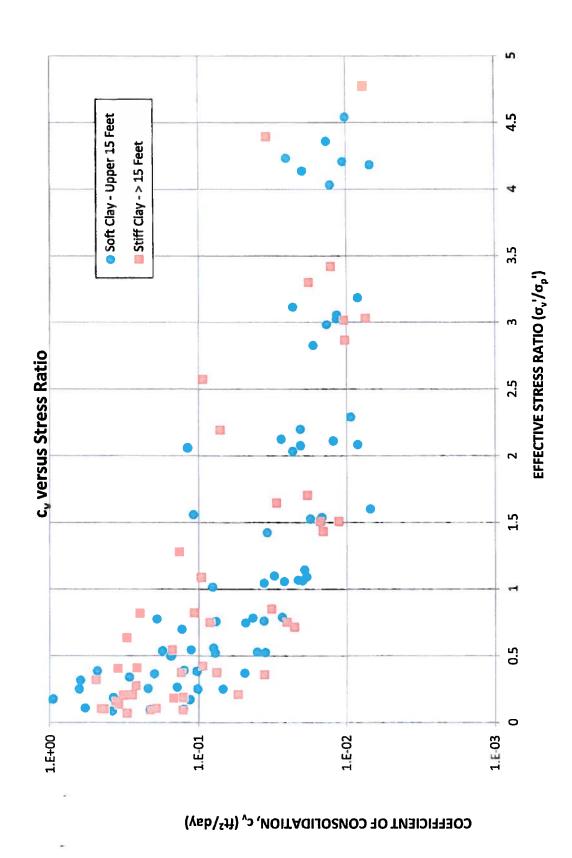
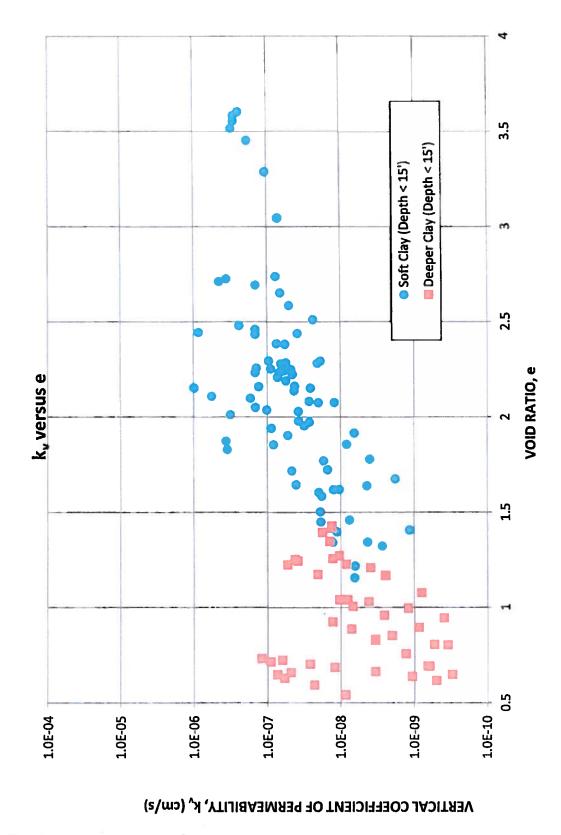


Figure B-14

Confidential Information.
Privileged & Confidential
Work Product

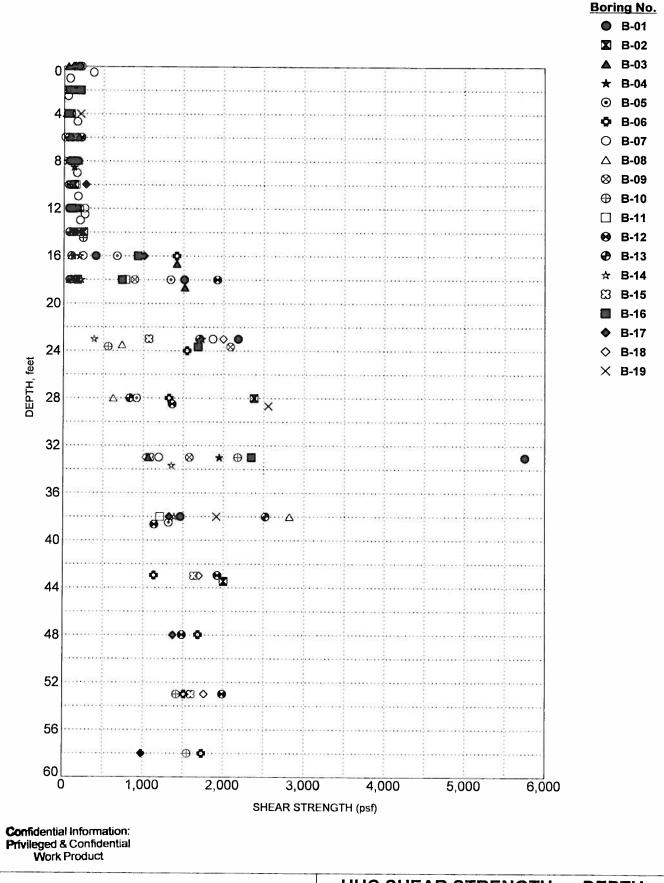
316 Highlandia Drive Baton Rouge, LA 70810 225-752-4790 (phone) 225-752-4878 (fax)

Client CPRA Project Oyster Bayou AAI Project No.12-80-3741



316 Highlandia Drive Baton Rouge, LA 70810 225-752-4790 (phone) 225-752-4878 (fax)

Confidential Information.
Privileged & Confidential
Work Product



RD DEPTH VS SHEAR STRENGTH 12-80-3741 GPJ US LAB GDT 8/9/13

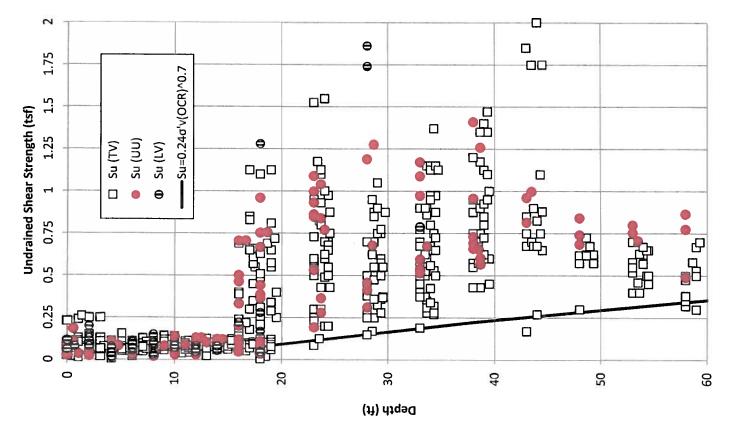
UUC SHEAR STRENGTH vs DEPTH

Project: Oyster Bayou Marsh Restoration

Client: CPRA

AAI Project Number: 12-80-3741

Figure No.: B-16



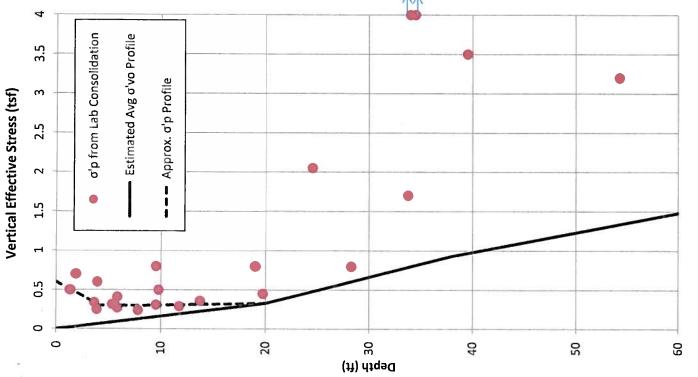


Figure: B-17

Project: Oyster Bayou Client: CPRA

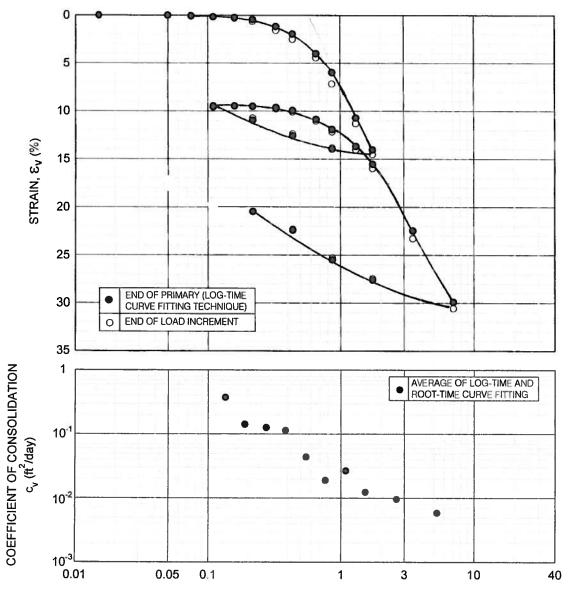
AAI Project No. 12-80-3741

APPENDIX C. CONSOLIDATION TEST RESULTS

This Appendix contains the following:

• Incremental Consolidation Test Results





VERTICAL EFFECTIVE STRESS, $\sigma^{\prime}_{\ vc}$ (tsf)

SAMP		DAT	٠.
SHIVIE	LE	ואט	м

BORING NO. SAMPLE NO. B-01

DEPTH (FEET):

DESCRIPTION:

Brown and gray CLAY (CH)

w/shells and trace organics

INDEX PROPERTIES

LIQUID LIMIT (%): 104 PLASTIC LIMIT (%): 33 PLASTICITY INDEX (%): 71 SPECIFIC GRAVITY: 2.74 95 ORGANIC CONTENT (%): 10.29

SPECIMEN CONDITIONS	INITIAL	FINAL
MOISTURE CONTENT (%)	78.1	62.4
DRY DENSITY (Ib/ft ³)	52.5	63.8

8. VOID RATIO: 1.69

CONSOLIDATION PARAMETERS

EFFECTIVE OVERBURDEN STRESS, σ'_{vo} (tsf):	0.027
PRECONSOLIDATION PRESSURE, o', (isf):	0.70
VIRGIN COMPRESSION RATIO, CR.	0.285
RECOMPRESSION RATIO, RR:	0.045

INCREMENTAL CONSOLIDATION **TEST RESULTS**

Confidential Information. Privileged & Confidential Work Product



Ardaman & Associates, Inc. Geotechnical, Environmental and Materials Consultants

OYSTER BAYOU

CPRA

DRAWN BY. RJB

03/13/13

12-80-3741

C1

0.00265 0.00788 0.00394 0.00606 0.00960 0.00176 0.00649 0.00303 0.000328 0.01018 CRE 0.00 0.03 0.03 0.03 0.03 0.03 1.156 1.156 1.158 12.15 25.30 22.30 Strain at EOI (%) 14.03 15.96 23.27 20.44 20.30 17.55 11.01 30.56 ONE-DIMENSIONAL INCREMENTAL LOADING CONSOLIDATION TEST SUMMARY SHEET Strain at EOP (%) 13.66 15.52 22.46 29.88 27.58 25.47 22.38 20.44 20.30 17.55 Void Ratio at EOI 1.9512 2.1783 2.1152 2.0267 1.8916 1.7859 1.9098 2.2594 2.2586 2.2569 2.2534 2.2495 2.2392 2.2392 1.8087 1.9516 1.9417 1,9309 1,9007 1.8636 1.7392 1.5009 1.2635 1.3649 .4349 Void Ratio at 2.2594 2.2594 2.2573 2.2520 2.2520 2.2452 2.2219 1.9110 1.9513 2.1964 2.1291 2.0656 1.8502 1.7535 1.8053 1.9482 1.9460 1.9063 1.8718 1.8143 1.2855 1.3606 1.4293 1,5976 1.9361 1.6874 EOP Height at EOI (inch) 0.7550 0.7548 0.7544 0.7536 0.7537 0.7503 0.7432 0.7432 0.7362 0.7362 0,6698 0.6616 0.6836 0.6830 0.6814 0,6719 0.6491 0.6345 0.5793 0.6789 0.5243 0.5478 0.5640 0.5866 0,6506 0.6837 0,6017 0.6225 0.7550 0.7550 0.7538 0.7538 0.7537 0.7617 0.748 0.7248 0.6743 0.6491 0.6622 0.6824 0.6824 0,6732 0.6519 0.6378 0.5854 0.5294 0.5468 0.5627 0.5860 0.6007 0.6017 0.6225 Height at 0.6801 inch) 0.0025
0.093
0.093
0.0135
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.0275
0.02 Average Effective Stress (tst) 1.06E-02 1.87E-02 1.05E-02 2.59E-02 1.18E-02 5.50E-03 4.98E-02 2.26E-02 2.21E-02 1.94E-02 1.14E-02 7.66E-03 5.06E-03 6.30E-03 2.81E-01 1.40E-01 1.11E-01 1.13E-01 4.39E-02 Cv (ft²/day) (L=log, S=sq rt) 120 150 150 144 1440 750 1230 480 too (sec) 080 1440 800 350 800 1080 2400 3720 660 Time 0.0808 0.0814 0.0833 0.0876 0.0954 0.1034 0.1192 0.1192 0.1725 0.1905 0.1562 0.1569 0.1612 0.1773 0.2429 0.2415 0.2204 0.1790 0.1662 0.1563 0.1684 0.1920 0.2069 0.2641 0.2965 0.2572 0.2797 Ö Dial Readings (inch) 0.0813 0.0831 0.0862 0.0923 0.0923 0.1160 0.1310 0.1680 0.1930 0.1913 0.1804 0.1678 0.1563 0.1565 0.1575 0.1754 0.1892 0.2036 0.2580 0.2975 0.2810 0.2578 0.2429 0.2415 0.2204 0.1671 EOP 0.0806 0.0806 0.0810 0.0835 0.0835 0.0852 0.0863 0.1046 0.1412 0.1958 0.1659 0.1569 0.1687 0.1923 0.3200 0.2570 0.2425 0.2412 0.1786 0,1562 0.1614 0.1563 0.2798 0.2661 Initial 0.110 0.160 0.220 0.330 0.440 0.660 0.870 1.310 1.740 0.870 0.870 0.110 0.160 0.220 0.330 0.440 0.860 0.870 1.310 1.740 3.510 7.040 1.740 0.870 0.440 0.220 0.110 Effective Stress (tsf)

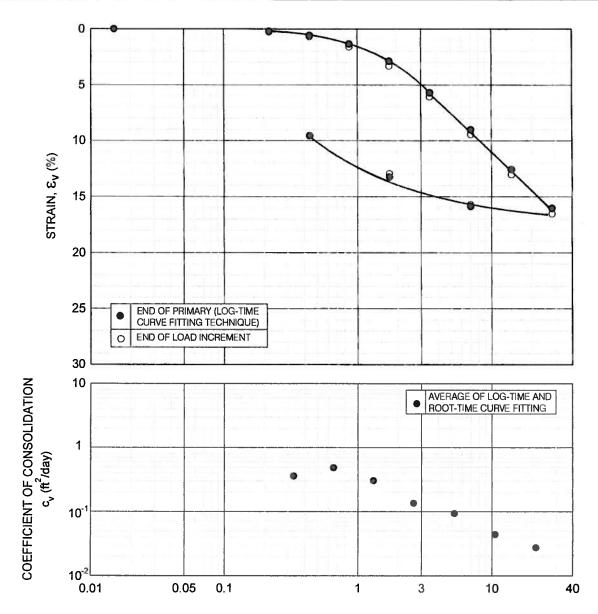
dation	ypically 24 hrs +/-)		2.743	2.0000	62,50	0.2316	32.71
EOP= End of Primary Consoli	EOI = End of load increment (typically 24 hrs +/-)		Specific Gravity	Ring Diameter (in)	Ring weight (g)	Height of Solids (in)	Weight of Dry Soil (g)
Final	Conditions	0,6222	62.4	103.5	63.8	101.5	1,6861
Initial	Conditions	0.7550	78.1	93,6	52.5	94.9	2.2594
		Height (in)	Wc (%)	yt (pal)	7d (pct)	Saturation (%)	Void ratio, e
	Oyster Bayon	12-80-3741	B-01	0-2 (1.75)			
	Project Name:	File Number:	Boring Number:	Depth:			

GEOTECHNICAL TESTING LABORATORY

E-DIMENSIONAL INCREMENTAL LOADING CONSOLIDATION TEST SLIMMARY SHE

Thirding ECP ECI Time, Line, Cap Average Fig. Height at North Line, Cap Eci Ecp ECI Raio at Raio at ECP (%) ECI														
Time	Dial	Readings (inc	£											
0.0806 0.0806 0.0806 0.0806 0.0756 0.7550 0.7556 2.2584 2.2894 0.00 0.00 0.0806 0.0803 0.0804 4 70E 0.7536 0.7548 2.2594 2.2896 0.07 0.08 0.0833 0.0834 1.54 5 4.70E-01 0.135 0.7536 0.7546 2.2543 2.2896 0.07 0.08 0.0833 0.0874 5 1.42E-01 0.753 0.7527 2.2543 2.2896 0.07 0.09 0.0893 0.0876 5 1.42E-01 0.775 0.7405 2.7522 2.2843 0.06 0.07 0.0893 0.1024 6.148E-01 0.775 0.7405 0.7405 0.7405 0.7405 0.7405 0.7406 0.750 0.7406 0.750 0.7406 0.7406 0.7406 0.7406 0.7406 0.7406 0.7406 0.7406 0.7406 0.7406 0.7406 0.7406 0.7406 0.7406 0.7406 0.	Initial	EOP		Time,	Method (L=log, S=sq rt)	Cv (ft²/day)	Average Effective Stress (tsf)	Height at EOP (inch)	Height at EOI (inch)	Void Ratio at EOP	Void Ratio at EOI	Strain at EOP (%)	Strain at EOI (%)	Cae
0.0896 0.0806 0.0806 0.0806 0.0806 0.0806 0.0807 0.0754 2.2564 2.2586 0.007 0.08 0.0814 0.0833 1.48 5 4.76E-01 0.135 0.7536 2.2542 2.2530 0.07 0.08 0.09 0.09 0.7536 2.2449 2.2592 0.04 0.08 0.08 0.7536 2.2449 2.2592 0.04 0.08 0.08 0.7536 0.7536 2.2449 2.2592 0.04 0.09 0.09 0.7536 0.7536 2.2449 2.2592 0.04 0.08 0.08 0.7536 0.7536 2.2449 2.2592 0.04 0.08 0.08 0.7536	0.080	1	0.0806				,	0.7550	0.7550	2.2594	2.2594	0.00	0.00	
0.08313 0.08314 1.5 4.70E-01 0.063 0.7545 0.7543 2.2573 2.2569 0.07 0.019 0.0831 0.0833 0.0834 0.753 0.7536 2.2543 0.16 0.19 0.0863 0.0846 50.4 5.47E-01 0.190 0.7536 0.7536 2.2448 2.2852 0.2449 0.19 0.0895 0.0874 5.04 5.47E-01 0.750 0.7503 2.2448 1.02 1.44 0.0195 0.0196 0.7504 2.142 2.289 0.76 0.7507 2.448 1.02 1.44 0.1195 0.1192 1.661 5.47E-02 0.765 0.7707 2.0639 1.771 1.11 1.14	0.080		0.0808				0.025	0.7550		2.2594	2.2586	0.00	0.03	1
0.0831 0.0834 0.0834 0.0834 0.0834 0.0834 0.0834 0.0839 0.7539 0.7539 0.2534 0.16 0.19 0.0838 0.0844 5.04 4.70E-01 0.135 0.7533 0.7527 2.2849 2.2849 0.13 0.03 0.0836 5.04 5 1.43E-01 0.275 0.7534 2.282 2.2849 0.15 0.03 0.0833 0.1034 5 1.14E-01 0.275 0.7344 2.282 2.049 0.15 0.1155 0.1034 5 1.14E-01 0.385 0.7405 0.7344 2.196 0.717 2.196 0.754 2.196 0.754 0.754 2.157 0.154 <	0.081		0.0814				0.063	0.7545		2.2573	2,2569	0.07	0.08	1
0.0838 0.0844 154 S 4.70E-01 0.155 0.7533 0.7527 2.2520 2.2495 0.23 0.03 0.0863 0.0876 5.04 S 1.43E-01 0.190 0.7516 0.7540 2.2262 2.2994 1.05 0.65 0.0815 0.0954 5.04 S 1.44E-01 0.385 0.7405 2.7964 2.2992 2.46 1.54 0.01155 0.1192 1.561 S 1.44E-01 0.385 0.7254 2.1317 2.1157 2.197 2.154 1.54 <	0.082		0.0833				0.093	0.7538	0.7536	2.2543	2,2534	0.16	0.19	1
0.0865 0.0876 504 S 1.48E-01 0.190 0.7505 2.2449 2.2362 0.445 0.62 0.09815 0.0954 5 1.48E-01 0.275 0.7473 0.7474 2.266 2.2084 1.02 1.45 0.09815 0.1034 61.4 5 1.44E-01 0.275 0.7214 2.196 2.2084 1.02 1.45 0.1155 0.1102 1640 0.7725 0.7217 2.1157 2.1157 2.1157 2.1157 2.1157 2.1154 1.02 1.45 0.1315 0.1102 1.750 5 2.75E-02 0.765 0.7097 0.7017 2.1663 2.276 7.13 0.1802 0.1750 0.1750 0.6600 0.6619 1.8618 1.71 1.112 1.112 0.1820 0.1760 0.1760 0.765 0.7657 0.7017 2.1693 2.077 1.112 1.112 0.1820 0.1760 0.1760 0.7017 1.8619	0.083		0.0844	15	S	4.70E-01	0.135	0.7533	0.7527	2,2520	2.2495	0.23	0.30	1
0.08915 0.0894 504 S 1.42E-01 0.275 0.7473 0.7264 2.202 2.2020 1.00 1.19 1.54 0.0893 0.1034 614 S 1.14E-01 0.385 0.7405 0.7344 2.1367 2.146 3.92 2.441 0.1155 0.1190 2.881 S 2.75E-02 0.765 0.7784 0.7217 2.1347 2.1457 3.92 2.441 0.1801 0.1725 1.75C 0.765 0.7784 0.7217 2.1377 2.1430 1.8933 9.71 1.123 0.1824 0.1908 3837 S 1.42E-02 1.305 0.6639 0.6463 1.8499 1.8491 1.8481 1.240 1.440 0.1824 0.1806 0.1602 0.0509 0.6639 0.6639 1.8489 1.8481 1.8481 1.8491 1.8481 1.8481 1.8491 1.8481 1.8481 1.8481 1.8481 1.8481 1.8481 1.8481 1.8481 1.848	0.085	_	0.0876	504	S	1.43E-01	0.190	0.7516	0.7503	2.2449	2.2392	0.45	0.62	1
0.09893 0.1034 614 S 1.14E-01 0.385 0.7405 2.1968 2.1791 2.197 2.246 0.1155 0.1192 1.561 S 4.37E-02 0.550 0.7274 2.117 2.1157 3.92 4.41 0.1155 0.1490 1.381 S 4.37E-02 0.7054 0.7012 2.0639 2.0272 6.00 1.1123 0.1400 0.1720 1.200 0.8617 0.6751 1.6702 1.3400 1.1123 0.1802 0.1905 866 S 6.19E-02 1.305 0.6519 1.8061 1.8143 1.391 1.366 0.1820 0.1862 866 S 6.19E-02 1.305 0.6559 1.8489 1.8618 1.250 1.220 0.1820 0.1730 3110 S 1.77E-02 0.6559 0.6659 1.8489 1.8618 1.250 1.250 0.1566 0.1862 3246 S 4.2EE-04 0.165 0.6659 1.	0.088	_	0.0954	504	S	1.42E-01	0.275	0.7473	0.7434	2.2262	2.2094	1.02	12,	1
0.1155 0.1192 1.561 S 4.37E-02 0.550 0.7254 0.7217 2.1317 2.1157 3.92 4.41 0.1315 0.1400 2.381 S 2.75E-02 1.096 0.06817 0.7702 1.993 2.0772 6.00 7.13 0.1893 0.1400 2.381 S 1.45E-02 1.525 0.6539 0.6702 1.8933 3.71 1.123 0.1802 0.1905 866 S 6.19E-02 1.525 0.6599 0.6659 1.8061 1.8143 13.91 13.66 0.1824 0.1662 886 S 6.19E-02 1.505 0.6659 0.6659 1.8489 1.8481 13.91 13.66 0.1820 0.1662 886 S 6.82E-03 0.330 0.6854 0.6659 1.8489 1.8481 12.50 1.550 0.1820 0.1662 882E-03 0.653 0.6854 1.8682 1.8481 1.361 1.250 1.250 1.250 <t< td=""><td>960'0</td><td></td><td>0.1034</td><td>614</td><td>S</td><td>1.14E-01</td><td>0.385</td><td>0.7405</td><td>0.7364</td><td>2.1968</td><td>2.1791</td><td>1.92</td><td>2.46</td><td>0.00303</td></t<>	960'0		0.1034	614	S	1.14E-01	0.385	0.7405	0.7364	2.1968	2.1791	1.92	2.46	0.00303
0.1315 0.1400 2381 S 2.75E-02 0.765 0.7097 0.7012 2.0639 2.0272 6.00 7.13 0.1893 0.1725 1.750 S 3.49E-02 1.090 0.6617 1.6702 1.8933 9.71 11.23 0.1893 0.1968 3837 S 6.19E-02 1.305 0.6559 1.8255 1.8933 9.71 11.23 0.1820 0.1968 8.61 S 6.19E-02 1.305 0.6559 1.8469 1.8461 1.391 1.326 0.1820 0.1662 8854 S 6.82E-04 0.165 0.6559 0.6659 1.8469 1.8461 1.240 1.220 0.1866 0.1662 8854 S 6.82E-04 0.165 0.6859 1.9659 1.9664 9.41 9.21 9.21 0.1563 0.1562 0.6853 0.6854 0.6854 1.9659 1.9659 9.21 9.21 1.220 0.1563 0.1563 0.6854	0.104		0.1192	1561	S	4.37E-02	0.550	0.7254	0.7217	2.1317	2.1157	3.92	4.41	0.00033
0.1610 0.1725 1750 S 3.49E-02 1.090 0.6817 0.6702 1.8430 1.8933 9.71 11.23 0.1893 0.1988 3837 S 1.4ZE-02 1.525 0.6538 0.6463 1.8055 1.7802 1.340 14.40 0.1924 0.1905 3810 S 6.19E-02 1.305 0.6559 0.6459 1.8061 1.8143 13.91 13.66 0.1820 0.1780 3816 S 6.19E-02 0.0559 0.6629 1.8469 18618 12.60 10.53 0.1578 0.1563 0.1865 0.839 0.6854 0.6854 1.9691 1.969 1.220 0.1563 0.1569 0.1664 0.186 0.8855 0.6854 1.9691 1.969 9.21 1.520 0.1563 0.1569 0.1864 0.1864 0.1864 1.9691 1.969 9.21 1.220 0.1569 0.1669 0.6892 0.6884 0.6854 0.6854	0.119		0.1400	2381	S	2.75E-02	0.765	0.7097	0.7012	2.0639	2.0272	6.00	7.13	0.00649
0.1968 0.1968 3937 S 1.42E-02 1.525 0.6538 0.6463 1.8225 1.7902 13.40 14.40 0.1924 0.1965 866 S 6.19E-02 1.305 0.6509 0.6519 1.8061 1.8143 13.91 13.66 0.1820 0.1730 3110 S 1.77E-02 0.6559 0.6599 0.6675 1.9059 19162 10.85 0.1676 0.1662 1.8862 S 4.25E-04 0.165 0.6854 1.9689 1.9162 10.85 0.1576 0.1662 1.662 0.330 0.6854 0.6854 1.9699 9.21 12.50 0.1563 0.1660 8 9.99E-01 0.190 0.6852 0.6834 1.9699 9.21 9.21 0.1563 0.1660 8 9.99E-01 0.190 0.6852 0.6834 1.9699 9.21 1.250 0.1564 0.1662 8 9.99E-01 0.190 0.6852 0.6834 <td< td=""><td>0.141</td><td></td><td>0.1725</td><td>1750</td><td>တ</td><td>3.49E-02</td><td>1.090</td><td>0.6817</td><td>0.6702</td><td>1.9430</td><td>1.8933</td><td>9.71</td><td>11.23</td><td>0.00788</td></td<>	0.141		0.1725	1750	တ	3.49E-02	1.090	0.6817	0.6702	1.9430	1.8933	9.71	11.23	0.00788
0.1924 0.1905 866 S 6.19E-02 1.305 0.6500 0.6519 1.8061 1.8143 13.91 13.66 0.1820 0.1780 3110 S 1.77E-02 0.6559 0.6599 0.6675 1.9069 1.8469 1.8161 12.20 0.1820 0.1762 3834 S 4.25E-04 0.165 0.6639 0.6854 1.9069 1.9162 10.153 0.1563 0.1563 6.0589 0.6875 1.9069 1.9162 9.41 9.21 0.1565 0.1569 6.0 S 9.99E-01 0.190 0.6852 1.9581 1.9581 1.9162 9.21 0.1565 0.1569 6.0 S 2.49E-01 0.190 0.6852 0.6854 1.9581 1.9581 9.21 0.1575 0.1580 2.40 S 2.49E-01 0.795 0.6872 1.9581 1.9495 9.21 1.959 0.1576 0.1682 0.1864 0.6872 0.6842 <t< td=""><td>0.172</td><td></td><td>0.1968</td><td>3937</td><td>S</td><td>1.42E-02.</td><td>1.525</td><td>0.6538</td><td>0.6463</td><td>1.8225</td><td>1.7902</td><td>13.40</td><td>14.40</td><td>0.00833</td></t<>	0.172		0.1968	3937	S	1.42E-02.	1.525	0.6538	0.6463	1.8225	1.7902	13.40	14.40	0.00833
0.1820 0.1790 3110 S 1.77E-02 0.6559 0.6529 1.8489 1.8618 1.260 12.20 0.1686 0.1662 8854 S 6.82E-03 0.330 0.6731 0.6755 1.9059 1.9162 10.85 10.53 0.1563 0.1563 0.1563 0.6834 0.8655 1.9564 9.41 9.21 9.21 0.1563 0.1563 0.1569 0.1664 0.1664 0.6854 0.6842 1.9561 1.9564 9.21 9.22 0.1564 0.1569 2.49E-01 0.190 0.6862 1.9581 1.9564 9.25 9.30 0.1574 0.1564 0.1684 1.9681 1.9681 1.9684 9.87 1.9564 9.21 9.21 0.1574 0.1684 1.9862 1.987 1.9681 1.9680 9.87 1.9561 1.9561 1.958 1.957 0.1584 0.1684 1.9861 1.9862 1.987 1.9680 9.21 9.21	0.196		0.1905	866	ဟ	6.19E-02	1.305	0.6500	0.6519	1.8061	1.8143	13.91	13.66	1
0.1686 0.1662 8354 S 6.82E-03 0.330 0.6731 0.6755 1.9059 1.9162 10.53 0.1578 0.1652 138652 S 4.25E-04 0.165 0.6839 0.6855 1.957 1.9594 9.41 9.21 0.1563 0.1563 0.1563 0.6842 0.6854 1.9584 1.9594 9.21 9.22 0.1563 0.1586 0.1586 0.6842 0.6842 1.9584 1.9594 9.21 9.21 0.1576 0.1584 0.1684 1.9564 1.9564 1.9564 9.23 9.31 0.1584 0.1685 0.0842 0.6842 0.6842 0.8932 1.9499 9.63 9.81 0.1580 0.1684 1.982 5 2.49E-01 0.275 0.6842 1.9684 1.9694 9.23 9.81 0.1584 0.1616 0.775 0.6842 0.6842 1.9684 1.9694 10.78 1.193 0.1746 0.1773	0.190		0.1790	3110	တ	1.77E-02	0.655	0.6599	0.6629	1.8489	1.8618	12.60	12.20	1
0.1578 0.1562 S 4.25E-04 0.165 0.6839 0.8855 1.957 1.9594 9.41 9.21 9.22 0.1563 0.1563 0.1563 0.6854 0.6854 1.9581 1.9584 9.41 9.21 9.22 0.1563 0.1563 0.6854 0.6854 1.9584 1.9584 9.25 9.30 0.1575 0.1586 2.49E-01 0.785 0.6862 0.6848 1.9584 1.9495 9.33 9.87 0.1584 0.1612 375 2.49E-01 0.285 0.6823 0.8836 1.9495 9.38 9.87 0.1584 0.1612 375 2.49E-01 0.385 0.6823 0.6836 1.9496 1.938 9.63 9.87 0.1584 0.1612 375 2.41E-02 0.785 0.6678 0.6836 1.8061 1.078 1.193 0.1880 0.1920 3.110 \$ 2.41E-02 1.090 0.6547 0.6507 1.8264 1.8075	0.178		0.1662	8354	တ	6.82E-03	0.330	0.6731	0.6755	1.9059	1.9162	10.85	10.53	1
0.1563 0.1563 0.1563 0.6854 0.8854 1.9591 1.9592 9.21 9.22 0.1565 0.1586 6.0848 1.9581 1.9564 9.25 9.30 9.21 0.1575 0.1585 2.498-01 0.189 0.6652 0.6848 1.9581 1.9495 9.25 9.30 0.1584 0.1684 0.1884 0.1884 1.9861 1.9495 9.63 9.51 0.1684 0.1684 1.986 1.9495 9.63 9.63 9.51 0.1684 0.1684 1.986 0.6873 0.6873 1.9495 9.63 9.87 0.1684 0.1684 1.986 0.6873 1.9486 1.987 9.63 9.87 0.1686 0.1684 1.986 1.686 0.6676 0.6676 1.988 1.074 1.078 0.1800 0.2861 2.266-0.2 0.785 0.6676 0.6676 1.8694 1.8076 1.948 0.2000 3.111 2.266-0.2	0.166		0.1562	138652	s	4.25E-04	0.165	0.6839	0.6855	1.9527	1.9594	9.41	9.21	1
0.1565 0.1569 60 S 9.99E-01 0.190 0.6862 0.6848 1.9581 1.9584 9.25 9.30 0.1575 0.1585 2.40 S 2.49E-01 0.275 0.6842 0.6832 1.9584 1.9495 9.38 9.51 0.1584 0.1684 1.382 0.6832 1.9589 1.9495 9.38 9.51 0.1584 0.1684 1.382 0.6832 0.6832 0.6832 1.9486 1.9378 9.63 9.51 0.1584 0.1782 2.66E-02 0.5650 0.6676 0.6837 1.9880 10.44 10.78 0.1800 0.1920 2.20E-02 0.6847 0.6697 1.8024 13.81 11.93 0.1800 0.2641 0.5807 1.8067 1.577 1.7457 15.09 15.76 0.2500 0.2641 0.2560 0.5807 1.3641 1.278 2.19 0.2801 0.2802 3.840 5.275 0.5849 0.5849	0.156		0.1563			90	0.135	0.6854	0.6854	1.9591	1.9590	9.21	9.22	1
0.1575 0.1885 240 S 2.49E-01 0.275 0.6842 0.8832 1.9538 1.9495 9.38 9.51 0.1594 0.1612 375 S 1.59E-01 0.385 0.6803 1.9496 1.9378 9.63 9.87 0.1584 0.1614 375 S 4.55E-02 0.550 0.6762 0.6793 1.9496 1.9378 9.63 9.87 0.1586 0.1684 1.381 1.980 0.674 0.6792 1.980 1.158 1.138 0.1890 0.1773 2.166 2.066 0.6649 1.802 1.139 1.138 0.180 0.180 2.41E-02 1.085 0.6649 1.802 1.139 1.381 0.200 0.260 0.180 0.6649 1.802 1.381 1.381 0.200 0.260 0.260 1.806 1.7677 1.7457 1.59 1.381 0.200 0.264 0.260 1.586 1.584 1.576	0.156		0.1569	9	တ	9.99E-01	0.190	0.6852	0.6848	1.9581	1.9564	9.25	9.30	1
0.1594 0.1612 375 S 1.59E-01 0.385 0.6823 0.6805 1.9456 1.9378 9.63 9.87 0.1658 0.1684 1.382 S 4.25E-02 0.550 0.6762 0.6736 1.9193 1.9090 10.44 10.78 0.1736 0.1773 2.160 S 2.64E-02 0.765 0.6767 0.6736 1.9193 1.9090 10.44 10.78 0.1880 0.1737 2.166 S 2.41E-02 1.090 0.6547 0.6597 1.8264 18821 18705 11.58 11.93 0.2004 0.2069 3.110 S 1.14E-02 2.625 0.6597 1.7677 1.7457 15.09 15.76 0.2500 0.2641 4.236 0.5569 0.5569 1.5677 1.7457 15.09 15.76 0.3014 0.2665 3.840 5 2.64E-03 3.526 0.5569 0.5569 1.5678 21.19 21.96 0.2578 <	0.156		0.1585	240	တ	2.49E-01	0.275	0.6842	0.6832	1,9538	3495	9.38	9.51	ı
0.1658 0.1884 1382 S 425E-02 0.550 0.6762 0.6736 1.9183 1.9080 10.44 10.78 0.1746 0.1773 2160 S 2.66E-02 0.765 0.6676 0.6649 1.8021 1.8705 11.58 11.93 0.1880 0.1920 2.206E-02 0.765 0.6677 0.6677 1.8705 11.58 11.93 0.2018 0.1920 2.206 2.6677 0.6677 1.8767 1.7877 1.787 1.787 0.2100 0.2641 4.236 0.5809 1.5687 1.5078 2.19 2.06 0.3111 0.3211 4800 5.275 0.5358 0.5891 1.5687 1.5078 2.13 2.19 2.06 0.311 0.2065 3840 5.275 0.5368 0.5661 1.4396 1.449 2.725 0.2656 0.5661 1.4496 2.729 0.2662 0.5891 0.5661 1.4496 2.119 2.203 0.2662 0.5891 </td <td>0.158.</td> <td></td> <td>0.1612</td> <td>375</td> <td>S</td> <td>1.59E-01</td> <td>0.385</td> <td>0.6823</td> <td>0.6805</td> <td>1.9456</td> <td>1.9378</td> <td>9.63</td> <td>9.87</td> <td></td>	0.158.		0.1612	375	S	1.59E-01	0.385	0.6823	0.6805	1.9456	1.9378	9.63	9.87	
0.1746 0.1773 2160 S 2.66E-02 0.765 0.6676 0.6649 1.8821 1.8705 11.58 11.38 0.1880 0.1920 2.24E-02 1.090 0.6547 0.6507 1.8705 11.58 11.38 0.2018 0.1920 2.206 2.657 0.6577 1.7877 1.7877 1.7877 1.587 1.381 0.2100 0.2500 0.2641 0.6590 1.7677 1.7877 1.7877 1.5767	0.161		0.1684	1382	S	4.25E-02	0.550	0.6762	0.6736	1,9193	1.9080	10.4	10.78	0.00176
0.1880 0.1920 2306 S 241E-02 1.090 0.6547 0.6507 1.8264 1.8092 13.38 13.81 0.2018 0.2069 3110 S 1.71E-02 1.525 0.6411 0.6560 1.7647 1.7457 15.09 15.76 0.2500 0.2641 4234 S 1.14E-02 2.625 0.5890 0.5808 1.5687 1.5078 21.19 23.06 0.3111 0.3211 6000 S 6.63E-03 5.275 0.5368 0.5891 1.3671 27.09 25.03 30.36 0.2808 0.2965 3.840 S 2.64E-03 1.305 0.5641 0.5661 14.436 25.18 25.02 0.2878 0.272 1.305 0.5649 0.5661 1.5887 1.5078 25.18 25.02 0.2429 0.2429 1.6067 0.6028 0.6028 0.6028 1.6067 20.03 20.03 0.2204 0.2204 0.0280 0.6028	0.168		0.1773	2160	S	2.66E-02	0.765	0.6676	0.6649	1.8821	1.8705	11.58	11.93	0.00265
0.2018 0.2069 3110 S 1.71E-02 1.525 0.6411 0.6360 1.7677 1.7457 15.09 15.76 0.2500 0.2661 4234 5 1.14E-02 2.625 0.5569 1.5687 1.5078 21.19 23.06 0.3111 0.3211 6000 5 6.63E-03 5.275 0.5569 1.5687 1.5078 21.19 23.06 0.2804 0.2965 3.340 5 2.5EE-03 4.390 0.5644 0.5493 1.3503 1.3744 27.89 25.18 0.2878 0.2797 4.4978 5 2.644E-03 4.390 0.5643 0.5641 1.4386 25.18 25.02 0.2878 0.2797 4.497 5 2.648E-03 0.5649 0.5661 1.5415 22.11 22.03 0.2429 0.2429 0.2429 0.6028 0.6028 0.6028 1.6067 20.03 20.03 0.2204 0.2204 0.080 0.6028 0.6028	0.177		0.1920	2306	တ	2.41E-02	060	0.6547	0.6507	1.8264	1.8092	13.28	13.81	0.00394
0.2500 0.2641 4234 S 1.14E-02 2.625 0.5950 0.5809 1.5687 1.5078 21.19 23.06 0.3111 0.3211 6000 S 6.63E-03 5.275 0.5558 0.5558 1.3131 1.2700 29.03 30.36 0.3014 0.2965 3.344 0.5493 0.5494 0.5493 1.3503 1.3714 27.89 27.25 0.2878 0.2797 14978 S 2.64E-03 0.5649 0.5661 1.5436 2.4149 22.11 22.03 0.2878 0.2797 4.3976 0.5649 0.5661 1.588 1.5436 22.11 22.03 0.2479 0.2429 2.244 0.5887 1.536 1.5436 22.11 22.03 0.2415 0.2415 0.2415 0.06028 0.6028 0.6038 1.6067 20.03 20.03 0.2204 0.2204 0.080 0.6028 0.6028 1.6067 1.6067 20.03 20.03	0.192		0.2069	3110	တ	1.71E-02	1.525	0.6411	0.6360	1.7677	1.7457	15.09	15.76	0.00606
0.3111 0.3211 6000 S 6.63E-03 5.275 0.5358 0.5258 1.3131 1.2700 29.03 30.36 0.3014 0.2965 3840 S 9.52E-03 4.390 0.5444 0.5493 1.3503 1.3714 27.89 27.25 0.2809 0.2797 14978 S 2.64E-03 1.305 0.5649 0.5661 1.4386 1.4439 25.18 25.02 0.2429 0.2429 0.5627 0.5881 0.5887 1.5389 1.5415 22.01 22.03 0.2429 0.2429 0.5628 0.6028 0.6028 0.6028 1.6024 20.16 20.03 0.2415 0.2415 0.2429 0.6028 0.6028 0.6028 1.6067 20.03 20.03 0.2204 0.2204 0.6226 0.6038 0.6028 0.6038 0.6038 0.6038 0.6038 0.6038 0.6039 0.6039 0.6039 0.6039 0.6039 0.6039 0.6039 0.6039	0.209		0.2641	4234	ဟ	1.14E-02	2.625	0.5950	0.5809	1.5687	1.5078	21.19	23.06	0.00960
0.3014 0.2965 3840 S 9,52E-03 4,390 0.5444 0.5493 1.374 27,89 0.2809 0.2797 14978 S 2,64E-03 1,305 0,5649 0,5661 1,4396 1,4396 25,18 0.2429 0.2429 0,5887 1,5387 1,5399 1,5415 22,11 0.2415 0,2429 0,2429 0,665 0,6981 0,5887 1,5415 22,11 0,2415 0,2415 0,2415 0,652 0,6938 0,6038 1,6024 1,6067 20,03 0,2204 0,2204 0,6246 0,6246 1,6067 1,6067 20,03	0.266		0.3211	9009	တ	6.63E-03	5,275	0.5358	0.5258	1.3131	1.2700	29.03	30.36	0.01018
0.2809 0.2797 14978 S 2.64E-03 1.305 0.5649 0.5661 1.4396 1.4439 25.18 0.2578 0.2572 0.2429 0.2655 0.5887 1.5399 1.5415 22.11 0.2429 0.2429 0.6028 0.6028 0.6028 1.6024 1.6024 20.16 0.2415 0.2415 0.665 0.663 0.6038 0.6038 1.6067 1.6067 20.16 0.2204 0.2204 0.204 0.6246 0.6246 1.6965 1.6965 17.27	0.320		0.2965	3840	တ	9,52E-03	4.390	0.5444	0.5493	1.3503	1.3714	27.89	27.25	1
0.2578 0.2572 0.655 0.5881 0.5887 1.5389 1.5415 22.11 0.2429 0.2429 0.330 0.6028 0.6028 1.6024 1.6024 20.16 0.2415 0.2415 0.2415 0.65 0.653 0.6038 1.6067 1.6067 20.03 0.2204 0.2204 0.2204 0.6546 0.6246 1.6965 1.6965 17.27	0.296		0.2797	14978	တ	2,64E-03	1.305	0.5649	0.5661	1.4386	1.4439	25.18	25.02	1
0.2429 0.2429 0.2429 0.2429 0.2429 0.2429 0.2429 0.2415 0.2415 0.2415 0.2415 0.2504 0.6528 0.6538 0.6038 0.6038 0.6038 0.6038 0.6038 0.6038 0.6047 0.003 0.2204 0.2204 0.2204 0.6246 0.6246 0.6246 1.6965 1.6965 17.27	0,279		0.2572				0,655	0.5881	0.5887	1.5389	1.5415	22.11	22,03	1
0.2415 0.2415 0.2204 0.	0.257		0.2429				0.330	0.6028	0.6028	1.6024	1.6024	20.16	20.16	1
0.2204 0.2204 1.6965 1.6965 17.27	0.242		0.2415				0.165	0.6038	0.6038	1.6067	1.6067	20.03	20.03	1
	0.241		0.2204	•			0.080	0.6246	0.6246	1.6965	1,6965	17.27	17.27	1

dation	rement (typically 24 hrs +/-)		2.743	2.0000	62.50	0.2316	32.71
EOP= End of Primary Consolidation	EOI= End of load increment (t)		Specific Gravity	Ring Diameter (In)	Ring weight (g)		Weight of Dry Soil (g)
Final	Conditions	0.6222	62.4	103.5	63.8	101.5	1.6861
Initial	Conditions	0.7550	78.1	93.6	52,5	94.9	2.2594
		Height (in)	Wc (%)	yt (pct)	7d (pct)	Saturation (%)	Void ratio, e
	Oyster Bayon	12-80-3741	8 0	0-2 (1.75)			
	Project Name:	File Number:	Boring Number:	Depth:			



VERTICAL EFFECTIVE STRESS, $\sigma^{\scriptscriptstyle t}_{\ vc}$ (tsf)

SAMPLE DATA	
BORING NO.:	B-01
SAMPLE NO.:	
DEPTH (FEET):	24.5
DESCRIPTION	Gray SILTY CLAY (CL)
INDEX PROPERTIES	
LIQUID LIMIT (%):	47
PLASTIC LIMIT (%):	12
PLASTICITY INDEX (%):	35
SPECIFIC GRAVITY:	2.69
-200(%)	60

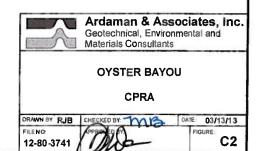
SPECIMEN CONDITIONS	INITIAL	FINAL
MOISTURE CONTENT (%):	23.5	20.4
DRY DENSITY (lb/ft3):	101.0	109.8
VOID RATIO	0.66	0.53

CONSOLIDATION PARAMETERS

EFFECTIVE OVERBURDEN STRESS, o'vo (tsf):	0.52
PRECONSOLIDATION PRESSURE, o'p (tsf):	2.05
VIRGIN COMPRESSION RATIO, CR:	0.152

INCREMENTAL CONSOLIDATION TEST RESULTS

Confidential Information: Privileged & Confidential Work Product



L INCREMENTAL LOADING CONSOLIDATION TEST SUMMARY SHEET		Void Void Strain at Strain at EOP (%) EOI (%)	0.6636 0.6636 0.00 0.00	0.6603 0.6592 0.20 0.27	0.6540 0.6523 0.58 0.68 0.00047	0.6415 0.6370 1.33 1.60 0.00124	0.6156 0.6084 2.89 3.32 0.00213	0.5689 0.5627 5.69 6.07 0.00288	0.5137 0.5066 9.01 9.44	0.4547 0.4469 12.56 13.03 0.00494	0.3970 0.3888 16.03 16.52 0.00505	0.3999 0.4023 15.85 15.71	0.4434 0.4480 13.24 12.96	0.5048 0.5048 9.55 9.55
TION 1		Height at EOI (inch)	0.7500	0.7480	0.7449	0.7380	0.7251	0.7045	0.6792	0.6523	0.6261	0.6322	0.6528	0.6784
SOLIDA		Height at EOP (inch)	0.7500	0.7485	0.7457	0.7400	0.7284	0.7073	0.6824	0.6558	0.6298	0.6311	0.6507	0.6784
NG CON		Average Effective Stress (tsf)		0.118	0.330	0.655	1.305	2.625	5.275	10.570	21.230	17.700	4.390	1.090
L LOADII		Cv (ft²/day)			2.76E-01	2.72E-01	2.66 E -01	6.34E-02	3.71E-02	2.20E-02	1.56E-02	3.91E-02	3.70E-03	
MENTA		Method (L=log, S=sq rt)				_	_	_	_	_	_	_	_	
INCRE		Time, t ₁₀₀ (sec)			9	8	9	240	384	009	780	300	3300	
	ich)	EOI	0.0301	0.0321	0.0361	0.0446	0.0597	0.0823	0.1097	0.1390	0.1682		0.1366	0.1115
ONE-DIMENSIONA	Dial Readings (inch)	EOP	0.0301	0.0316	0.0354	0.0426	0.0565	0.0795	0.1065	0.1355	0.1645	0.1596	0.1387	0.1115
ONE	Dial R	Initial	0.0301	0.0301	0.0330	0.0377	0.0468	0.0617	0.0844	0.1121	0.1420	0.1646	0.1572	0.1371
		Effective Stress (tsf)	0	0.220	0.440	0.870	1.740	3.510	7.040	14.100	28.360	7.040	1.740	0.440

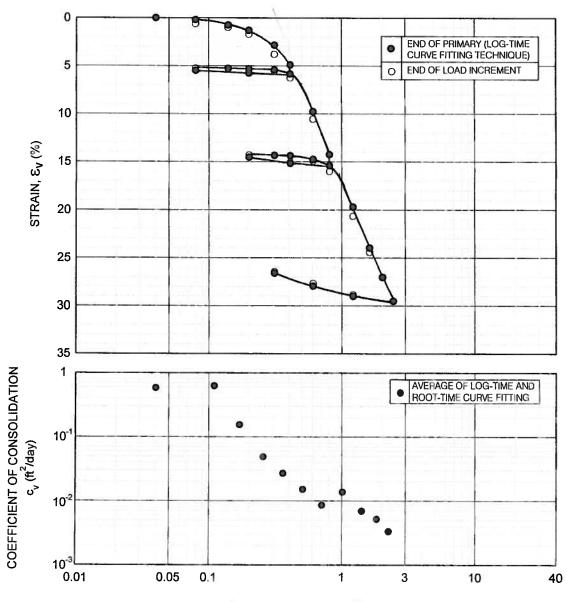
EOP= End of Primary Consolidation	EOI= End of load increment (typically 24 hrs +/-)		Specific Gravity 2,6925	Ring Diameter (in) 2.0000	Ring weight (g) 62.40	Height of Solids (in) 0.4508	Weight of Dry Soil (g) 62.49
Final	Conditions	0.6900	20.4	132.2	109.8	103.5	0.5305
Initial	Conditions	0.7500	23.5	124.8	101.0	95.5	0.6636
		Height (in)	Wc (%)	γt (pcf)	γ d (pct)	Saturation (%)	Void ratio, e
	Oyster Bayou	12-80-3741	B-01	23-25 B2 (24.5)			
	Project Name:	File Number:	Boring Number:	Depth:			

ARDAMAN & ASSOCIATES, INC

GEOTECHNICAL TESTING LABORATORY

		စ ပ	İ	,	•	0.00047	0.00124	0.00213	0.00288	0.00359	0.00494	0.00505	,	1	,					
H		Strain at EOI (%)		0.00	0.27	0.68	1.51	2.91	5.56	8.88	12.35	15.84	15.29	12.84	9.49				,	
Y SHEE		Strain at EOP (%)		0.0	0.20	0.52	1.12	2.29	4.28	7.40	10.77	14.37	15.72	13.56	9.93	*********		-		
MMAR		Void Ratio at	Š	0.6636	0.6592	0.6523	0.6386	0.6153	0.5711	0.5159	0.4582	0.4001	0.4092	0.4500	0.5057					
EST SU		Void Ratio at	វ្ន	0.6636	0.6603	0.6550	0.6450	0.6255	0.5924	0.5405	0.4844	0.4245	0.4021	0.4380	0.4984	(*)				
TION		Height at EOI		0.7500	0.7480	0.7449	0.7387	0.7282	0.7083	0.6834	0.6574	0.6312	0.6353	0.6537	0.6788					
SOLIDA:		Height at EOP		0.7500	0.7485	0.7461	0.7416	0.7328	0.7179	0.6945	0.6692	0.6422	0.6321	0.6483	0.6755					
NO CON		Average Effective	(ISI) SEBIIO	-	0.110	0.220	0.435	0.870	1.755	3.520	7.050	14.180	3.520	0.870	0,220					
GEOTECHNICAL TESTING LABORATORY INCREMENTAL LOADING CONSOLIDATION TEST SUMMARY SHEET		Cv (ft²/day)				4.45E-01	7.05E-01	3.45E-01	2.09E-01	1.49E-01	6.56E-02	3.91E-02	1.08E-01	4.74E-03	1.76E-03					
MENTA		Method (L=log,	(1) be-0			တ	တ	တ	တ	တ	တ	S	S	S	S			-		-
GENCRE		Time, t ₁₀₀ (sec)				160	100	200	320	420	890	1380	470	11098	32017					
	(hot		EOI	0.0301										0.1366	0.1115					
ONE-DIMENSIONAL	Dial Readings (inch)		EOP	0.0301	0.0316	0.0349	0.0417	0.0551	0.0727	0.0986	0.1272	0.1572	0.1617	0.1420	0.1148				- *	
ONE	Dial F		nitia	0.0301	0.0301	0.0330	0.0384	0.0492	0.0624	0.0848	0.1130	0.1420	0.1626	0.1550	0.1366					
		Effective Stress	<u> </u>	0	0.220	0.440	0.870	1.740	3.510	7.040	14.100	28.360	7.040	1.740	0.440					

solidation It (typically 24 hrs +/-)	ly 2.6925	2.0000 (۱	j) 62.40) 0.4508 j) 62.49
EOP= End of Primary Consolidation EOI= End of load increment (typically 24 hrs +/-)	Specific Gravity 2,6925	Ring Diameter (in)	Ring weight (g)	Height of Solids (in) Weight of Dry Soil (g)
Final Conditions	20.4	132.2	109.8	103.5 0.5305
Initial Conditions	23.5	124.8	101.0	95.5 0.6636
	meignit (in) w _c (%)	γt (pcf)	γ d (pct)	Saturation (%) Void ratio, e
Oyster Bayou	B-01	23-25 B2 (24.5)		
Project Name:	Boring Number:	Depth:		



VERTICAL EFFECTIVE STRESS, σ'_{vc} (tsf)

SAMP	LE	DA	T/	١

BORING NO.:

B-02

SAMPLE NO.: DEPTH (FEET):

3.5

DESCRIPTION:

Gray CLAY (CH)

w/silt and trace organics

INDEX PROPERTIES

LIQUID LIMIT (%): 70 PLASTIC LIMIT (%): 21 PLASTICITY INDEX (%): 49 SPECIFIC GRAVITY: 2.67 -200(%): 97 ORGANIC CONTENT (%): 5.24

SPECIMEN CONDITIONS	INITIAL	FINAL
MOISTURE CONTENT (%):	101.4	70.4
DRY DENSITY (lb/ft3):	44.7	61.0
VOID RATIO:	2.73	1.74

CONSOLIDATION PARAMETERS

EFFECTIVE OVERBURDEN STRESS, o'vo (tsf):	0.057
PRECONSOLIDATION PRESSURE, o'p (tsf):	0.34
VIRGIN COMPRESSION RATIO, CR:	0.36
RECOMPRESSION RATIO, RR.	0.03

INCREMENTAL CONSOLIDATION TEST RESULTS

Confidential Information. Privileged & Confidential Work Product



Ardaman & Associates, Inc. Geotechnical, Environmental and Materials Consultants

OYSTER BAYOU

CPRA

FILE NO:

DATE: 03/13/13

12-80-3741

C3

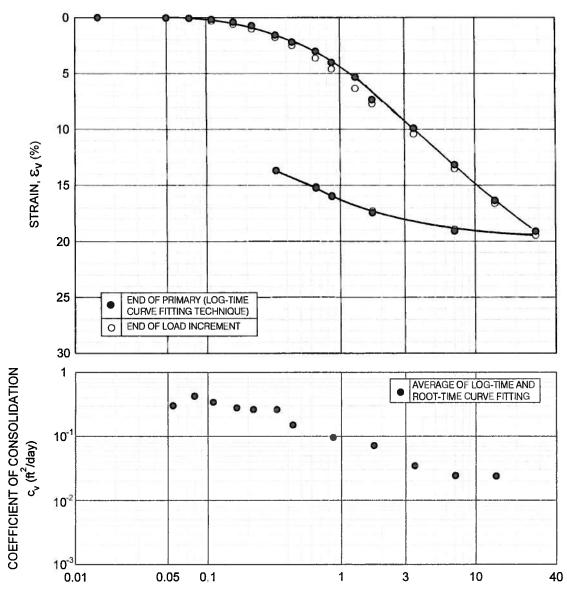
SECTECHNICAL TESTING LABORATORY SUMMARY SHE

	ONE-	DIMENS	NONAL	INCREN	JENTA	ONE-DIMENSIONAL INCREMENTAL LOADING CONSOLIDATION TEST SUMMARY SHEET	NG CON	SOLIDA	TION TE	ST SUI	MMAR	Y SHEE	Ξ.	
	Dia! Re	Dial Readings (inch)	ch)											
Effective Stress (tsf)	Initial	EOP	EOI	Time, t ₁₀₀ (sec)	Method (L=log, S=sq rt)	Cv (ft²/day)	Average Effective Stress (tsf)	Height at EOP (inch)	Height at EOI (inch)	Void Ratio at EOP	Void Ratio at EOI	Strain at EOP (%)	Strain at EOI (%)	Cae
0	0.1540	0.1540	0.1540					0.7500	0.7500	2.7306	2.7306	00.0	00.00	1
080.0	0.1616	0.1630	0.1662	30	_	5.55E-01	0.040	0.7486	0.7454	2.7237	2.7078	0.19	0.61	
0.140	0.1977	0.1987	0.2007	30	_	5.48E-01	0.110	0.7444	0.7425	2.7028	2.6931	0.75	1.01	0.00072
0.200	0,2112	0.2134	0.2166	120	_	1.36E-01	0.170	0.7403	0.7371	2.6821	2.6665	1.30	1.72	0.00219
0.310	0.2169	0.2253	0.2325	480	_	3.32E-02	0.255	0.7287	0.7215	2.6247	2.5889	2.84	3.80	0.00685
0.410	0.2326	0.2408	0.2479	810	_	1.88E-02	0.360	0.7133	0.7062	2.5481	2.5128	4.89	5.84	0.0082
0.200	0.2474	0.2467	0.2464	2	_	2.31E-01	0.305	0.7068	0.7072	2.5159	2.5177	5.76	5.71	-
0.080	0.2463	0.2446	0.2430	9	_	2.48E-01	0.140		0.7105	2.5264	2.5342	5.47	5.27	1
0.140	0.2433	0.2433	0.2433			Y.	0.110	0.7105	0.7105	2.5342	2.5342	5.27	5.27	1
0.200	0.2433	0.2436	0.2437				0.170	0.7102	0.7101	2.5327	2.5322	5,31	5.32	1
0,310	0.2439	0.2446	0.2458	24	_	6.22E-01	0.255	0.7095	0.7083	2.5289	2.5230	5.41	5.57	0.00023
0.410	0.2459	0.2479	0.2510	78	_	1.90E-01	0.360	0.7062	0.7031	2.5128	2.4974	5.84	6.25	0.00133
0,610	0.2512	0.2775	0.2835	1500	_	9.41E-03	0.510	0.6768	0.6708	2.3663	2.3367	9.77	10.56	0.01382
0.810	0,2835	0.3110	0.3194	1860	_	6.88E-03	0.710	0.6433	0.6349	2.1996	2.1579	14.23	15.35	0.01354
0.410	0.3193	0.3179	0.3170		_	2.85E-01			0.6372	2.1646	2.1693	15.17	15.05	-
0.200	0.3168	0.3129	0.3113	186	_	6.51E-02			0.6426	2.1885	2.1964	14.53	14.32	1
0.310	0.3113	0.3115	0.3115				0.255	0.6425	0.6424	2.1957	2.1954	14.34	14.35	1
0.410	0.3117	0.3119	0.3122	48	_	2.55E-01	0360	0.6422	0.6419	2.1943	2.1927	14.38	14.42	0.00013
0.610	0.3123	0.3147	0.3161	72	_	1.69E-01	0.510	0.6394	0.6381	2.1806	2.1740	14.74	14.92	0.00083
0.810	0.3161	0.3196	0.3243	126		9.53E-02	0.710	0.6346	0.6299	2.1566	2.1332	15.39	16.01	0.00267
1.220	0.3244	0.3520	0.3592	_		1.04E-02	1.015		0.5951	1.9957	1.9601	19.70	20.65	0.01347
1.625	0.3593	0.3840	0.3875	1920	_	5.24E-03	1.423	0.5704	0.5669	1.8370	1.8199	23.95	24.41	i
2.030	0.3876	0.4070	0.4074	3240	_	2.84E-03	1.828		0.5471	1.7231	1.7211	27.01	27.06	1
2.440	0.4076	0.4260	0.4260	4500		1.91E-03	2.235	0.5287	0.5287	1.6296	1.6296	29.51	29.51	1
1.220	0.4256	0.4217	0.4206	108		7.73E-02	1.830	0.5325	0.5337	1.6489	1.6545	29.00	28.85	j
0.610	0.4203	0.4134	0.4114	480	_	1.78E-02	0.915	0.5405		1.6885	1.6985	27.93	27.67	1
0.310	0.4112	0.4032	0.4020	1260	_	7.03E-03	0.460	0.5505	0.5517	1.7383	1.7443	26.60	26.44	1
	•													

EOP= End of Primary Consolidation	EOI= End of load increment (typically 24 hrs +/-)		ific Gravity 2.6735	Ring Diameter (in) 2.0000	Ring weight (g) 62.51	Height of Solids (in) 0.2010	
EOP= End of Pri	EOI= End of load		Spec	Ring Di	Ring	Height of	Weight of
Final	Conditions	0.5500	70.4	104.0	61.0	108.4	1,7358
Initial	Conditions	0.7500	101.4	90.1	44.7	99.3	2.7306
		Height (in)	Wc (%)	7t (pct)	√d (bct)	Saturation (%)	Void ratio, e
	Oyster Bayon	12-80-3741	B-02	2-4 (3.5)			
	Project Name:	File Number:	Boring Number:	Depth:			

	ONE	-DIMENS	SIONAL	INCRE	MENTA	ONE-DIMENSIONAL INCREMENTAL LOADING CONSOLIDATION TEST SUMMARY SHEET	NG CON	SOLIDA	TION TE	ST SU	MMAR	YSHE	ET	
	Dial R	Dial Readings (inch)	ch)											
Effective Stress (tsf)	Initial	ЕОР	EOI	Time, t ₁₀₀ (sec)	Method (L=log, S=sq rt)	Cv (ft²/day)	Average Effective Stress (tsf)	Height at EOP (inch)	Height at EOI (inch)	Void Ratio at EOP	Void Ratio at EOI	Strain at EOP (%)	Strain at EOI (%)	C n e
0	0.1540	0.1540	0.1540				,	0.7500	0.7500	2.7306	2.7306	0.00	00.0	1
080	0.1610	0.1623	0.1662	118	S	6.07E-01	0.040	0.7487	0.7448	2.7242	2.7048	0.17	69.0	
0.140		0.1984	0.2007	101	S	7.00E-01	0.110	0.7441	0.7419	2.7013	2.6901	0.79	1.09	0.00072
0.200		0.2133	0.2166	405	S	1.73E-01	0.170	0.7398	0.7365	2.6797	2.6635	1.37	1.80	0.00219
0.310	0.2168	0.2232	0.2325	1058	S	6.49E-02	0.255	0.7301	0.7208	2.6317	2.5854	2.65	3.89	0.00685
0.410	0.2325	0.2386	0.2479	1882	S	3.49E-02	0.360	0.7147	0.7054	2.5551	2.5088	4.71	5.95	0.0082
0.200	0.2474	0.2468	0.2464	194	S	3.28E-01	0.305	0.7060	0.7064	2,5115	2.5138	5.87	5.81	ı
080.0	0.2461	0.2444	0.2430	406	S	1.57E-01	0.140	0.7081	0.7095	2.5222	2.5292	5.59	5.40	1
0.140	0.2430	0.2433	0.2433				0.110	0.7093	0.7092	2.5279	2.5277	5.43	5.44	1
0.200		0.2437	0.2437				0.170	0.7088	0.7088	2.5255	2,5255	5.50	5.50	
0.310	0.2439	0.2447	0.2458	173	S	3.70E-01	0.255	0.7080	0.7069	2.5216	2.5164	5.60	5.74	0.00023
0.410		0.2476	0.2510	240	S	2.65E-01	0.360	0.7052	0.7018	2.5079	2,4910	5.97	6.42	0.00133
0.610	0.2510	0.2697	0.2835	2940	S	2.08E-02	0.510	0.6831	0.6694	2.3980	2.3296	8.92	10.75	0.01382
0.810	0.2835	0.3060	0.3194	5415	S	1.02E-02	0.710	0.6469	0.6334	2,2177		13.75	15.54	0.01354
0.410	0.3192	0.3178	0.3170	217	S	2.37E-01	0.610	0.6348	0.6357	2.1578		15.36	15.24	1
0.200	0.3167	0.3133	0.3113	735	S	7.05E-02	0.305	0.6391	0.6411	2.1789	2.1889	14.79	14.52	1
0.310		0.3115	0.3115				0.255	0.6409	0.6409	2.1879		14.55	14.55	-
0.410		0.3119	0.3122	194	S	2.70E-01	0,360		0.6403	2.1865		14.59	14.62	0.00013
0.610	0.3124	0,3146	0,3161	290	ဟ	1.80E-01	0.510	0.6381	0.6366	2.1742	2.1668	14.91	15.11	0.00083
0.810	0.3162	0.3196	0,3243	577	S	8.92E-02	0.710		0.6285	2.1499	2.1265	15.57		0.00267
1.220	0.3243	0.3467	0.3592	2857	S	1.70E-02	1.015		0.5937	2.0151	•	19.18		0.01347
1.625	0.3592	0.3789	0.3875	5078	S	8.57E-03	1,423	0.5739	0.5654	1.8549	•	23.47		1
2.030	0.3875	0.4005	0,4074	5302	S	7.52E-03	1,828	0.5523	0.5454	1.7474	•-	26,35		I
2.440	0.4076	0,4186	0.4260	7798	S	4.77E-03	2.235	0.5344	0.5270	1.6584	1.6216	28.74		1
1,220	0.4255	0.4223	0.4208	375	S	9.51E-02	1.830	0.5302	0.5320	1.6375	•	29.30		1
0.610		0.4145	0.4114	1382	S	2.64E-02	0.915	0.5378	0.5409	1.6751		28.29		1
0.310		0.4053	0.4020	2940	S	1.28E-02	0.460	0.5468	0.5501	1.7198	1.7363	27.09	26.65	1

Project Name:	Oyster Bayou		Conditions	Conditions	EOI= End of load increment (typically 24 hrs +/-)	typically 24 hrs +/-)
File Number:	12-80-3741	Height (in)	0.7500	0.5500		
Boring Number:	B-02	w _c (%)	101.4	70.4		2.6735
Depth:	2-4 (3.5)	7t (pct)	90.1	104.0		2.0000
		yd (bcl)	44.7	61.0	Ring weight (9) 62.51	62.51
		Saturation (%)	8.66	108.4		0.2010
		Void ratio. e	2.7306	1.7358		27.67



VERTICAL EFFECTIVE STRESS, $\sigma_{vc}^{'}$ (tsf)

SAMPLE DATA	
BORING NO.:	B- 0 3
SAMPLE NO.:	
DEPTH (FEET):	19.0
DESCRIPTION	Gray SILTYCLAY (CL)
	w/silt pockets
INDEX PROPERTIES	
LIQUID LIMIT (%):	49
PLASTIC LIMIT (%):	14
PLASTICITY INDEX (%)	35

SPECIMEN CONDITIONS	INITIAL	FINAL
MOISTURE CONTENT (%):	23.0	19.3
DRY DENSITY (lb/ft3):	95.7	110.8
VOID RATIO:	0.72	0.49

CONSOLIDATION PARAMETERS

EFFECTIVE OVERBURDEN STRESS, o'vo (tsf):	0.35
PRECONSOLIDATION PRESSURE, o', (isf):	0.80
VIRGIN COMPRESSION RATIO, CR:	0.09

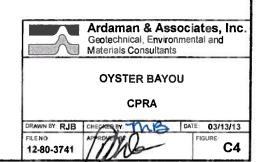
INCREMENTAL CONSOLIDATION TEST RESULTS

2.64

Confidential Information. Privileged & Confidential Work Product

SPECIFIC GRAVITY.

-200(%):

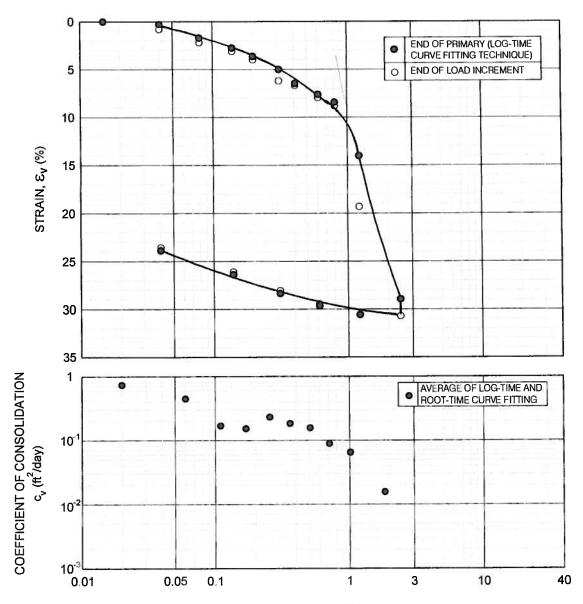


	ONE	ONE-DIMENS		INCRE	MENTA	ONAL INCREMENTAL LOADING CONSOLIDATION TEST SUMMARY SHEET	NG CON	SOLIDA	TION TE	ST SU	MMAR	YSHE	<u></u>	
	Dial R	Dial Readings (incl	(hor											
Effective Stress (tsf)				Time,	Method (L≂log, S=sq rt)	Cv (ft²/day)	Average Effective Stress	Height at EOP (inch)	Height at EOI (inch)	Void Ratio at EOP	Void Ratio at EOI	Strain at EOP (%)	Strain at EOI (%)	O O
	Initial	EOP	<u>G</u>		-		(ISI)							
0	-0.0526	-0.0521	-0.0520					0.7500	0.7500	0.7231	0.7231	0.00	00.0	1
0.050	-0.0482	-0.0480	-0.0478				0.025	0.7498	0.7496	0.7227	0.7222	0.02	0.05	
0.075		-0.0475	-0.0475				0.038	0.7495	0.7495	0.7220	0.7220	0.07	0.07	1
0.110	·	-0.0462	-0.0451	\$	_	3.08E-01	0.055	0.7488	0.7476	0.7203	0.7176	0.17	0.32	0.00042
0.160		-0.0443	-0.0428	42		3.94E-01	0.080	0.7470	0.7455	0.7162	0.7128	0.40	0.60	0.00050
0.220		0.0411	-0.0389	45	۷	3.66E-01	0.110	0.7446	0.7424	0.7107	0.7057	0.72	1.01	0.00102
0.330		-0.0342	-0.0326	09	_	2.71E-01	0.165	0.7383	0.7367	0.6962	0.6926	1.56	1.77	0.00100
0.440		-0.0288	-0.0265	99	٦	2.43E-01	0.220	0.7336	0.7313	0.6853	0.6801	2.19	2.50	0.00181
0.660		-0.0198	-0.0152	54	٦	2.92E-01	0.330	0.7274	0.7228	0.6711	0.6605	3.02	3.63	0.00236
0.870	-0.0120	-0.0091	-0.0047	102	١	1.51E-01	0.435	0.7199	0.7155	0.6540	0.6438	4.01	4.61	0.00273
1.310		0.0032	0.0108	\$		2.79E-01	0.655	0.7100	0.7025	0.6312	0.6139	5.33	6.34	0.00454
1.740		0.0192	0.0220	240	ر	6.03E-02	0.870	0.6950	0.6922	0.5967	0.5902	7.34	7.71	0.00361
3.510		0.0445	0.0484	240	۔۔	5.78E-02	1.755	0.6758	0.6719	0.5526	0.5436	9.30	10.42	0.00392
7.040			0.0746	480		2.70E-02	3.520	0.6513	0.6486	0.4964	0.4901	13.16	13.53	0.00392
14.100			0.1009	750		1.61E-02	7.050	0.6274	0.6255	0.4415	0.4370	16.35	16.61	0.00375
28.360			0.1254	930		1.79E-02	14.180	0.6068	0.6040	0.3940	0.3876	19.10	19.47	0.00459
7,040			0.1177	144	۔۔۔	7.55E-02	3.520	0.6069	0.6080	0.3944	0.3968	19.08	18.94	-
1.740			0.1034	1560	ب	7.16E-03	0.870	0.6193	0.6203	0.4227	0.4252	17.43	17.29	1
0.870		0.0932	0.0927	0099		1.76E-03	0.435	0.6301	0.6306	0.4476	_	15.99	15.92	1
0.660	0.0923	0.0872	0.0865	12300	٢	9.66E-04	0.330	0.6357	0.6365	0.4605	0.4623	15.24	15.14	-
0.330	0.0863	0.0754	0.0754				0.165	0.6474	0.6474	0.4873	0.4873	13.69	13.69	
									9					
			_			_								

EOP= End of Primary Consolidation	EOI= End of load increment (typically 24 hrs +/-)		Specific Gravity 2.6402	Ring Diameter (in) 2.0000	Ring weight (g) 62.48	Height of Solids (in) 0.4353	Weight of Dry Soil (g) 59.16
Final	Conditions	0.6473	19.3	132.3	110.8	104.8	0.4872
Initial	Conditions	0.7500	23.0	117.7	95.7	84.1	0.7231
		Height (in)	Wc (%)	71 (pcf)	yd (bal)	Saturation (%)	Void ratio, e
	Oyster Bayon	12-80-3741	B-03	18-20 (19.0)			
	Project Name:	File Number:	Boring Number:	Depth:			

ı						_	7	_	<u>~</u>	_	_	<u> </u>	က	4	-	<u>~</u>	2	<u>v</u>	<u>ნ</u>						
		O O		1		<u> </u>		0.00050	0.00102	0.00100	0.00181	0.00236			0.00361			0.00375	0.00459		1	1		1	
ET		Strain at EOI (%)		00:00	0.57	0.60	0.85	1.13	1.54	2.38	3.02	4.09	5.07	6.85	8.08	10.72	13.63	16.72	19.53	19.08	17.52	16.14	15.31	13.83	
YSHE		Strain at EOP (%)		00.00	0.55	0.58	0.71	0.91	1.25	2.05	2.72				7.49						18.16	16.32	15.54	13.86	
IMMAR		Void Ratio at EOI		0.7231	0.7134	0.7128	0.7085	0.7037	0.6966	0.6821			0.6358		0.5840	0.5385	0.4883			0.3943	0.4213	0.4451	0.4593	0.4848	
EST SU		Void Ratio at EOP		0.7231	0.7137	0.7132	0.7110	0.7074	0.7015	0.6878	0.6763	0.6635	0.6458		0.5941	0.5543	0.5054			0.3921	0.4102	0.4420	0.4553	0.4843	
TION TI		Height at EOI (inch)		0.7500	0.7458	0.7455	0.7436	0.7415	0.7384	0.7321	0.7273	0.7193	0.7120	0.6986	0.6894	0.6696	0.6478	0.6246	0.6035	0.6069	0.6186	0.6290	0.6352	0.6463	
SOLIDA		Height at EOP (inch)		0.7500	0.7459	0.7457	0.7447	0.7432	0.7406	0.7346	0.7296	0.7240	0.7163	0.7051	0.6938	0.6765	0.6552	0.6400	0.6105	0.6059	0.6138	0.6276	0.6334	0.6460	
NG CON		Average Effective Stress	(iei)		0.025	0.038	0.055	0.080	0.110	0.165	0.220	0.330	0.435	0.655	0.870	1.755	3.520	7.050	14.180	3.520	0.870	0.435	0.330	0.165	
ONAL INCREMENTAL LOADING CONSOLIDATION TEST SUMMARY SHEET		Cv (ft²/day)					2.95E-01	4.58E-01	3.23E-01	2.88E-01	2.84E-01	2.32E-01	1.50E-01	2.21E-01	1.32E-01	8.58E-02	4.23E-02	3.26E-02	3.00E-02	3.84E-02	1.41E-02	1.56E-03	1.60E-03	8.52E-04	
MENTA		Method (L=log, S=sq rt)					S	S	S	S	S	S	S	S	S	S	S	S	S	S	S	ဟ	S	ဟ	
INCRE		Time, t ₁₀₀ (sec)					240	154	217	240	240	290	437	290	470	694	1325	1622	1622	1215	3375	31740	31740	61440	
	ich)		Ö	-0.0520	-0.0478	-0.0475	-0.0451	-0.0428	-0.0389	-0.0326	-0.0265	-0.0152	-0.0047	0.0108	0.0220	0.0484	0.0746	0.1009	0.1254	0.1177	0.1034	0.0927	0.0865	0.0754	
ONE-DIMENS	Dial Readings (inch)	(g O	-0.0520	-0.0479	-0.0476	-0.0461	-0.0444	-0.0411	-0.0351	-0.0288	-0.0199	-0.0090	0.0043	0.0176	0.0415	0.0671	0.0855	0.1184	0.1186	0.1082	0.0940	0.0882	0.0756	
ONE	Dial R		nitia	-0.0526	-0.0520	-0.0477	-0.0469	-0.0449	-0.0420	-0.0389	-0.0313	-0.0232	-0.0120	-0.0026	0.0128	0.0286	0.0527	0.0777	0.1043	0.1210	0.1151	0.1030	0.0927	0.0865	
		Effective Stress (tsf)		0	0.050	0.075	0.110	0.160	0.220	0.330	0.440	099.0	0.870	1.310	1.740	3.510	7.040	14.100	28.360	7.040	1.740	0.870	0.660	0.330	

EOP= End of Primary Consolidation	EOI= End of load increment (typically 24 hrs +/-)		Specific Gravity 2.6402	Ring Diameter (in) 2.0000	Ring weight (g) 62.48	Height of Solids (in) 0.4353	
Final	Conditions	0.6473	19.3	132.3	110.8	104.8	0.4872
Initial	Conditions	0.7500	23.0	117.7	2.56	84.1	0.7231
		Height (in)	Wc (%)	$\gamma t (pcf)$	7d (pct)	Saturation (%)	Void ratio, e
	Oyster Bayou	12-80-3741	B-03	18-20 (19.0)			
	Project Name:	File Number:	Boring Number:	Depth:			



sf)

SAMPLE DATA	
BORING NO.:	B-04
SAMPLE NO.:	
DEPTH (FEET):	9.5
DESCRIPTION:	Gray CLAY (CH) w/trace organics
	and shell fragments
INDEX PROPERTIES	S
LIQUID LIMIT (%):	64
PLASTIC LIMIT (%):	16
PLASTICITY INDEX (%):	48
SPECIFIC GRAVITY:	2,62
-200(%):	86
ORGANIC CONTENT (%): 2.70

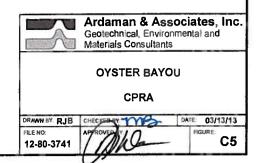
INITIAL	<u>FINAL</u>
87.6	63.4
49.0	64.0
2.34	1.55
	87.6 49.0

CONSOLIDATION PARAMETERS

EFFECTIVE OVERBURDEN STRESS, o'w (tsi):	0.16
PRECONSOLIDATION PRESSURE, o' (isf):	0.80
VIRGIN COMPRESSION RATIO, CR:	0.50

INCREMENTAL CONSOLIDATION TEST RESULTS

Confidential Information: Privileged & Confidential Work Product

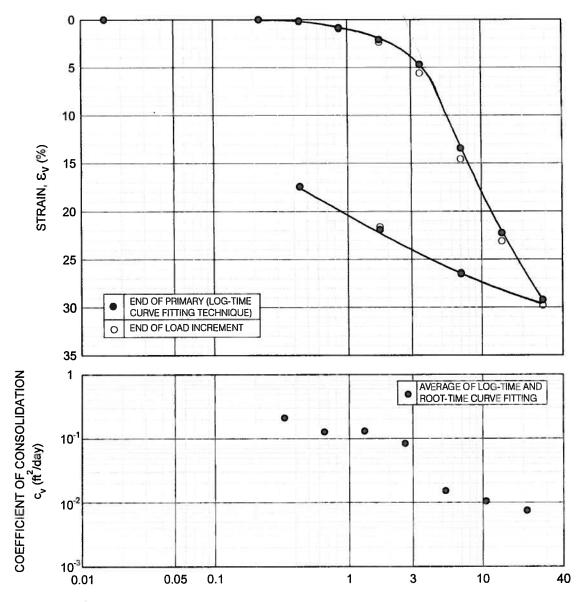


		C C C								0.00078	0.00124	0.002		0.01805							
				-	1				<u> </u>				I								
ET		Strain at EOI (%)		00.0	0.82	2.19	3.13	3.98	6.19	6.67	7.95	8.82	19.31	30.71	30.53	29.47	28.06	26.10	23.55		
Y SHE		Strain at EOP (%)		00.0	0.29	1.72	2.77	3.63	5.00	6.46	7.61	8.43	14.02	28.95	30.57	29.65	28.36	26.38	23.87		
MMAR		Void Ratio at	EOI	2.3374	2.3100	2.2642	2.2330	2.2045	2.1307	2.1147		2.0430	1.6930	1.3126	1.3186	1.3540	1.4009	1.4663	1.5513		
EST SL		Void Ratio at	EOP	2.3374	2.3278	2.2800	2.2450	2.2161	2.1705	2.1218	2.0835	2.0561	1.8695	1.3713	1.3173	1.3477	1.3909	1.4570	1.5409		
TION T		Height at EOI	(inch)	0.7500	0.7439	0.7336	0.7266	0.7202	0.7036	0.7000	0.6904	0.6839	0.6052	0.5197	0.5211	0.5290	0.5396	0.5543	0.5734		
SOLIDA		Height at EOP	(inch)	0.7500	0.7479	0.7371	0.7293	0.7228	0.7125	0.7016	0.6930	0.6868	0.6449	0.5329	0.5208	0.5276	0.5373	0.5522	0.5710		
NG CON		Average Effective	Stress (tsf)	-	0.020	0.060	0.110	0.170	0.255	0.360	0.510	0.710	1.015	1.830	1.830	0.915	0.460	0.225	0.090		
INCREMENTAL LOADING CONSOLIDATION TEST SUMMARY SHEET		Cv (ff ² /dav)	(it roay)		2.77E-01	7.74E-02	1.23E-01	7.63E-02	1.27E-01	1.52E-01	1.50E-01	1.09E-01	5.45E-02	8.89E-03	7.43E-02	1.70E-02	7.39E-03	2.45E-03	1.36E-03		
MENTA		Method (L=log,	S=sq rt)						_				٦			ب	ب				
INCRE		Time,	200		9	210	129	204	120	96	8	129	240	1080	108	480	1140	3600	0069		
SIONAL	ch)		EOI	0.0879	0.0960	0.1080	0.1163	0.1240	0.1417	0.1455	0.1554	0.1632	0.2447	0.3312	0.3297	0.3213	0.3106	0.2957	0.2765		
ONE-DIMENSIONAL	Dial Readings (inch)		EOP	0.0879	0.0920	0.1044	0.1136	0.1214	0.1327	0.1439	0.1528	0.1602	0.2050	0,3180	0.3300	0.3227	0.3128	0.2978	0.2788		
ONE	Dial R		Initial	0.0879	0.0899	0.0977	0.1093	0.1176	0.1251	0.1419	0.1458	0.1567	0.1660	0.2457	0.3311	0.3293	0.3211	0.3104	0.2956		
		Effective Stress	(tsf)	0	0.040	0.080	0.140	0.200	0.310	0.410	0.610	0.810	1.220	2.440	1.220	0.610	0.310	0.140	0.040		

EOP= End of Primary Consolidation	EOI= End of load increment (typically 24 hrs +/-)		Specific Gravity 2.619	Ring Diameter (in) 2.0000	Ring weight (g) 62.50	Height of Solids (in) 0.2247	Weight of Dry Soil (g) 30.30
Final	Conditions	0.5740	63.4	104.6	64.0	106.8	1.5542
Initial	Conditions	0.7500	9.78	91.9	49.0	98.1	2.3374
		Height (in)	Wc (%)	γt (pcf)	γd (pcf)	Saturation (%)	Void ratio, e
	Oyster Bayou	12-80-3741	B-04	8-10 (9.5)			
	Project Name:	File Number:	Boring Number:	Depth:			

	ONE	ONE-DIMENSION		INCRE	MENTA	GEOTECHNICAL TESTING LABORATORY AL INCREMENTAL LOADING CONSOLIDATION TEST SUMMARY SHEET	NG CON	SOLIDA	TION TE	est su	MMAR	Y SHE	ΕT	
	Dial F	Dial Readings (inch)	Jch)											
Effective Stress				Time,	Method (L=log,	Cv (ff ² /dev)	Average Effective	Height at EOP	Height at EOI	=	Void Ratio at	Strain at	Strain at	Coe
(tsf)	Initial	EOP	EOI	Carlo Military	S=sq rt)	(it rady)	Stress (tsf)	(inch)	(inch)	O O	<u> </u>) 1		
0	0.0879	0.0879	0.0879			i		0.7500	0.7500	2.3374	2.3374	0.00	0.00	
0.040	0.0895	0.0911	0960.0	99	ဟ	1.19E+00	0.020	0.7484	0.7435	2.3303	2.3085	0.21	0.87	1
0.080	0.0974	0.1003	0.1080	98	တ	8.17E-01	090:0	0.7406	0.7330	2.2955	2.2615	1.25	2.27	-
0.140	0.1090		0.11	317	တ	2.15E-01	0.110	0.7301	0.7257	2.2486	2.2290	2.66	3.25	1
0.200	0.1163			290	တ	2.29E-01	0.170	0.7180	0.7180	2.1948	2.1948	4.27	4.27	-
0.310	0.1243			194	တ	3.36E-01	0.255	0.7121	0.7006	2.1688	2.1173		6.59	-
0.410	0.1421			290	S	2.15E-01	0.360	0.6986	0.6972	2.1084	2.1022		7.05	0.00078
0.610	0.1455			375	တ	1.64E-01	0.510	0.6894	0.6873	2.0675	2.0581	8.09	8.37	0.00124
0.810	0.1567			998	တ	6.92E-02	0.710	0.6833	0.6808	2.0403	2.0294	8.90	9.23	0.002
1.220	0.1632			694	တ	7.53E-02	1.015	0.5993	0.5993	1.6668	1.6668	20.09	20.09	
2.440	0.2470			1882	တ	2.25E-02	1.830	0.5515	0.5151	1.4541	1.2921	26.47	31.32	0.01805
1.220	0.3311	0.3301	0.3297	317	တ	1.07E-01	1.830	0.5160	0.5165	1.2962	1.2982	31.20	31.14	1
0.610	0.3293	0.3237	0.3213	1441	တ	2.39E-02	0.915	0.5221	0.5245	1.3231	1.3338	30,39	30.07	-
0.310	0.3211	0.3131	0.3106	4438	တ	8.03E-03	0.460	0.5325	0.5350	1.3694	1.3808	29.00	28.66	1
0.140	0.3105		0.2957	11098	တ	3.36E-03	0.225	0.5459	0.5498	1.4293	1.4466	27.21	26.69	1
0.040	0.2956	0.2788	0.2765	35138	တ	1.13E-03	0.090	0.5666	0.5690	1.5214	1.5318	24.45	24.14	1
									-					

idation	typically 24 hrs +/-)		2.619	2.0000	62.50	0.2247	30.30
EOP= End of Primary Consolidation	EOI= End of load increment (typically 24 hrs +/-)		Specific Gravity 2.619	Ring Diameter (in)	Ring weight (g)	Height of Solids (in)	Weight of Dry Soil (g)
Final	Conditions	0.5740	63.4	104.6	64.0	106.8	1.5542
Initial	Conditions	0.7500	9.78	91.9	49.0	98.1	2.3374
		Height (in)	Wc (%)	γ t (pcf)	γd (pct)	Saturation (%)	Void ratio, e
	Oyster Bayou	12-80-3741	B-04	8-10 (9.5)	•		
	Project Name:	File Number:	Boring Number:	Depth:			



VERTICAL EFFECTIVE STRESS, $\sigma'_{\nu c}$ (tsf)

B-05
39.5
Tan and gray CLAY (CH)
w/silt layers
·
84
26
58
2.77
100

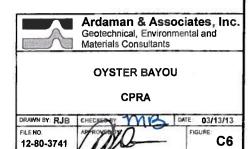
SPECIMEN CONDITIONS	INITIAL	<u>FINAL</u>
MOISTURE CONTENT (%):	51.6	36.9
DRY DENSITY (Ib/ft3):	71.2	86.3
VOID RATIO:	1.43	1.01
DRY DENSITY (Ib/ft³):	71.2	86.3

CONSOLIDATION PARAMETERS

EFFECTIVE OVERBURDEN STRESS, σ'_{vo} (tsf):	0.97
PRECONSOLIDATION PRESSURE, σ'p (tsf):	3.5
VIRGIN COMPRESSION RATIO, CR:	0.32

INCREMENTAL CONSOLIDATION TEST RESULTS

Confidential Information: Privileged & Confidential Work Product



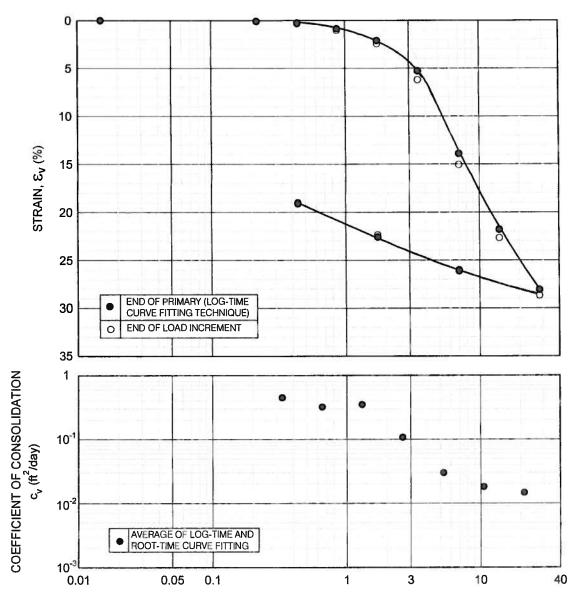
		Cos			1	0.00037	0.00075	0.00138	00900	0.01230	0.00889	0.00646		Ĩ	Ī				
H:		Strain at EOI (%)		0.00	0.00	0.21	0.95	2.37	2.60	14.56	23.11	29.80	26.40	21.61	17.45				
Y SHEE		Strain at EOP (%)		0.00	0.00	0.13	0.84	2.09		13.43	22.25			21.92	17.41				
MMAR		Void Ratio at	EOI	1.4297	1.4297	1.4245	1.4067	1.3720	1.2936	1.0759			0.7883	0.9046	1.0056				
ST SU		=	EOP	1.4297	1.4297	1.4265	1.4093	1.3789	1.3157	1.1035	0.8890	0.7196	0.7857	0.8971	1.0066				
TION		Height at EOI	(inch)	0.7500	0.7500	0.7484	0.7429	0.7322	0.7080	0.6408	0.5767	0.5265	0.5520	0.5879	0.6191				
SOLIDA		Height at EOP	(inch)	0.7500	0.7500	0.7490	0.7437	0.7343	0.7148	0.6493	0.5831	0.5308	0.5512	0.5856	0.6194				
NO CON		Average Effective	Stress (tsf)		0.118	0.330	0.655	1.305	2.625	5.275	10.570	21,230	17.700	4.390	1.090		2		
LINCREMENTAL LOADING CONSOLIDATION TEST SUMMARY SHEET		CV (#2/42w)				2.14E-01	7.86E-02	8.99E-02	4.31E-02	1.11E-02	8.22E-03	6.31E-03	9.57E-03	2.66E-03	1.20E-03				
MENTA		Method (L=log,	S=sq rt)				ب		_	ب				ب	_				
INCRE		Time,				78	210	180	360	1230	1350	1440	006	3600	0006				
	ich)		EOI	0.0700	0.0700	0.0717	0.0780	0.0901	0.1163	0.1855	0.2514	0.3033	0.2767	0.2397	0.2078				
ONE-DIMENSIONA	Dial Readings (inch)		EOP	0.0700	0.0700	0.0711	0.0772	0.0880	0.1095	0.1770	0.2450	0.2990	0.2775	0.2420	0.2075				
ONE	Dial R		Initial	0.0700	0.0700	0.0701	0.0725	0.0794	0.0921	0.1183	0.1873	0.2531	0.3022	0.2756	0.2390			=	
		Effective Stress	(tsf)	0	0.220	0.440	0.870	1.740	3.510	7.040	14.100	28.360	7.040	1.740	0.440				

EOF= End of Primary Consolidation	EOI= End of load increment (typically 24 hrs +/-)		Specific Gravity 2.7726	Ring Diameter (in) 2.0000	Ring weight (g) 62.49		Weight of Dry Soil (g) 44.06
		0.6193	36.9	118.2	86.3		1,0063 W
Initial	Conditions	0.7500	51.6	108.0	71.2	100.0	1.4297
		Height (in)	w _c (%)	γ t (pcf)	yd (pct)	Saturation (%)	Void ratio, e
	Oyster Bayon	12-80-3741	B-05	38-40 B3 (39.5)			
	Project Name:	File Number:	Boring Number:	Depth:			

ARDAMAN & ASSOCIATES, INC GEOTECHNICAL TESTING LABORATORY ONE-DIMENSIONAL INCREMENTAL LOADING CONSOLIDATION TEST SUMMARY SHEET

Effective Stress	T T	July Southe	Ę											
(tst)				Time, t ₁₀₀ (sec)	Method (L=log, S=sq rt)	Cv (ff²/day)	Average Effective Stress (tsf)	Height at EOP (inch)	Height at EOI (inch)	Void Ratio at EOP	Void Ratio at EOI	Strain at EOP (%)	Strain at EOI (%)	Cae
	Initial	<u>О</u>	Ö											
0	0.0700	0.0700	0.0700					0.7500	0.7500	1.4297	1.4297	00.0	00.0	
0.220	0.0700	0.0700	0.0700				0.110	0.7500	0.7500	1.4297	1.4297	0.00	0.00	1
	0.0701	0.0711	0.0717	345	တ	2.08E-01	0.330	0.7490	0.7484	1.4265	1.4245	0.13	0.21	0.00037
	0.0726	0.0758	0.0780	406	S	1.75E-01	0.655	0.7452	0.7430	1.4142	1.4070		0.93	0.00075
	0.0794	0.0856	0.0901	406	S	1.72E-01	1.305	0.7368	0.7323	1.3870	1.3724		2.36	0.00138
	0.0930	0.1036	0.1163	540	ဟ	1.25E-01	2.625	0.7217	0.7090	1.3380	1.2969		5.47	0.00600
	0.1185	0.1646	0.1855	3110	S	1.93E-02	5.275	0.6629	0.6420	1.1475	1.0798	11.61	14.40	0.01230
	0.1885	0.2357	0.2514	3840	တ	1.27E-02	10.570	0.5948	0.5791	0.9269	0.8761		22.79	0.00889
	0.2545	0.2928	0.3033	4640	တ	8.62E-03	21.230	0.5408	0.5303	0.7520	0.7180		29.29	0.00646
	0.2988	0.2889	0.2767			6.09E-02	17.700	0.5402	0.5524	0.7500	0.7896		26.35	1
	0.2738	0.2511	0.2397	u	တ	6.76E-03	4.390	0.5751	0.5865	0.8631	0.9000			1
	0.2390	0.2096	0.2078	(1)		1.32E-03	1.090	0.6159	0.6177	0.9953	1.0011	17.88	17.64	1
	_													
						7.4	<u>.</u>	Ü	7	EOD= En	of Prim	EOB≡ End of Primary Consolidation	lidation	
o we come		1				Conditions	iai Fone	Conditions		FOI FIRE	of load is	EQL = Life of load increment (typically 24 hrs +/-)	(typically 2	4 hrs +/-)

dation	ypically 24 hrs +/-)		2.7726	2.0000	62.49		44.06
EOP= End of Primary Consolidation	EOI= End of load increment (typically 24 hrs +/-)		Specific Gravity 2.7726	Ring Diameter (in)	Ring weight (g)	Height of Solids (in)	Weight of Dry Soil (g)
Final	Conditions	0.6193	36.9	118.2	86.3	101.8	1.0063
Initial	Conditions	0.7500	51.6	108.0	71.2	100.0	1 4297
		Height (in)	w _c (%)	yt (pcf)	yd (pct)	Saturation (%)	Void ratio P
	Oyster Bayou	12-80-3741	B-05	38-40 B3 (39.5)			
	Project Name:	File Number:	Boring Number:	Depth:	_		



VERTICAL EFFECTIVE STRESS, $\sigma^{\prime}_{\ vc}$ (tsf)

SAMPLE DATA	
BORING NO.:	B-06
SAMPLE NO.:	
DEPTH (FEET):	54.25
DESCRIPTION:	Gray CLAY (CH)
	w/silt layers
INDEX PROPERTIES	
LIQUID LIMIT (%):	63
PLASTIC LIMIT (%):	20
PLASTICITY INDEX (%):	43
PLASTICITY INDEX (%): SPECIFIC GRAVITY:	43 2.77

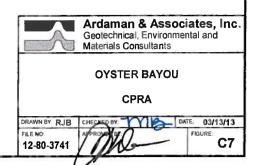
INITIAL	FINAL
44.7	31.3
76.5	94.5
1.26	0.83
	44.7 76.5

CONSOLIDATION PARAMETERS

EFFECTIVE OVERBURDEN STRESS, σ _{vo} (tsf):	1.34
PRECONSOLIDATION PRESSURE, o'p (tsf):	3.2
VIRGIN COMPRESSION RATIO, CR:	0.29

INCREMENTAL CONSOLIDATION TEST RESULTS

Confidential Information: Privileged & Confidential Work Product



GEOTECHNICAL TESTING LABORATORY

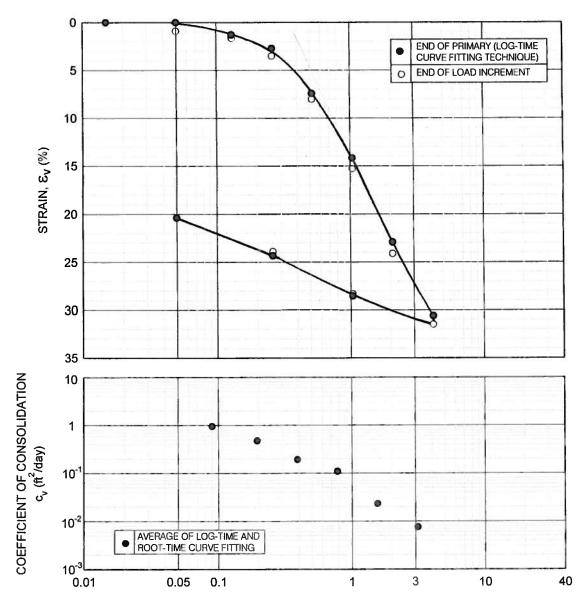
		Cae		1		0.000355	0.000889	0.00133	0.00587	0.009778	0.00711	0.00542	1	-		
E		Strain at EOI (%)		0.00											19.00	
Y SHE		Strain at EOP (%)		00.0	0.08										19.11	
MMAF		Void Ratio at EOI		1.2565	1.2538	1.2487	•	1.2015	1.1166	0.9165	0.7447				0.8278	
EST SL		Void Ratio at EOP		1.2565	1.2547	1.2508	1.2373	1.2090	1.1374	0.9430	0.7646	0.6229	0.6674	0.7468	0.8254	
TION T		Height at EOI (inch)		0.7500	0.7491	0.7474	0.7422	0.7317	0.7035	0.6370	0.5799	0.5349	0.5551	0.5822	0.6075	
SOLIDA		Height at EOP (inch)		0.7500	0.7494	0.7481	0.7436	0.7342	0.7104	0.6458	0.5865	0.5394	0.5542	0.5806	0.6067	
NG CON		Average Effective Stress (tsf)			0.118	0.330	0.655	1.305	2.625	5.275	10,570	21.230	17.700	4.390	1.090	
INCREMENTAL LOADING CONSOLIDATION TEST SUMMARY SHEET		Cv (ft²/day)				3.46E-01	2,75E-01	2.45E-01	7.14E-02	2.14E-02	1.48E-02	1.19E-02	1.63E-01	4.83E-03	1.75E-03	
MENTA		Method (L=log, S=sa rt)	<u> </u>				_	١		اس		ب			ب	
INCRE		Time, t ₁₀₀ (sec)				48	9	99	216	630	750	780	32	1980	0009	
ONE-DIMENSIONAL	ch)		EOI	0.1304	0.1313	0.1338	0.1400	0.1519	0.1819	0.2503	0.3096	0.3570	0.3356	0.3061	0.2802	
DIMEN	Dial Readings (inch)		EOP	0.1304	0.1310	0.1331	0.1386	0.1494	0.1750	0.2415	0.3030	0.3525	0.3365	0.3077	0.2810	
ONE	Dial R		Initia	0.1304	0.1304	0.1321	0.1348			0.1838	0.2525	0.3120	0.3558			
		Effective Stress	Ž		0.220	0.440	0.870	1.740	3.510	7.040	14.100	28.360	7.040	1.740	0.440	

EOP= End of Primary Consolidation	EOI= End of load increment (typically 24 hrs +/-)		Specific Gravity 2.7665	Ring Diameter (in) 1.9990	Ring weight (g) 62.62		Weight of Dry Soil (g) 47.29
Final	Conditions	0.6075	31.3	124.1	94.5	104.7	0.8278
Initial	Conditions	0.7500	44.7	110.8	76.5	98.5	1,2565
		Height (in)	Wc (%)	7t (pcf)	yd (bat)	Saturation (%)	Void ratio, e
	Oyster Bayon	12-80-3741	B-06	53-55 B2 (54.25)			
	Project Name:	File Number:	Boring Number:	Depth:			,

ONE-DIMENSIONAL INCREMENTAL LOADING CONSOLIDATION TEST SUMMARY SHEET

F					2	თ	က	~	8	_	7				
		Cas				0	0.00133	0.00587	0.009778	0.00711	0.00542	i	1		
		Strain at EOI (%)	0.00	0.12	0.35	1.0	2.19	5.57	14.12	21.40	27.27	25.08	21.57	18.12	
		Strain at EOP (%)	0.00	0.08	0.23	0.75	1.65	3.96	11.32	19.57	25.84	25.64	22.32	18.52	
		Void Ratio at EOI	1.2565	1.2538	1.2487	1.2340	1.2072	1.1308	0.9379	0.7736	0.6412	0.6906	0.7697	0.8476	
		Void Ratio at EOP	1.2565	1.2547	1.2514	1.2397	1.2192	1.1672	1.0011	0.8148	0.6734	0.6779	0.7529	0.8386	
		Height at EOI (inch)	0.7500	0.7491	0.7474	0.7425	0.7336	0.7082	0.6441	0.5895	0.5455	0.5619	0.5882	0.6141	
		Height at EOP (inch)	0.7500	0.7494	0.7483	0.7444	0.7376	0.7203	0.6651	0.6032	0.5562	0.5577	0.5826	0.6111	
		Average Effective Stress (tsf)		0.110	0.330	0.655	1.305	2.625	5.275	10.570	21.230	17.700	4.390	1.090	
		Cv (ft²/day)			5.50E-01	3.66E-01	4.54E-01	1.44E-01	3.86E-02	2.16E-02	1.75E-02	2.06E-02	6.44E-03	2.16E-03	
		Method (L=log, S=sq rt)			ဟ	တ	S	S	တ	တ	တ	တ	ဟ	တ	
		Time, t ₁₀₀ (sec)			130	194	45	470	1560	2300	2400	1882	6490	21206	
	ch)	EOI	0.1304	0.1313	0.1338	0.1400	0.1519	0.1819	0.2503	0.3096	0.3570	0.3356	0.3061	0.2802	
	Dial Readings (inch)	EOP	0.1304	0.1310	0.1329	0.1381	0.1479	0.1698	0.2293	0.2959	0.3463	0.3398	0.3117	0.2832	
	Dial R	Initial	0.1304	0.1304	0.1321	0.1351	0.1430	0.1565	0.1862	0.2550	0.3130	0.3520	0.3324	0.3061	
		Effective Stress (tsf)	0	0.220	0.440	0.870	1.740	3.510	7.040	14.100	28.360	7.040	1.740	0.440	

EOP= End of Primary Consolidation EOI= End of load increment (typically 24 hrs +/-)		Specific Gravity 2.7665	Ring Diameter (in) 1.9990	Ring weight (g) 62.62	Height of Solids (in) 0.3324 Weight of Dry Soil (g) 47.29
Final Conditions	0.6075	31.3	124.1	94.5	104.7 0.8278
Initial Conditions	0.7500	44.7	110.8	76.5	98.5 1.2565
	Height (in)	w _c (%)	yt (pcf)	γ d (pct)	Saturation (%) Void ratio, e
Oyster Bayou	12-80-3741	B-06	53-55 B2 (54.25)		
Project Name:	File Number:	Boring Number:	Depth:		



VERTICAL EFFECTIVE STRESS, σ'_{vc} (tsf)

SAMPLE DATA	
BORING NO.:	B-07
SAMPLE NO.:	
DEPTH (FEET):	₋ 1.25
DESCRIPTION:	Gray CLAY (CH) w/silt
INDEX DOODEDTIES	
INDEX PROPERTIES	
LIQUID LIMIT (%):	114
PLASTIC LIMIT (%):	27
PLASTICITY INDEX (%):	87

SPECIMEN CONDITIONS	INITIAL	FINAL
MOISTURE CONTENT (%):	79.8	61.7
DRY DENSITY (lb/ft3):	52.7	66.2
VOID RATIO:	2.17	1.53

CONSOLIDATION PARAMETERS

EFFECTIVE OVERBURDEN STRESS, o'vo (tsf):	0.02
PRECONSOLIDATION PRESSURE, o'p (tsf):	0.50
VIRGIN COMPRESSION RATIO, CR:	0.29

INCREMENTAL CONSOLIDATION TEST RESULTS

2.68

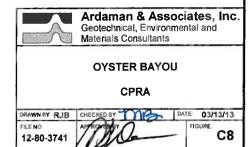
94

Confidential Information: Privileged & Confidential Work Product

SPECIFIC GRAVITY:

ORGANIC CONTENT (%):

-200(%):

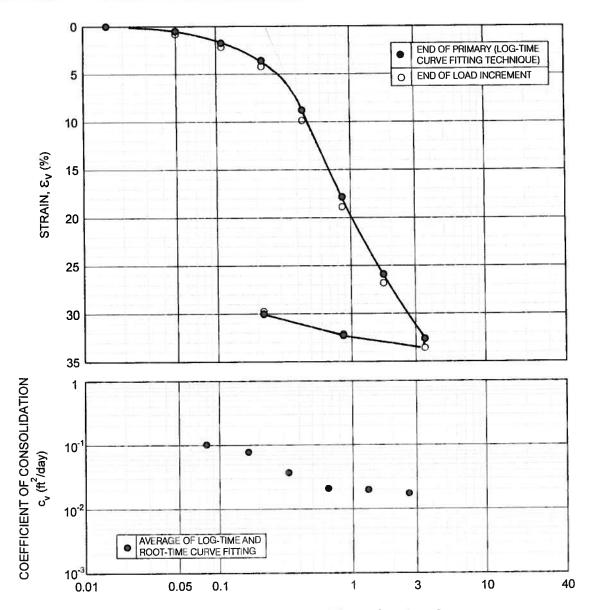


SHEET	
RY	
SUMM	
TION TEST SUMN	
ATION	
SOLIE	20,000
100 S	X
L LOADING CONS	
NTAL I	83
REME	
NSIONAL INCREMENTAL LOADING CONSOLIDATION TEST SUMMA	
NOISNE	
E-DIME	
NO O	

	CNE	UIMEN	SIONAL	NCKE	MENIA	ONE-DIMENSIONAL INCREMENTAL LOADING CONSOLIDATION TEST SUMMARY SHEE	NG CON	SOLIDA	ION IE	INC I S	WIMAR	Y SHE		
	Dial R	Dial Readings (inch)	ch)											
Effective Stress (tsf)	Initial	EOP	EOI	Time, t ₁₀₀ (sec)	Method (L=log, S=sq rt)	Cv (ff²/day)	Average Effective Stress (tsf)	Height at EOP (inch)	Height at EOI (inch)	Void Ratio at I	Void Ratio at EOI	Strain at EOP (%)	Strain at EOI (%)	Cae
0 0.050 0.130 0.260 0.520 1.040 1.040 0.260 0.050	0.1167 0.1167 0.1236 0.1294 0.1442 0.1790 0.2248 0.3266 0.3219 0.2883	0.1167 0.1167 0.1265 0.1376 0.2820 0.3243 0.2920 0.2920	0.1167 0.1234 0.1291 0.1435 0.1781 0.2335 0.3478 0.3227 0.2618	15 30 270 244 720 1440 4140		1.09E+00 5.32E-01 5.52E-02 5.40E-02 1.52E-02 6.11E-03 6.48E-03 2.19E-03	- 0.033 0.090 0.195 0.390 0.780 1.560 3.120 2.600 0.650 0.155	0.7500 0.7500 0.7405 0.7297 0.6945 0.6782 0.5206 0.5361 0.5676	0.7500 0.7434 0.7379 0.6899 0.6354 0.5138 0.5138 0.5377 0.5973	2.1742 2.1742 2.1337 2.0880 1.9391 1.7249 1.2687 1.2687 1.5277	2.1742 2.1460 2.1227 2.0631 1.9196 1.6889 1.1743 1.2755 1.5277	0.00 0.00 1.27 2.71 7.41 14.15 22.91 30.59 28.53 24.33 20.37	0.00 0.89 3.50 8.02 15.29 24.11 31.50 23.30 20.37	0.00130 0.00320 0.00610 0.00900 0.01080
Project Name: File Number: Boring Number: Depth:	Ľ.	Oyster Bayou 12-80-3741 B-07 0-2 B2 (1.25)	Bayou -3741 07 (1.25)	Satur	Height (in) w _c (%) γt (pcf) γd (pcf) Saturation (%)	Initial Conditions 0.7500 79.8 94.7 52.7 98.3	tial titions 500 1.8 7 (.3	Final Conditions 0.5972 61.7 107.0 66.2 108.2	aal trions 772 7.7 7.0 2.2 3.2	EOP= End EOI= End H	of load in Specif Ring Dian Ring v eight of Sight of Dian	EOP= End of Primary Consolidation EOI= End of load increment (typically Specific Gravity 2.000 Ring Diameter (in) 2.000 Ring weight (g) 62.4 Height of Solids (in) 0.230 Weight of Dry Soil (g) 32.0	EOP= End of Primary Consolidation EOI= End of load increment (typically 24 hrs +/-) Specific Gravity 2.68 Ring Diameter (in) 2.0000 Ring weight (g) 62.49 Height of Solids (in) 0.2363 Weight of Dry Soil (g) 32.60	hrs +/-)

		CAR			1	0.00130	0.00320	0.00610	0.0000	0.01080	0.00900	1	-				
		Strain at EOI (%)		00'0	0.89	1.62	3.50	8.02						20.37			
Y SHE		Strain at EOP (%)	-	00:00		1.27	2.71	7.41		22.91		28.53		20.37			
MMAF		Void Ratio at EOI		2.1742	2.1460	2.1227	2.0631	1.9196	1.6889	1.4088	1.1743	1.2755	1.4155	1.5277			
ST SU		Void Ratio at EOP		2.1742	2.1742	2.1337	2.0880	1.9391	1.7249	1.4469	1.2031	1.2687	1.4020	1.5277			
TION TE		Height at EOI (inch)		0.7500	0.7434	0.7379	0.7238	0.6899	0.6354	0.5692	0.5138	0.5377	0.5708	0.5973			
SOLIDA		Height at EOP (inch)		0.7500	0.7500	0.7405	0.7297	0.6945	0.6439	0.5782	0.5206	0.5361	0.5676	0.5973			
NG CON		Average Effective Stress (tsf)			0.025	0.090	0.195	0.390	0.780	1.560	3.120	2.600	0.650	0.155		5	
INCREMENTAL LOADING CONSOLIDATION TEST SUMMARY SHEET		Cv (ff²/day)				8.17E-01	4.29E-01	3.31E-01	1.65E-01	3.13E-02	9.02E-03	1.13E-02					
WENTA		Method (L=log, S=sa rt)	<u> </u>			တ	တ	S	S	တ	Ø	S					
INCRE		Time, t ₁₀₀ (sec)				98	160	194	345	1500	4200	3110					
	ch)		EOI	0.1167	0.1234	0.1291	0.1435	0.1781	0.2335	0.2910	0.3478	0.3227	0.2888	0.2618			
ONE-DIMENSIONAL	Dial Readings (inch)		EOP	0.1167	0.1167	0.1265	0.1376	0.1735	0.2250	0.2820	0.3410	0.3243	0.2920	0.2618			
ONE	Dial R	•	nitial	0.1167	0.1167	0.1236	0.1294	0.1442	0.1790	0.2248	0.2924	0.3466	0.3219	0.2883			
;		Effective Stress		0	0.050	0.130	0.260	0.520	1.040	2.080	4.160	1.040	0.260	0.050			

	rs +/-)						
lation	pically 24 h		2.68	2.0000	65.49	0.2363	32.60
EOP= End of Primary Consolidation	EOI= End of load increment (typically 24 hrs +/-)		Specific Gravity 2.68	Ring Diameter (in)	Ring weight (g)	Height of Solids (in)	Weight of Dry Soil (g)
Final	Conditions	0.5972	61.7	107.0	66.2	108.2	1.5276
Initial	Conditions	0.7500	79.8	94.7	52.7	98.3	2.1742
		Height (in)	wc (%)	<pre>/t (pcf)</pre>	γd (pct)	Saturation (%)	Void ratio, e
	Oyster Bayon	12-80-3741	B-07	0-2 B2 (1.25)	•		
	Project Name:	File Number:	Boring Number:	Depth:	•		



VERTICAL EFFECTIVE STRESS, σ'_{vc} (tsf)

SAMPLE DATA	
BORING NO.:	B-07
SAMPLE NO.:	
DEPTH (FEET):	5.25
DESCRIPTION:	Gray CLAY (CH)
	w/silt and shells
INDEX PROPERTIES	
LIQUID LIMIT (%):	91
PLASTIC LIMIT (%):	25
PLASTICITY INDEX (%):	66
SPECIFIC GRAVITY	2.72
-200(%):	89

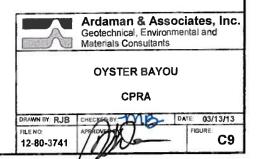
45.5
77.1
1.20

CONSOLIDATION PARAMETERS

EFFECTIVE OVERBURDEN STRESS, o (tsf):	0.086
PRECONSOLIDATION PRESSURE, o'p (tsf):	0.315
VIRGIN COMPRESSION RATIO, CR:	0.29

INCREMENTAL CONSOLIDATION TEST RESULTS

Confidential Information: Privileged & Confidential Work Product

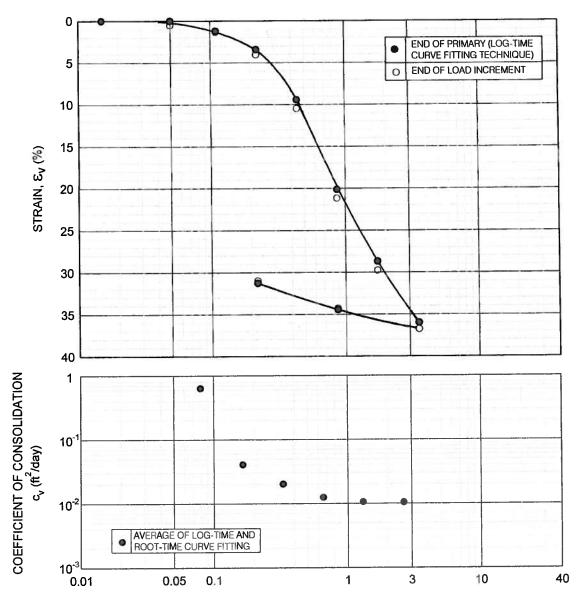


		COE		-		0.00210	0.00380	0.01020	0.01020	0.00800	0.00710	_		
ET	1	Strain at EOI (%)		00.0	0.81	2.17	4.21	9.87				32.15	29.75	
Y SHE		Strain at EOP (%)	1	00.0	0.49		3.60	8.77				32.28	30.01	
MMAF		Void Ratio at		2.1356	2.1101		2.0035	1.8262	1.5436	1.2948	1.0829	1.1276	1.2029	
EST SU		Void Ratio at	j	2.1356	2.1201	2.0813	2.0227	1.8605	1.5762	1.3237	1.1126	1.1234	1.1945	
TION TI		Height at EOI		0.7500	0.7439	0.7337	0.7184	0.6760	0.6084	0.5489	0.4982	0.5089	0.5269	
SOLIDA		Height at EOP		0.7500	0.7463	0.7370	0.7230	0.6842	0.6162	0.5558	0.5053	0.5079	0.5249	
NG CON		Average Effective	(ici) ecano		0.033	0.080	0.165	0.330	0.655	1.305	2.625	2.190	0.545	
ONE-DIMENSIONAL INCREMENTAL LOADING CONSOLIDATION TEST SUMMARY SHEET		Cv (ff²/day)				9.03E-02	5.24E-02	2.21E-02	1.59E-02	1.59E-02	1.45E-02	3.38E-02	6.00E-03	
MENTA		Method (L=log,	0-8d-10			ب	ب					ب	_	
INCRE		Time,	170			180	300		780	630	920	222	1320	
SIONAL	ch)		EO	0.0215	0.0276	0.0384	0.0540	0.0974	0.1638	0.2237	0.2752	0.2632	0.2442	
DIMEN	Dial Readings (inch)		EOP	0.0215	0.0252	0.0351	0.0494	0.0892	0.1560	0.2168	0.2681	0.2642	0.2462	
ONE	Dial R		Initial	0.0215	0.0215	0.0282	0.0387	0.0550	0.0962	0.1642	0.2245	0.2739	0.2622	
		Effective Stress	(ISI)	°	0.050	0.110	0.220	0.440	0.870	1.740	3.510	0.870	0.220	

EOP= End of Primary Consolidation EOI= End of load increment (typically 24 hrs +/-)		Ring Diameter (in) 1.9990		_	Weight of Dry Soil (g) 33.46
Final Conditions	0.5268 45.5	112.2	77.1	102.9	1.2024
Initial	0.7500 79.0	6.96	54.2	100.6	2.1356
	Height (in) w _c (%)	7t (pcf)	γ d (pct)	Saturation (%)	Void ratio, e
Oyster Bayou	12-80-3741 B-07	4-6 B1 (5.25)			
Project Name:	File Number: Boring Number:	Depth:			

		COR		1	1	0.200.0	0.00380	0.01020	0.01020	0.00800	0.00710	1	1	1
13		Strain at EOI (%)		00.0	0.81	2.17	4.21	9.87	18.88	26.81	33.57	32.15	29.75	
Y SHE		Strain at EOP (%)											30.01	
MMAF		Void Ratio at EOI						•			_		1.2029	
EST SU		Void Ratio at EOP		l				•	<u> </u>	1.3237	1.1126	1.1234	1.1945	
TION TI		Height at EOI (inch)		0.7500	0.7439	0.7337	0.7184	0.6760	0.6084	0.5489	0.4982	0.5089	0.5269	
SOLIDA		Height at EOP (inch)		Į.			0.7230	0.6842	0.6162	0.5558	0.5053	0.5079	0.5249	
NG CON		Average Effective Stress (tsf)			0.025	0.080	0.165	0.330	0.655	1.305	2.625	2.190	0.545	
ONE-DIMENSIONAL INCREMENTAL LOADING CONSOLIDATION TEST SUMMARY SHEET		Cv (ff²/day)				1.14E-01	1.04E-01	5.17E-02	2.55E-02	2.38E-02	2.03E-02	4.65E-02	8.45E-03	
MENTA		Method (L=log, S=sa rt)	<u>;</u>			တ	တ	S	S	တ	တ	S	S)
INCRE		Time, t ₁₀₀ (sec)	·			614	653	1215					4034	t P
SIONAL	ch)		ËŌ	0.0215	0.0276	0.0384	0.0540	0.0974	0.1638	0.2237	0.2752	0.2632	0.2442	7
DIMEN	Dial Readings (inch)		EOP	0.0215	0.0215	0.0352	0.0494	0.0892	0.1560	0.2168	0.2681	0.2642	0 2462	7047.0
ONE	Dial R		Initial	0.0215	0.0215	0.0282	0.0387	0.0550	0.0962	0.1642	0.2245	0.2739	0.2622	7787.0
		Effective Stress		0	0.050	0.110	0.220	0.440	0.870	1.740	3.510	0.870	0 2 2 0	

EOP= End of Primary Consolidation	EOI= End of load increment (typically 24 hrs +/-)	i		Ring Diameter (in) 1.9990	Ring weight (g) 62.49		Weight of Dry Soil (g) 33.46
Final	Conditions	0.5268	45.5	112.2	77.1	102.9	1.2024
Initial	Conditions	0.7500	79.0	6.96	54.2	100.6	2.1356
		Height (in)	(%) Mc (%)	yt (pcf)	√d (pct)	Saturation (%)	Void ratio, e
	Ovster Bayou	12-80-3741	B-07	4-6 B1 (5.25)			
	Project Name:	File Number	Boring Number	Depth:			



VERTICAL EFFECTIVE STRESS, σ'_{vc} (tsf)

SAMPLE DATA	
BORING NO.:	B-07
SAMPLE NO.:	
DEPTH (FEET):	9.5
DESCRIPTION:	Gray CLAY (CH)
	w/silt and sand
INDEX PROPERTIES	
LIQUID LIMIT (%):	71
PLASTIC LIMIT (%):	19
PLASTICITY INDEX (%):	52
SPECIFIC GRAVITY:	2.74
-200(%):	97
ORGANIC CONTENT (%):	4.13

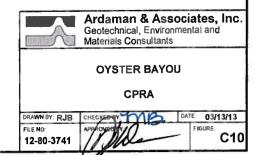
SPECIMEN CONDITIONS	INITIAL	FINAL
MOISTURE CONTENT (%):	89.2	52.0
DRY DENSITY (lb/ft3):	49.3	71.5
VOID RATIO:	2.47	1.39

CONSOLIDATION PARAMETERS

EFFECTIVE OVERBURDEN STRESS, o'vo (tsf):	0.156
PRECONSOLIDATION PRESSURE, o', (isf):	0.31
VIRGIN COMPRESSION RATIO, CR:	0.34

INCREMENTAL CONSOLIDATION TEST RESULTS

Confidential Information: Privileged & Confidential Work Product

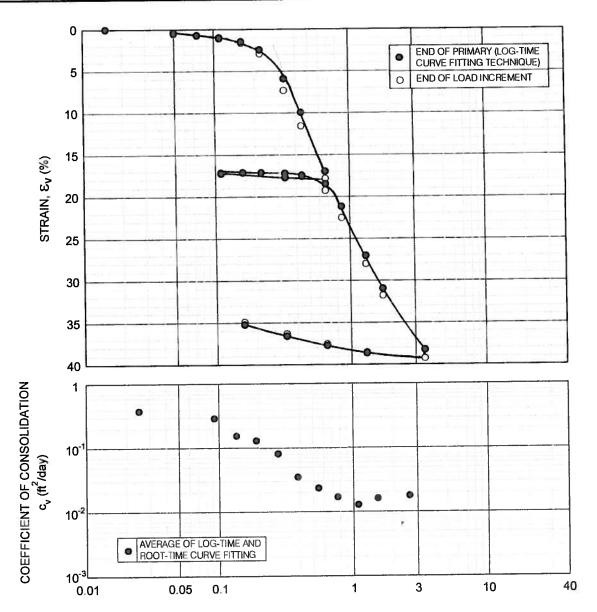


		Cae			-	0.00170	0.00430	0.01080	0.01070	0.00930	0.00670	1	1				 	
ᆸ		Strain at EOI (%)											30.97					
Y SHE		Strain at EOP (%)						9.41			35.99		31.25		 			
IMMAR		Void Ratio at EOI					2.3264	2.1031	1.7324	1.4348	ì		1.3927					
EST SL		Void Ratio at EOP			2.4664		2.3476	2.1401	1.7690	1,4722	1.2190	1.2726	1.3830					
TION T		Height at EOI (inch)		0.7500	0.7461	0.7401	0.7197	0.6714	0.5912	0.5268	0.4743	0.4929	0.5177					
SOLIDA		Height at EOP (inch)		0.7500	0.7500	0.7411	0.7243	0.6794	0.5991	0.5349	0.4801	0.4917	0.5156					
NG CON		Average Effective Stress (tsf)			0.033	0.080	0.165	0.330	0.655	1.305	2.625	2.190	0.545					
LINCREMENTAL LOADING CONSOLIDATION TEST SUMMARY SHEET		Cv (ft²/day)				4.55E-01	2.79E-02	1.73E-02	1.05E-02	9.22E-03	8.95E-03	1.44E-02	4.05E-03					
MENTA		Method (L=log, S=sort)	<u> </u>			۔۔	_	_		_								
INCRE	5	Time, t ₁₀₀ (sec)	24			36	570	840	1140	1020	840	480	1860					
	ch)		EOI	0.0548	0.0587	0.0650	0.0866	0.1360	0.2169	0.2819	0.3352	0.3158	0.2907	-				
ONE-DIMENSIONA	Dial Readings (inch)		EOP	0.0548	0.0548	0.0640	0.0820	0.1280	0.2090	0.2738	0.3294	0.3170	0.2928					
ONE	Dial R		Initia	0.0548	0.0548	0.0590	0.0662	0.0877	0.1367	0.2175	0.2827	0.3344	0.3155					
		Effective Stress (tef)		0	0.050	0.110	0.220	0.440	0.870	1.740	3.510	0.870	0.220					

	/ 24 hrs +/-)		4	8	41	54	52
EOF End of Filliary Consolidation	EOI= End of load increment (typically 24 hrs +/-)		Specific Gravity 2.7	Ring Diameter (in) 2.0000	Ring weight (g) 62.41	Height of Solids (in) 0.2164	Weight of Dry Soil (g) 30.5
Final	Conditions	0.5177	52.0	108.7	71.5	102.3	1.3927
Initial	Conditions	0,7500	89.2	93.4	49.3	99.1	2.4664
		Height (in)	Wc (%)	yt (pcf)	yd (pct)	Saturation (%)	Void ratio, e
	Oyster Bayou	12-80-3741	B-07	8-10 B3 (9.5)			
	Project Name:	File Number:	Boring Number:	Depth:			

		C		1	-	0.00170	0.00430	0.01080	0.01070	0.00930	0.00670			
13		Strain at EOI (%)		00.0	0.52	1.32	40.4	10.48	21.17		36.76	34.28	30.97	lidation
RY SHE		Strain at EOP (%)		0.00	0.00	1.19	3.43	9.41	20.12		35.99	34.44	31.25	EOP= End of Primary Consolidation
MMAF		Void Ratio at FOI	i	2.4664	2.4484	2.4206	2.3264	2.1031	1.7324	1.4348	1.1921	1.2781	1.3927	od of Prior
ST SU		Void Ratio at	j i	2.4664	2.4664	2.4253	2.3476	2.1401	1.7690	1.4722	1.2190	1.2726	1.3830	FOD= Fr
TION T		Height at EOI		0.7500	0.7461	0.7401	0.7197	0.6714	0.5912	0.5268	0.4743	0.4929	0.5177	- C
SOLIDA		Height at EOP		0.7500	0.7500	0.7411	0.7243	0.6794	0.5991	0.5349	0.4801	0.4917	0.5156	ů
NO CON		Average Effective	(151) 553 110		0.025	080.0	0.165	0.330	0.655	1.305	2.625	2.190	0.545	7
SECTECHNICAL TESTING CABONATION TEST SUMMARY SHEET		Cv (ft²/day)				8.21E-01	5.39E-02	2.32E-02	1.45E-02	1.20E-02	1.20E-02	2.81E-02	5.75E-03	3
MENTA		Method (L=log,	; ; ;			ဟ	တ	S	S	တ	S	S	S	
INCRE		Time, t _{io0} (sec)				98	1269	2693	3557	3375	2700	1058	5645	
	ch)		Ö	0.0548	0.0587	0.0650	0.0866	0.1360	0.2169	0.2819	0.3352	0.3158	0.2907	
ONE-DIMENSIONAL	Dial Readings (inch)		EOP	0.0548	0.0548	0.0640	0.0820	0.1280	0.2090	0.2738	0.3294	0.3170	0.2928	
ONE	Dial R		nitial	0.0548	0.0548	0.0590	0.0662	0.0877	0.1367	0.2175	0.2827	0.3344	0.3155	
		Effective Stress	<u> </u>	°	0.050	0.110	0.220	0.440	0.870	1.740	3.510	0.870	0.220	

Final	Conditions Conditions EOI= End of load increment (typically 24 hrs +/-)	0.5177	52.0	93.4 108.7 Ring Diameter (in) 2.0000		102,3 Height of Solids (in)	4 2007
		Height (in)	wc (%)	7t (pcf)	√d (bct)	Saturation (%)	
	Oyster Bayon	12-80-3741	B-07	8-10 B3 (9.5)			
	Project Name:	File Number:	Sample Name:	Depth:	-		



VERTICAL EFFECTIVE STRESS, σ'_{vc} (tsf)

SAMPLE DATA	
BORING NO.:	B-08
SAMPLE NO.:	
DEPTH (FEET):	5.75
DESCRIPTION:	Gray SANDY CLAY (CL)
	w/shells
INDEX PROPERTIES	
LIQUID LIMIT (%):	85
PLASTIC LIMIT (%):	25
PLASTICITY INDEX (%):	60
SPECIFIC GRAVITY:	2.69
-200(%):	86

SPECIMEN CONDITIONS	INITIAL	FINAL
MOISTURE CONTENT (%):	85.5	47.4
DRY DENSITY (lb/lt3):	51.0	7 8.7
VOID RATIO:	2.30	1.14
CONSOLIDATION PARAMETER	RS	

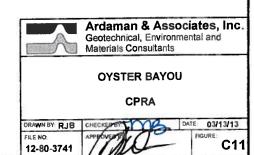
EFFECTIVE OVERBURDEN STRESS, $\sigma^{i}_{\nu\rho}$ (tsf):

PRECONSOLIDATION PRESSURE, o'p (tsf):

VIRGIN COMPRESSION RATIO, CR:

INCREMENTAL CONSOLIDATION TEST RESULTS

Confidential Information: Privileged & Confidential Work Product



0.094

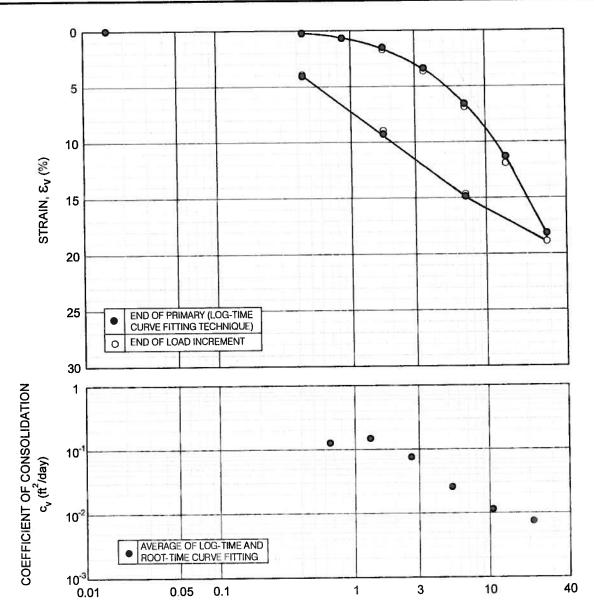
0.27 0.36

								_			_							_	-	~	*	_			_		_
_	C Q			1	1	1					0.01080	1		1	-	1							1	1		1	
·	Strain at EOI (%)		0.00	0.55	0.75	1.11																					
	Strain at EOP (%)		0.00	0.41	0.70	0.98	1.47				_		17.23														
	Void Ratio at EOI		2.2993							-	_	<u>,</u>	_			_	_	~	<u>~</u>	_	_	_	_				
	Void Ratio at EOP						2.2509				_	_	~	~	Ψ.				_			_	_	•	-	•	
	Height at EOI (inch)		0.7500	0.7459	0.7444	0.7417	0.7379	0.7281	0.6952	0.6634	0.6163	0.6175	0.6218	0.6218		0.6204	0.6182			0.5400	0.5116						
	Height at EOP (inch)		0.7500	0.7469	0.7448	0.7427	0.7390	0.7317	0.7057	0.6756	0.6226	0.6172	0.6208	0.6218	0.6216	0.6211	0.6193	0.6114	0.5913	0.5472	0.5180	0.4632	0.4603	0.4672	0.4756		
	Average Effective Stress	(ISI)		0.025	0.063	0.093	0.135	0.190	0.275	0.385	0.550	0.495	0.220	0.135	0.190	0.275	0.385	0.550	0.765	1.090	1.525	2.625	2.410	0.985	0.495	0.245	
	Cv (ft²/day)			3.46E-01	-	3.41E-01	1.50E-01	1.33E-01	7.62E-02	3.32E-02	1.51E-02	9.40E-02	5.57E-02			1.91E-01	1.90E-01	5.49E-02	1.54E-02	1.43E-02	1.06E-02	1.47E-02	3.34E-02	1.42E-02	5.50E-03	2.29E-03	
	Method (L≃log, S=sq π)			_		_	_	_	ر												بـ	٦	٦	_	_		
	Time, t ₁₀₀ (sec)			48		48	108	120	200	420	810	120	204			99	99	204	069	099	780	480	186	450	1200	3000	
£		EO.	0.0703	0.0744	0.1022	0.1154	0.1259	0.1362	0.1696	0.2022	0.2501	0.2483	0.2435	0.2428	0.2433	0.2450	0.2474	0.2605	0.2855	0.3272	0.3559	0.4136	0.4074	0.3995	0.3895	0.3785	
eadings (inc		ЕОР				0.1144	0.1248	0.1326	0.1591	0.1900	0.2438	0.2485	0.2445	0.2428	0.2433	0.2443	0.2463	0.2546	0.2755	0.3200	0.3495	0.4060	0.4082	0.4008	0.3916	0.3808	
Dial R		Initial	0.0701	0.0703	0.1007	0.1127	0.1221	0.1264	0.1367	0.1704	0.2030	0.2495	0.2478	0.2428	0.2431	0.2438	0.2452	0.2478	0.2613	0.2859	0.3275	0.3576	0.4129	0.4069	0.3987	0.3891	
	Effective Stress (tsf)		0	0.050	0.075	0.110	0.160	0.220	0.330	0.440	0.660	0.330	0.110	0.160	0.220	0.330	0.440	0.660	0.870	1,310	1.740	3.510	1.310	0.660	0.330	0.160	
	Dial Readings (inch)	Dial Readings (inch) Time, Method Cv Effective EOP EOI Ratio at Ratio at EOP (%) EOI (inch) (inch) (inch) (inch)	Dial Readings (inch) Time, (L=log, (1=log, sec) S=sq rt) Initial EOP EOI Time, (R2/day) Stress (inch) (inch) Average Height at Heigh	Dial Readings (inch) Method (L=log, log) Cv (L=log, log) Reflective EOP Height at EOP Height at EOP Height at EOP Void EOI Void EOP (%) Strain at EOP (%) EOI Ratio at EOP (%) EOI (%)	Dial Readings (inch) Dial Readings (inch) Line,	Dial Readings (inch) Line, Method Cv Effective EOP EO Ratio at Ratio at EOP EO Ratio at EOP EO EO	Dial Readings (inch) Time, Method Cv Effective EOP EO Ratio at Ratio at Strain at	Dial Readings (inch) Time, Method Cv Effective EOP EO Ratio at Ratio at Strain at	Dial Readings (inch) Filme, Method Cv Effective EOP EO Ratio at Ratio at Strain a	Dial Readings (inch) Filme, Method Cv Effective EOP EO Ratio at Ratio at Ratio at Ratio at Ratio at Ratio at Ratio at Ratio at Ratio at Ratio at Ratio at EOP (%) EO (%) EO	Dial Readings (inch) Line, Method Cv Effective EOP EO Ratio at Ratio at Ratio at Ratio at Ratio at EOP EO EO	Dial Readings (inch) Time, (II=log, Cv Effective EOP EO Ratio at Ratio at EOP (%) EO (%) E	Dial Readings (Inch) Time, (t=log, (t=log, 0.0703) Time, (sec) S=sq rf) Time, (t=log, 0.0703	Dial Readings (inch) Dial Readings (inch) Laboration Laboratio	Dial Readings (Inch) Time, Hethod Cv Effective EOP FOP For For EOP For For EOP For For EOP For For EOP For For EOP For For EOP For For EOP For For EOP For For EOP For For EOP For For EOP EOP E	Dial Readings (inch)	Dial Readings (Inch) Line, Method Cv Effective EOP EO E	Dial Readings (Inch) Time, Method Cv Effective EOP EOI Ratio at Ratio at Ratio at Strain at Strain at Strain at Strain at Strain at Strain at Strain at Initial EOP EOI Ratio at Ratio at Ratio at Ratio at Strain at Strain at Strain at Strain at Initial EOP EOI	Dial Readings (inch) Fivo (sec) Fivo (Dial Readings (inch) Line, Method CV Effective EOP EOI Ratio at Ratio at Strain at	Dial Readings (inch) Time, (i=iog) Time,	Dial Readings (Inch) Height at Height at Height at Height at Height at EOP (IL=10g, Cs=2) Height at Height at Height at EOP (IL=10g, Cs=2) Height at Height at EOP (IL=10g, Cs=2) Height at Height at EOP (IL=10g, Cs=2) Height at EOP (IL=10g, Cs=2) Height at EOP (IL=10g, Cs=2) Height at EOP (IL=10g, Cs=2) Height at EOP (IL=10g, Cs=2) Height at EOP (IL=10g, Cs=2) Height at EOP (IL=10g, Cs=2) Height at EOP (IL=10g, Cs=2) Height at EOP (IL=10g, Cs=2) Height at EOP (IL=10g, Cs=2) Height at EOP (IL=10g, Cs=2) Height at EOP (IL=10g, Cs=2) Height at EOP (IL=10g, Cs=2) Height at EOP (IL=10g, Cs=2) Height at It EOP (IL=10g, Cs=2) Height at It EOP (IL=10g, Cs=2) Height at It II EOP (IL=10g, IL=10	Dial Readings (Inct) Cv Effective EOP EOI Ratio at EOP (%) EOI (%) E	Dial Readings (inch)	Dial Readings (Inch) Time, Method Cv Effective EOP EOI Ratio at Ratio at EOP (%) EOI (%)	Dial Readings (Inch) Line, (sec) Lile, (rif) (ay) Stress (Inch) Lile, (Diel Readings (inch) Line, (sec) Carolino (inch) Carolino (inch) Erop (inch)

EOP= End of Primary Consolidation EOI= End of load increment (typically 24 hrs +/-)		Ring Diameter (in)	Ring weight (g)	Height of Solids (in)	>
Final Conditions	0.4860	116.0	78.7	112.3	1.1379
Initial Conditions	0.7500	94.6	51.0	100.2	2.2993
	Height (in)	yt (pct)	yd (pct)	Saturation (%)	Void ratio, e
Ovster Bayou	12-80-3741 R-08	4-6 (5.75)			
Project Name:	File Number:	Depth:			

ſ		m			—			081	224	037	177	080			—			046	425	84	988	084	1220	_			
		C		0.00	1	1	1					0.01080		1		1	1						0.01077	1	1	1	
ET		Strain at EOI (%)													•												33.04
₹ SHE		Strain at EOP (%)												<u> </u>													33.48
IMMAF		Void Ratio at EOI		2.2993 2.2993			• • • • • • • • • • • • • • • • • • • •			.,	_		<u> </u>	_	•	•	_	<u> </u>			_	_	<u>`</u>	_	_	•	1.2093
ST SU		Void Ratio at EOP			2.2960						.,	•••		-	-			_		_	_	-	_	_	_	•	1.1948
TION TE		Height at EOI (inch)			0.7481	0.7465												0.6280								0.4919	0.5022
SOLIDA		Height at EOP (inch)			0.7493	0.7468	0.7452	0.7411	0.7360	0.7203	0.6872	0.6448	0.6274	0.6298	0.6321	0.6316	0.6309	0.6291	0.6221	0.6014	0.5571	0.5358	0.4854	0.4749	0.4813	0.4906	0.4989
LOADING CONSOLIDATION TEST SUMMARY SHEET		Average Effective Stress	(tsf)		0.025	0.063	0.093	0.135	0.190	0.275	0.385	0.550	0.495	0.220	0.135	0.190	0.275	0.385	0.550	0.765	1.090	1,525	2.625	2.410	0.985	0.495	0.245
REMENTAL LOADING CONSOLIDATION		Cv (#²/day)	ļ		4.15E-01		2.45E-01	1.61E-01	1.29E-01	8.66E-02	3.67E-02	3.17E-02	1.34E-01	9.34E-02			2.94E-01	2.11E-01	7.64E-02	1.86E-02	1.15E-02	2.16E-02	2.09E-02	3.88E-02	2.03E-02	3.88E-03	3.40E-03
MENTAL	Method (L=log, S=sq rt)				s		s	s	S	s	s	s	s	s			S	S	s	s	s	S	S	S	S	s	S
INCREA		Time, t ₁₀₀ (sec)			173		290	437	540	777	1685	1750	375	540			173	240	653	2535	3650				4		
ENSIONAL INCREMENTAL	ch)		EOI	0.0703	0.0744	0.1022	0.1154	0.1259	0.1362	0.1696	0,2022		0.2483	0.2435											0.3995	0.3895	0.3787
	eadings (inch)		EOP	0.0703	0.0732	0.1019	0.1145	0.1254	0.1325	0.1547	0.1892	0.2319	0.2486	0.2451	0.2428	0.2433	0.2443	0.2463	0.2537	0.2749	0.3199	0.3435	0.3990	0,4086	0.4016	0.3908	0.3820
ONE-DIM	Dial Reading		Initial	0.0701	0.0725	0.1007	0.1132	0.1222	0.1279	0.1427	0.1710	0.2025	0.2495	0.2472	0.2435	0.2428	0.2436	0.2452	0.2478	0.2610	0.2862	0.3274	0.3590	0.4127	0.4068	0.3980	0.3890
		Effective Stress (tsf)	Villa V	0	0.050	0.075	0.110	0.160	0.220	0.330	0.440	0.660	0.330	0.110	0,160	0.220	0.330	0.440	0.660	0.870	1.310	1.740	3.510	1.310	0.660	0.330	0.160
				ـــــا	_										—	_				—							

EOP= End of Primary Consolidation EOI= End of load increment (typically 24 hrs +/-)		Specific Gravity 2.6942	Ring Diameter (in) 2,0000	Ring weight (g) 62.39		
Final Conditions	0.4860	47.4	116.0	7.8.7	112.3	1.1379
Initial Conditions	0.7500	85.5	94.6	51.0	100.2	2.2993
	Height (in)	w _c (%)	yt (pcf)	7d (pct)	Saturation (%)	Void ratio, e
Ovster Bavou	12-80-3741	B-08	4-6 (5.75)			
Project Name	File Number:	Boring Number:	Depth:	•		



SAMPLE DATA		
BORING NO.:	B-09	
SAMPLE NO.:		
DEDTH LICEETS.	24.5	

DEPTH (FEET): Tan and gray SILTY CLAY (CL) DESCRIPTION:

INDEX PROPERTIES		
LIQUID LIMIT (%):	39	
PLASTIC LIMIT (%)	20	
PLASTICITY INDEX (%):	19	
SPECIFIC GRAVITY	2.78	
-200(%):	100	

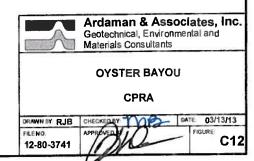
SPECIMEN CONDITIONS	INITIAL	FINAL
MOISTURE CONTENT (%):	44.4	42.7
DRY DENSITY (lb/ft3):	76.1	79.2
VOID RATIO:	1.28	1.19

CONSOLIDATION PARAMETERS

EFFECTIVE OVERBURDEN STRESS, o'vo (tsf):	0.825
PRECONSOLIDATION PRESSURE, o'p (tsf):	7.0
VIRGIN COMPRESSION RATIO, CR:	0.23

INCREMENTAL CONSOLIDATION TEST RESULTS

Confidential Information: Privileged & Confidential Work Product



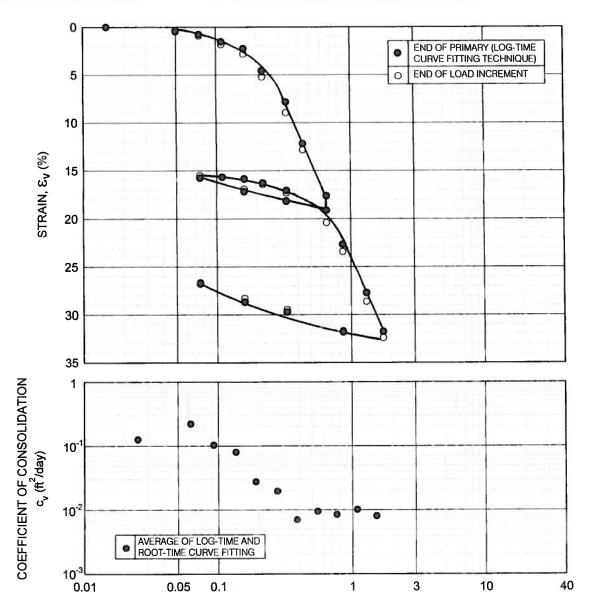
ARDAMAN & ASSOCIATES, INC GEOTECHNICAL TESTING LABORATORY ONE-DIMENSIONAL INCREMENTAL LOADING CONSOLIDATION TEST SUMMARY SHEET

		Cae	ı.		0.00066	0.00131	0.00185	0.00360	0.00552	0.00870	9	1	,	
ŀ			<u> </u>	1_							1	9	<u>၂</u>	
		Strain at EOI (%)						6.87	11.91		14.67	8.96	3.93	
		Strain at EOP (%)	0.00	0.20	0.67			6.57	11.31	18.15	14.86	9.27	4.07	
		Void Ratio at EOI	1.2815	1.2756	1,2654	1.2426	1.1982	1.1249	1.0099	0.8506	0.9469	1.0771	1.1918	
		Void Ratio at EOP	1.2815	1.2770	1.2663	1.2471	1.2043	1.1316	1.0236	0.8675	0.9425	1.0701	1.1887	-
		Height at EOI (inch)	0.7500	0.7481	0.7447	0.7372	0.7226	0.6985	0.6607	0.6084	0.6400	0.6828	0,7205	
בונה ה		Height at EOP (inch)	0.7500	0.7485	0.7450	0.7387	0.7246	0.7007	0.6652	0.6139	0.6386	0.6805	0.7195	
		Average Effective Stress (tsf)		0.228	0.655	1,305	2.625	5.275	10.570	21.230	17.700	4.390	1.090	
		Cv (ff²/day)			6.40E-02	1.24E-01	3.30E-02	1.93E-02	9.99E-03	5.90E-03	6.20E-03	3.47E-03	1.21E-03	rii
		Method (L=log, S=sq rt)			_	ب	٦	_			٦	؎		oj.
		Time,			258	132	480	780	1380	2040	1860	3720	12000	
	ch)	EOI	0.0109	0.0129	0.0171	0.0265	0.0432	0.0697	0.1102	0.1656	0.1316	0.0907	0.0540	
ONE DIMENSION	Dial Readings (inch)	EOP	0.0109	0.0124	0.0168	0.0250	0.0412	0.0675	0.1057	0.1600	0.1330	0.0930	0.0550	
ן יו	Dial R	Initial	0.0109	0.0109	0.0138	0.0190	0.0286	0.0456	0.0724	0.1132	0.1632	0.1335	0.0917	
		Effective Stress (tsf)	•	0.440	0.870	1.740	3.510	7.040	14.100	28.360	7.040	1.740	0.440	

EOP= End of Primary Consolidation		Specific Gravity 2.78	Ring Diameter (in) 1.9990	Ring weight (g) 62.52	Height of Solids (in) 0.3287	Neight of Dry Soil (g) 47.00
						Wei
Final	0.7205	42.7	113.0	79.2	266	1.1918
Initial	0.7500	44.4	109.8	76.1	36.2	1.2815
	Height (in)	(%) w (%)	yt (pal)	γd (pcf)	Saturation (%)	Void ratio, e
C	12-80-3741	B-09	33-35 B3 (34.5)			
	Floject Name:	Boring Number:	Depth:	•		

		C S S			1 0000	0.0000	0.00131	0.00185	0.00360	0.00552	0.008/0		1		 			
ET		Strain at EOI (%)								`				3.93				
Y SHE		Strain at EOP (%)										•	9.27	4.07	 	 		
MMAR		Void Ratio at EOI		ľ	•									1.1918	 		 -	
ST SU		Void Ratio at EOP		1.2815	1.2770			•					1.0701	1.1887	 <u></u>			
TION T		Height at EOI (inch)		0.7500			0.7372	0.7226	0.6985	0.6607			0.6828	0.7205				
SOLIDA		Height at EOP (inch)		0.7500	0.7485	0.7450	0.7387	0.7246	0.7007	0.6652	0.6139	0.6386	0.6805	0.7195				
NG CON		Average Effective Stress (tsf)			0.220	0.655	1.305	2.625	5.275	10.570	21.230	17.700	4.390	1.090			·-	
INCREMENTAL LOADING CONSOLIDATION TEST SUMMARY SHEET		Cv (ft²/day)	22			1.90E-01	1.73E-01	1.18E-01	3.20E-02	1.28E-02	9.00E-03	1.18E-02	3.62E-03					
MENTA		Method (L=log, S=sa rt)				တ	တ	တ	S	တ	S	တ	S					
		Time, t ₁₀₀ (sec)				375	406	576	2020	4640	5760	4200	15360			-		
ONE-DIMENSIONAL	ch)		E O	0.0109	0.0129	0.0171	0.0265	0.0432	0.0697	0.1102				0.0540				
DIMEN	Dial Readings (inch)		EOP	0.0109	0.0124	0.0168	0.0250	0.0412	0.0675	0.1057	0.1600	0.1330	0.0930	0.0550				
ONE-	Dial Re		Initial	0.0109	0.0109	0.0138	0.0190	0.0286	0.0456	0.0724	0.1132	0.1632	0.1335	0.0917				
		Effective Stress (tsf)		0	0.440	0.870	1.740	3.510	7.040	14.100	28.360	7.040	1.740	0.440	 			

tion	ically 24 hrs +/-)		2.78	1.9990	62.52	0.3287	47.00
EOP= End of Primary Consolidation	EOI= End of load increment (typically 24 hrs +/-)		Specific Gravity 2.78	Ring Diameter (in) 1	Ring weight (g)	_	Weight of Dry Soil (g)
Final	Conditions	0.7205	42.7	113.0	79.2	2.66	1.1918
Initial	Conditions	0.7500	4.4	109.8	76.1	96.2	1.2815
		Height (in)	(%) M	yt (pcf)	7d (pcf)	Saturation (%)	Void ratio, e
	Ovster Bayon	12-80-3741	B-03	33-35 B3 (34.5)	(2000) 22 22 22		
	Project Name:	File Number	Boring Number:	Denth:			



SAMPLE DATA

BORING NO.: SAMPLE NO.: DEPTH (FEET): B-10

DEPTH (FEET): 7.75
DESCRIPTION: Gray CLAY (CH)

INDEX PROPERTIES

LIQUID LIMIT (%):
PLASTIC LIMIT (%):
PLASTICITY INDEX (%):
SPECIFIC GRAVITY:
-200(%):

2.74 94

SPECIMEN CONDITIONS

 MOISTURE CONTENT (%):
 92.9
 59.8

 DRY DENSITY (lb/ft²):
 48.8
 67.7

 VOID RATIO:
 2.50
 1.52

INITIAL

CONSOLIDATION PARAMETERS

INCREMENTAL CONSOLIDATION TEST RESULTS

Confidential Information: Privileged & Confidential Work Product



Ardaman & Associates, Inc. Geotechnical, Environmental and Materials Consultants

OYSTER BAYOU

FINAL

CPRA

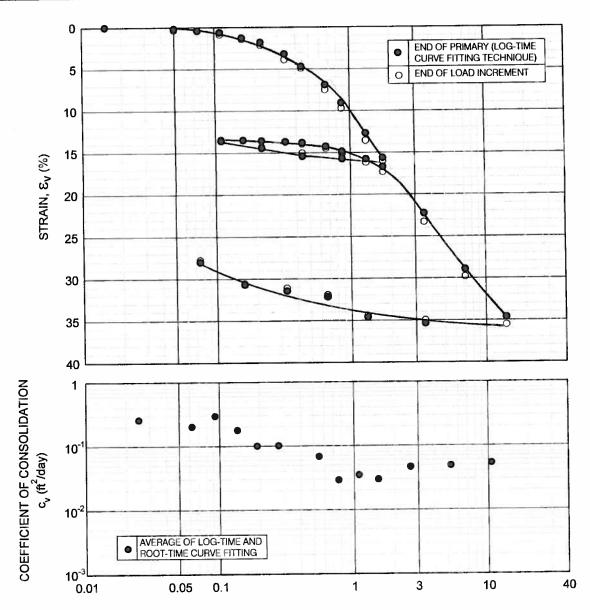
FILE NO 12-80-3741

DATE: 03/13/13
FIGURE: C13

EOP= End of Primary Consolidation FOI= End of load increment (typically 24 hrs +/-)		avity 2.7362	ır (in) 2.0000	Ring weight (g) 62.59	s (in) 0.2159	oil (g) 30.41
EOP= End of Primary C		Specific Gr	Ring Diamete	Ring weigh	Height of Solids (in)	Weight of Dry So
Final	0.5450	59.8	108.2	1.79	107.4	1.5245
Initial	0.7560	92.9	94.1	48.8	101.6	2.5019
	Height (in)	Wc (%)	yt (pcf)	7d (pct)	Saturation (%)	Void ratio, e
10000	12-80-3741	B-10	6-8 (7.75)			
N to See See See See See See See See See Se	lumber:	a Number:	. :-			

жеет		Strain at Strain at C α e EOP (%) EOI (%)	0.00 0.00		0.93	1.80	2.82	5.24	9.01							15.91	16.41	17.28		23.39	28.62		31.70 31.49	29.87 29.25	28.56 28.08	26.42 26.42	
ENSIONAL INCREMENTAL LOADING CONSOLIDATION TEST SUMMARY SHEET		Void Stra	2.5019	2.4848	2.4695	2.4389	2.4032	2.3185															1.3992	1.4775	1.5187	1.5766	
EST SU		Void Ratio at EOP	2.5019	2.4875			2.4236	2.3513	2.2411	.,	1.8872	1.8585	1.8849	1.9377	1.9560	1.9486	1.9356	1.9069	1.8351	1.7221	1.5563	1.4173	1.3918	1.4557	1.5016	1.5766	
TION TI		Height at EOI (inch)	0.7560	0.7523	0.7490		0.7347		0.6879	0.6586	0.6112	0.6188	0.6280		0.6374	0.6358		0.6254		0.5792	0.5397	0.5130	0.5180	0.5349	0.5438	0.5563	
SOLIDA		Height at EOP (inch)	0.7560	0.7529	0.7502	0.7449	0.7391	0.7235	0.6997	0.6675	0.6233	0.6171	0.6228	0.6342	0.6382	0.6366	0.6338	0.6276	0.6121	0.5877	0.5519	0.5219	0.5164	0.5302	0.5401	0.5563	
NG CON		Average Effective Stress (tsf)	,	0.025	0.063	0.093	0.135	0.130	0.275	0.385	0.550	0.495	0.245	0.118	0.093	0.135	0.190	0.275	0.495	0.765	1.090	1.525	1.305	0.600	0.245	0.118	
LLOADII		Cv (ff²/day)		1.18E-01	1.77E-01	1.09E-01	8.09E-02	3,25E-02	2.38E-02	8.38E-03	1.08E-02	1.52E-01	1.21E-01	2.13E-02	2.68E-01	1.63E-01	1.09E-01	3.99E-02	3.85E-02	9.94E-03	1.24E-02	9.13E-03	7.74E-02	1.86E-02	8.71E-03		
MENTA		Method (L=log, S=sq rt)		ဟ	S	ဟ	S	ဟ	တ	ဟ	တ	S	S	S	S	S	S	တ	တ	တ				S			
INCRE		Time, t ₁₀₀ (sec)		614	406	653	998	2089	2693	8669	4860	317		2381		318		1270		4541				_	•		
SIONAL	ich)	EOI	0.0724	0.0761	0.0794	0.0862	0.0939	0.1122	0.1406	0.1699	0.2173							0.2053		0.2517			0	0			
	eadings (inch)	EOP	0.0735	0.0755	0.0782	0.0837	0.0895	0.1051	0.1288	0.1610	0.2052	0.2133	0.2075	0.1960	0.1921			0.2031	0.2188	0.2432	0.2790	0.3090	0.3140			0.2731	
ONE-DIN	Dial Readir	Initial	0.0735	0.0724	0.0761	0.0796	0.0862	0.0939	0.1121	0.1406	0.1699	0.2192	0.2115	0.2022	0.1914	0.1929	0.1946	0.1987	0.2055	0.2288	0.2517	0.2912	0.3174	0.3115	0 2946	0.2856	
		Effective Stress (tsf)	•	0.050	0.075	0.110	0.160	0.220	0.330	0.440	0.660	0.330	0.160	0.075	0.110	0.160	0.220	0.330	0.660	0.870	1.310	1.740	0.870	0.330	0 160	0.075	

EOP= End of Primary Consolidation	EOI= End of load increment (typically 24 hrs +/-)		Specific Gravity 2.7362	Ring Diameter (in) 2.0000	Ring weight (g) 62.59		
Final	Conditions	0.5450	59.8	108.2	67.7	107.4	1.5245
Initial	Conditions	0.7560	92.9	1.46	48.8	101.6	2.5019
		Height (in)	w. (%)	yt (pct)	yd (pct)	Saturation (%)	Void ratio e
	Ovster Bayou	12-80-3741	B-10	6-8 (7.75)			
	Project Name:	File Number:	Boring Number:	Depth:			



B-11
3.75
Gray CLAY (CH)
w/organics
93
25
68
2.73
77

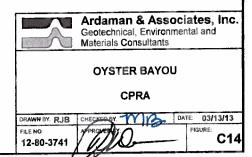
SPECIMEN CONDITIONS	INITIAL	FINAL
MOISTURE CONTENT (%): DRY DENSITY (lb/lt³): VOID RATIO:	66.1 60.6 1.81	41.0 80.8 1.11

CONSOLIDATION PARAMETERS

EFFECTIVE OVERBURDEN STRESS, σ'_{vo} (tsf):	0.062
PRECONSOLIDATION PRESSURE, σ_p (tsf):	0.6
VIRGIN COMPRESSION RATIO, CR:	0.22
RECOMPRESSION RATIO, RR:	0.04

INCREMENTAL CONSOLIDATION TEST RESULTS

Confidential Information: Privileged & Confidential Work Product



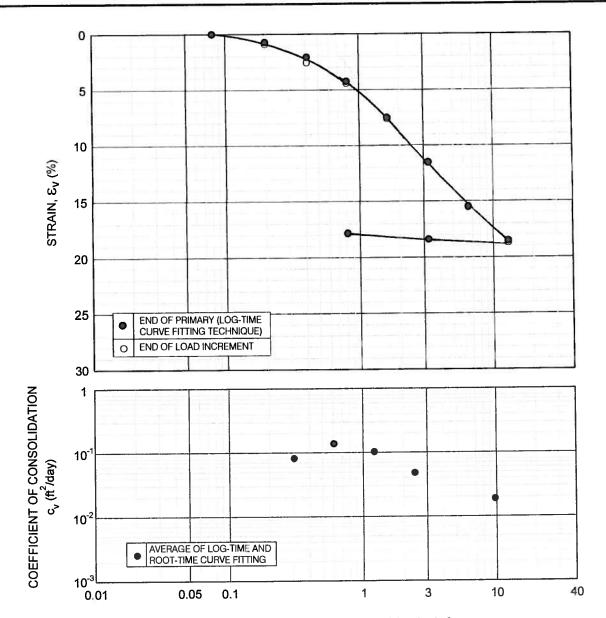
		ပ အ		1	1		1	1		0.00355		0.00701	0.00760	0.00730	0.00793	1	1		1				l	_	0.00133	0.00200								1		-	
		Strain at EOI (%)		00:0	0.33	4	0.85	141	2.14	3.89	08.4	7.47	0.0	3.00	16.02	5.65	15.03	4.30	13.43	13.50	3.59	13./1	3.94	14.46	15.13	2 5	17.31									27.11	
Y SHEE		Strain at EOP (%)		0.0	0.15	0.39	0.60	1.27	1.78	3.19	4.70	6.89	0.0	12.68	15.62	15.74	15.42	14.44	13.57			13.67		•				25.22								27.98	
MMAR		Void Ratio at EOI		1,8108	1.8015	1.7984	1.7869	1.7711	1.7506	1.7015	1.6730	1.6008	٠.		_	_	•	Ξ.	-		`	•	•		٠		•									1.0303	
ST SU		Void Ratio at EOP		1.8108	1.8065	1.7999	1.7939	-	-	<u>'</u>	'	_	•	_	_	_	٠	_	_		-	•	_	_		`	•						_		_	1,0242	
I NOL		Height at EOI (inch)		0.7590	0.7565	0.7557	0.7526	0.7483	0.7428	0,7295	0.7218	0.7023	0.6854	0.6561	0.6374	0.6402	0.6450	0.6505	0.6571	0.6566	0.6559	0.6550	0.6532	0.6493			0.6277			0.4894				_	_	0.5483	
SOLIDA		Height at EOP (inch)		0.7590	0.7579	0.7561	0.7545	0.7494	0.7455	0.7348	0.7233	0.7067	0.6903	0,6628	0.6405	0.6395	0.6420	0.6494	0.6560	0.6587				0.6509	0.6463							0.4964	0.5152	0.5205		0.5466	
G CON		Average Effective Stress	i		0.025	0.063	0.093	0.135	0.190	0.275	0.385	0.550	0.765	1,090	1.525	1.305	0.655	0.330	0.165	0.135	0.190	0,275	0.385	0.550	0.765	1,090	1.525	2,625	5.275	10.570	8.805	2.410	0,985	0.495	0.245	0.118	
ONE-DIMENSIONAL INCREMENTAL LOADING CONSOLIDATION TEST SUMMARY SHEET		Cv (ft²/day)			2.84E-01		3.76E-01	1.86E-01	9.19E-02	5.39E-02		2.80E-02	2.00E-02	2.36E-02	1.09E-02	2,24E-01	6.77E-02	2.07E-02	8.43E-03		2.84E-01	2.12E-01	2.12E-01	1.17E-01	1,22E-01	1.27E-01	1.42E-01	3.05E-02	3.11E-02	4.36E-02	1	3,36E-02	1.10E-02	2.66E-03	1.84E-03	1.51E-03	
MENTA		Method (L=log, S=sq rt)	Ä				_		ب	_		٦	ب	-	_		_	_			ر		_	٦	_	ר	ר	-1	ب	_		ب	٦	ب	۔۔		
NCREN		Time, t ₁₀₀ (sec)	-		09		45	06	180	300		540	720	570	1140	\$	180	009	1500		45	99	99	108	102	96	8	360	300	180		216	069	3000	4440	5640	
IONAL I	£		<u></u>	6660 0	0.1028	0.1038	0.1073	0.1123	0.1196	0.1333	0.1412	0.1614	0.1784	0.2082	0.2271	0.2235	0.2184	0.2125	0.2058	0.2063	0.2072	0.2083	0.2101	0.2142	0.2196	0.2278	0,2366	0.2828	0.3325	0,3769	0.3689	0.3843	0.3436	0.3372	0.3328	0.3114	
DIMENS	Dial Readings (Inch)		EOP	0 1002	0.1014	0.1034	0.1054	0.1112	0.1168	0.1280	0.1397	0.1570	0.1734	0.2015	0,2240	0.2242	0.2214	0.2136	0.2068	0.2062	0.2069	0.2080	0.2090	0.2126	0.2175	0.2246	0.2320	0.2750	0.3260	0,3702	0,3716	0.3656					
ONE-	Dial R		Initial	0.1002	0.1003	0.1030	0.1042	0.1081	0.1140	0.1200	0.1335	0.1419	0.1614	0.1789	0.2084	0.2263	0.2231	0.2181	0.2123	0.2058	0.2065	0.2074	0.2084	0.2103	0.2145	0.2199	0.2280	0.2376	0.2830	0.3334	0.3729	0.3686	0.3825	0.3435	0.3369	0.3326	
		Effective Stress (tsf)		,	0.050	0.075	0.110	0.160	0.220	0.330	0.440	099'0	0.870	1.310	1.740	0.870	0.440	0.220	0.110	0.160	0.220	0.330	0.440	0.660	0.870	1.310	1.740	3.510	7.040	14,100	3.510	1 310	0.860	0330	0.160	0.075	

EOP= End of Primary Consolidation EOI= End of load increment (typically 24 hrs +/-) Specific Gravity 2.7306 Ring Diameter (in) 2.0000 Ring weight (g) 62.61 Height of Solids (in) 0.2700 Weight of Dry Soil (g) 37.96
Final Conditions 0.5700 41.0 113.9 80.8 100.8
Conditions 0.7590 66.1 100.7 60.6 99.7 1,8108
Height (m) w _c (%) yt (pcf) yd (pcf) Saturation (%) Void ratio, e
Oyster Bayou 12-80.3741 B-11 2-4 (3.75)
Project Name: File Number; Boring Number; Depth:

ARDAMAN & ASSOCIATES, INC GEOTECHNICAL TESTING LABORATORY ONE-DIMENSIONAL INCREMENTAL LOADING CONSOLIDATION TEST SHAMMARY SHEET

		ONE-DIMENSIONAL INCREMENTAL LOADING CONSOLLIDATION LEST SOMMART STEEL	NOTATE L			127				<u>}</u>		5		
	Dial R	Dial Readings (Inch	ਓ											
Effective Stress				Time,	Method (L=log,	Cv Cv	Average Effective	Height at EOP	Height at EOI	- 4	#	Strain at	Strain at	COE
(tsf)	Initial	EOP	EOI		S=sq rð	(feed a)	(tst)	(inch)	(inch)	EOP	<u> </u>			
0	0.1002	0.1002	0.0999				-	0.7590	0.7590	1.8108	1.8108	00.00	0.00	
0.050	0.1003	0.1014	0.1028	318	s	2.31E-01	0.025	0.7579	0.7565	1.8067	1.8015	0.14	0.33	1
0.075	0.1027	0.1034	0.1038	360	S	2.03E-01	0.063	0.7559	0.7554	1.7991	1.7976	0.42	0.47	1
0.110	0.1042	0.1058	0.1073	345	s	2.11E-01	0.093	0.7539	0.7523	1.7918	1.7861	0.67	0.88	
0.160	0.1080	0.1112	0.1123	420	s	1.71E-01	0.135	0.7491	0.7480	1.7741	1.7702	1.30	4.	
0.220	0.1140	0.1166	0.1196	653	s	1.09E-01	0.190	0.7454	0.7425	1.7605	1.7496	1.79	2.18	
0.330	0.1200	0.1251	0.1333	470	v	1.49E-01	0.275	0.7374	0.7292	1.7307	1.7006	2.85	3.92	0.00355
0.440	0.1335	0.1397	0.1412				0.385	0.7230	0.7215	1.6776	1.6720	4.74	4.94	1
099'0	0.1421	0.1505	0,1614	614	Ø	1.07E-01	0.550	0.7131	0.7022	1.6409	1.6006	6.04	7.48	0.00701
0.870	0.1614	0.1700	0.1784	1622	ဟ	3.83E-02	0.785	0.6936	0.6853	1.5687	1.5378	8,61	9.71	0.00763
1,310		0.1959	0.2082	1270	Ø	4.60E-02	1.090	0.6683	0.6560	1.4748	1.4295	11.95	13.57	0.00750
1.740	0.2082	0.2171	0.2271	1109	S	4.89E-02	1,525	0.6471	0.6372	1.3965	1.3597	14.74	16.05	0.00793
0.870	0.2263	0.2245	0.2235	194	S	2.68E-01	1,305	0.6390	0.6400	1.3663	1,3700	15.81	15.68	
0.440	0,2231	0.2205	0.2184	375	S	1.40E-01	0,655	0.6426	0.6447	1,3797	1.3876	15.34	15.05	1
0.220	0.2183	0.2154	0.2125	735	s	7.25E-02	0.330	0.6476	0.6505	1.3984	1.4091	14.67	14.29	
0.110	0,2124	0.2085	0.2058	2774	S	1.96E-02	0.165	0.6544	0.6572	1.4236	1.4337	13.78	13.41	1
0.160	0.2058	0.2061	0.2063				0.135	0.6569	0.6567	1.4326	1.4319	13.45	13.48	
0.220	0.2065	0.2067	0,2072	438	s	1.26E-01	0.130	0.6564	0.6559	1.4310	1.4291	13.51	13,58	1
0.330	0.2072	0.2076	0.2083	154	s	3,56E-01	0.275	0.6555	0.6548	1.4276	1.4250	13.63	13.72	1
0.440	0.2083	0.2090	0.2101	317	s	1.72E-01	0,385	0.6541	0.6530	1.4224	1.4184	13.82	13,96	1
099'0	0.2103	0.2124	0.2142	406	S	1,34E-01	0.550	0.6509	0.6491	1.4106	1.4039	14.24	14.47	0.00108
0.870	0.2145	0.2171	0.2196	346	s	1.55E-01	0.765	0.6465	0.6441	1.3943	1.3852	14.82	15.14	0.00133
1,310		0.2242	0.2278	317	S	1.66E-01	1.090	0.6397	0.6361	_	•	15.72	16.19	0.00217
1.740	0.2280	0.2309	0.2366	240	S	2.14E-01	1.525	0.6332	0.6275	_	•	16.58	17.32	0.00289
3,510	0.2380	0.2679	0.2828	778	ဟ	6.16E-02	2,625	0.5976	0.5827	1.2132		21.26	23.22	
7.040	0.2830	0.3152	0.3325	614	S	6.67E-02	5,275	0,5505	0.5333	1.0388		27.47	29.74	_
14.100	0,3340	0.3634	0.3769	540	s	6.38E-02	10,570	0.5039	0.4904			33.61	35.39	0.00682
3.510	0.3769	0.3710	0.3689	540	s	5.75E-02	8.805	0.4963	0.4984			34.61	34.34	1
1.310	0.3684	0.3660	0.3643	998	s	3.68E-02	2.410	0.5008	0.5025	-		34.02	33.80	1
0.660	0.3621	0.3482	0.3436	2458	s	1.35E-02	0.985	0.5164	0.5210			31.96	31.36	1
0.330	0.3436	0.3396	0.3372	5529	s	6.31E-03	0.495	0.5250	0.5274			30.83	30.51	
0.160	0.3372	0.3351	0.3328		ဟ	9.52E-03	0.245	0,5295	0.5318		_	30.23	29.93	
0.075	0,3328	0.3164	0,3114	15360	S	2.42E-03	0.118	0.5482	0.5533	1,0303	1.0490	27.77	27.10	1
š			i.					0						
					\rceil							1		

lidation typically 24 hrs +/-)				62.61	0.2700	37.86
EQP= End of Primary Consolidation EQI= End of load increment (typically 24 hrs +/L)		Specific Gravity	Ring Diameter (in)	Ring weight (g)	Height of Solids (in)	Weight of Dry Soil (g)
Final	0.5700	41.0	113.9	80.8	100.8	1.1109
Initial Conditions	0,7590	66.1	100.7	9'09	2.66	1.8108
	Height (in)	Wc (%)	71 (pd)	yd (bct)	Saturation (%)	Void ratio, e
Oyster Bayou	12-80-3741	B-11	2-4 (3.75)	•		
Project Name:	File Number:	Boring Number:	Depth:			



SAMPLE DATA	
BORING NO.: SAMPLE NO.:	B-12
DEPTH (FEET):	28.25
DESCRIPTION:	Tan and gray CLAY (CH) w/silty sand layers
INDEX PROPERTIES	
LIQUID LIMIT (%):	59
PLASTIC LIMIT (%):	17
PLASTICITY INDEX (%):	42
SPECIFIC GRAVITY:	2.69
-200(%):	88

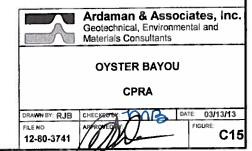
SPECIMEN CONDITIONS	INITIAL	FINAL
MOISTURE CONTENT (%):	33,8	32.6
DRY DENSITY (Ib/ft3):	87.5	91.1
VOID RATIO:	0.92	0.84

CONSOLIDATION PARAMETERS

EFFECTIVE OVERBURDEN STRESS, o'vo (tsf):	0.635
PRECONSOLIDATION PRESSURE, o'p (tsf):	0.80
VIRGIN COMPRESSION RATIO, CR:	0.132

INCREMENTAL CONSOLIDATION TEST RESULTS

Confidential Information. Privileged & Confidential Work Product

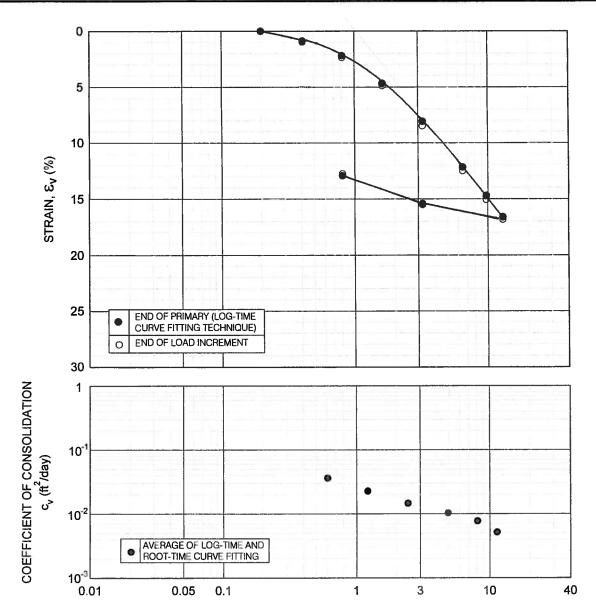


		O C G		1				1	-		1		1		
티		Strain at EOI (%)							•					12.62	
Y SHE		Strain at EOP (%)				2.07								12.99	
IMMAR		Void Ratio at EOI												0.6776	
EST SL		Void Ratio at EOP						0.7761						0.6704	
LION		Height at EOI (inch)		0.7500	0.7433	0.7308	0.7169	0.6929	0.6634	0.6336	0.6097	0.6121	0.6166	0.6554	
SOLIDA		Height at EOP (inch)		0.7500	0.7446	0.7345	0.7182	0.6939	0.6639	0.6340	0.6111	0.6121	0.6162	0.6526	
NO SON		Average Effective Stress (tsf)			0.100	0.305	0.610	1.218	2.438	4.875	9.750	8.125	2.030	0.505	
AL INCREMENTAL LOADING CONSOLIDATION TEST SUMMARY SHEET		Cv (ff²/day)			•	7.71E-02	1.18E-01	1.29E-01	5.68E-02		1.06E-02	3.69E-01	3.11E-02	2.84E-03	
MENTA		Method (L=log, S=sa rt)				ب	ت	_	ب				_	ب	
SEC INCREI		Time, t ₁₀₀ (sec)	_			210					1080	30	360	4200	
SIONAL	ਚਿੰ		<u>O</u>	0.0662	0.0730	0.0857	0.1003			0.1879	0.2144	0.2110	0.2065	0.1172	
ONE-DIMENSION	Dial Readings (inch)		EOP	0.0662	0.0716	0.0820	0.0990	0.1243	0.1558	0.1875	0.2130	0.2110	0.2068	0.1200	
ONE	Dial R		nitial	0.0662	0.0662	0.0732	0.0864	0.1013	0.1268	0.1581	0.1905	0.2134	0.2109	0.1560	
		Effective Stress	(3)		0.200	0.410	0.810	1.625	3.250	6.500	13.000	3.250	0.810	0.200	

EOP= End of Primary Consolidation	EOI= End of load increment (typically 24 hrs +/-)					Height of Solids (in) 0.3907	Weight of Dry Soil (g) 54.10
Final	Conditions	0.7200	32.6	120.8	91.1	104.0	0.8431
Initial	Conditions	0.7500	33.8	117.0	87.5	98.8	0.9199
		Height (in)	W _c (%)	γt (pcf)	√d (bct)	Saturation (%)	Void ratio, e
	Oyster Bayou	12-80-3741	B-12	28-30 B1 (28.25)			
	Project Name:	File Number:	Boring Number:	Depth:	§		

		C O		-	1	1		1		1	1	I		l				
ET		Strain at EOI (%)												12.62				
Y SHE		Strain at EOP (%)	:											12.99			 	
MMAR		Void Ratio at EOI							0.6980					0.6776		 		
EST SU		Void Ratio at EOP		0.9199					0.7111		0.5877		0.5779	0.6704	·			
TION		Height at EOI (inch)		0.7500	0.7433	0.7308	0.7169	0.6929	0.6634	0.6336	0.6097	0.6121	0.6166	0.6554				
SOLIDA'		Height at EOP (inch)		0.7500	0.7446	0.7332	0.7182	0.6952	0.6685	0.6387	0.6203	0.6121	0.6164	0.6526				
NG CON		Average Effective Stress (tsf)			0.100	0.305	0.610	1.218	2.438	4.875	9.750	8.125	2.030	0.505				
AL INCREMENTAL LOADING CONSOLIDATION TEST SUMMARY SHEET		Cv (ff²/day)				8.69E-02		1.59E-01	7.58E-02		3.95E-02		2.71E-02					
MENTA		Method (L=log, S=sq rt)	5			တ		တ	S		တ		S			 		
INCRE		Time, t ₁₀₀ (sec)				800		400	780		1270		1780					
SIONAL	ch)	1	EO	0.0662	0.0730	0.0857	0.1003							0.1172				
ONE-DIMENSION	Dial Readings (inch)		EOP	0.0662	0.0716	0.0833	0.0990	0.1230	0.1512	0.1828	0.2038	0.2110	0.2066	0.1200	- 	 	6.9	
ONE	Dial R		Initial	0.0662	0.0662	0.0732	0.0864	0.1013	0.1268	0.1581	0.1905	0.2134	0.2109	0.1560				
		Effective Stress	(ig)		0.200	0.410	0.810	1.625	3 250	6.500	13.000	3.250	0.810	0.200				

EOP= End of Primary Consolidation EOI= End of load increment (typically 24 hrs +/-)		•			Weight of Dry Soil (g) 54.10
Final Conditions	0.7200 32.6	120.8	91.1	104.0	0.8431
Initial	0.7500 33.8	117.0	87.5	98.8	0.9199
	Height (in) w _c (%)	γ t (pcf)	γ d (pcf)	Saturation (%)	Void ratio, e
Oyster Bayou	12-80-3741 B-12	28-30 B1 (28.25)	•		
Project Name:	File Number: Boring Number:	Depth:	•		



VERTICAL EFFECTIVE STRESS, $\sigma^{\scriptscriptstyle t}_{\ vc}$ (tsf)

SAMPLE DATA	
BORING NO.;	B-14
SAMPLE NO.:	
DEPTH (FEET):	33.75
DESCRIPTION:	Gray SILTY CLAY (CL)
	w/sand
INDEX PROPERTIES	
LIQUID LIMIT (%):	49
PLASTIC LIMIT (%):	20
PLASTICITY INDEX (%):	29
SPECIFIC GRAVITY:	2.74
-200(%);	92

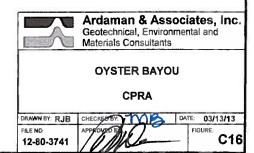
SPECIMEN CONDITIONS	INITIAL	FINAL
MOISTURE CONTENT (%):	33.9	30.4
DRY DENSITY (lb/ft3):	87.6	93.2
VOID RATIO:	0.96	0.84

CONSOLIDATION PARAMETERS

EFFECTIVE OVERBURDEN STRESS, a'vo (tsf):	0.80
PRECONSOLIDATION PRESSURE, o', (tsf):	1.7
VIRGIN COMPRESSION RATIO, CR:	0.145

INCREMENTAL CONSOLIDATION TEST RESULTS

Confidential Information: Privileged & Confidential Work Product

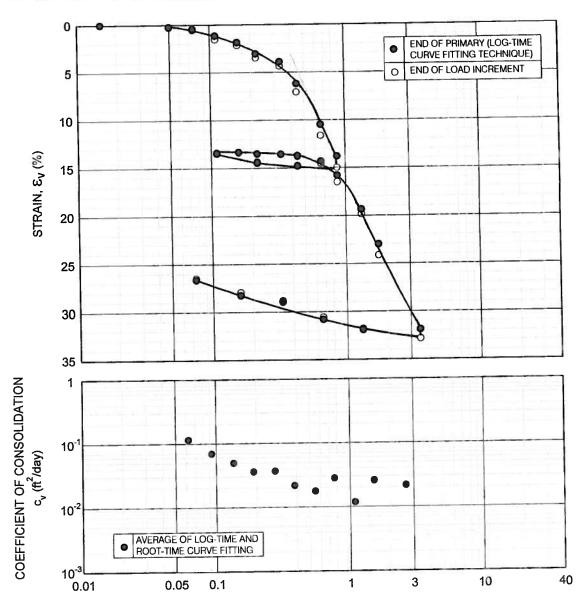


		COE			١	0.00126	0.00200	0.00333	0.00316	0.00367	0.00271	1	1					
		Strain at EOI (%)		0.00	0.97	2.35	4.87	8.47	12.49	15.05				4.32				
Y SHE		Strain at EOP (%)		00.0	0.88							15.49	12.92	4.73	 			
MMAR		Void Ratio at EOI		0.9551		0.9091	0.8598							0.8706	 			
ST SU		Void Ratio at EOP		0.9551	0.9379	0.9122	0.8640	0.7972	0.7173	0.6674	0.6305	0.6523	0.7025	0.8627				
TION TE		Height at EOI (inch)	***************************************	0.7500	0.7427	0.7324	0.7135	0.6865	0.6564	0.6371	0.6239	0.6347	0.6544	0.7176			-, -	
SOLIDA		Height at EOP (inch)		0.7500	0.7434	0.7336	0.7151	0.6895	0.6588	0.6397	0.6255	0.6339	0.6531	0.7146				
NO SON		Average Effective Stress (tsf)		E	0.205	0.610	1.218	2.438	4.875	8.125	11.375	8.125	2.030	0.610		-		
AL INCREMENTAL LOADING CONSOLIDATION TEST SUMMARY SHEET		Cv (ft²/day)				2.96E-02	1.99E-02	1.06E-02	9.72E-03	7.16E-03	4.69E-03	1.63E-02	3.41E-03					
MENTA		Method (L=log, S=sq rt)	-			_	٦	_	_	_	ب	ب	ب		 			
INCREI		Time, t ₁₀₀ (sec)				546	780	1380	1380	1740	2520	720	3600					
SIONAL	ch)		<u></u>	0.1544	0.1617	0.1724	0.1921	0.2202	0.2518	0.2708	0.2839	0.2718	0.2514	0.1860				
ONE-DIMENSION	Dial Readings (inch)		EOP	0.1544	0.1610	0.1712	0 1905	0.2172	0.2493	0.2682	0.2823	0.2726	0.2526	0.1890		-		
ONE	Dial R		Initial	0.1544	0.1544	0.1621	0.1732	0.1932	0.2217	0.2515			0.2710	0.2492				
		Effective Stress	ì		0.410	0.810	1 625	3 250	6,500	9.750	13.000	3.250	0.810	0.410				

ation	pically 24 hrs +/-)		2.7431	1.9990	1) 62.53	0.3836	54.12
EOP= End of Primary Consolidation	EOI= End of load increment (typically 24 hrs +/-)		Specific Gravity 2.7431	Ring Diameter (in)	Ring weight (g)		Weight of Dry Soil (g)
Final	Conditions	0.7050	30.4	121.5	93.2	99.5	0.8378
nitia	Conditions	0.7500	33.9	117.3	87.6	97.4	0.9551
		Height (in)	(%) M	γt (pcf)	7d (pct)	Saturation (%)	Coita ratio
	Oyster Bayon	12-80-3741	B-14	33-35 B4 (33 75)	(2.1.2) 12.22-22		
	Project Name:	File Number	Boring Mumber	Depth:	-		

		O O				0.00126	0.00200	0.00333	0.00316	0.00367	0.00271					
ET		Strain at EOI (%)		-00'0	- 0.97	2.35	4.87	8.47	12.49	15.05		15.37	12.75	4.32	ź	
Y SHE		Strain at EOP (%)		0.00	0.88	2.19	4.66	8.07	12.16	14.71	16.60	15.49	12.92	4.73		
MMAR		Void Ratio at EOI		0.9551	0.9360	0.9091	0.8598	0.7894	0.7109	0.6608	0.6264	0.6545	0.7057	0.8706		
EST SU		Void Ratio at EOP		0.9551	0.9379	0.9122	0.8640	0.7972	0.7173	0.6674	0.6305	0.6523	0.7025	0.8627		
TION TI		Height at EOI (inch)		0.7500	0.7427	0.7324	0.7135	0.6865	0.6564	0.6371	0.6239	0.6347	0.6544	0.7176		
SOLIDA		Height at EOP (inch)		0.7500	0.7434	0.7336	0.7151	0.6895	0.6588	0.6397	0.6255	0.6339	0.6531	0.7146		
NG CON		Average Effective Stress (tsf)			0.205	0.610	1.218	2.438	4.875	8.125	11.375	8.125	2.030	0.610		
ONE-DIMENSIONAL INCREMENTAL LOADING CONSOLIDATION TEST SUMMARY SHEET		Cv (ft²/day)				4.29E-02	2.56E-02	1.86E-02	1.09E-02	8.26E-03	5.70E-03	2.05E-02	3.82E-03			
MENTA		Method (L=log, S=sq rt)				S	S	ဟ	S	တ	တ	ဟ	Ø			
INCRE		Time, t ₁₀₀ (sec)				1620	2610	3375	2300	6490	8930	2460	13860			
SIONAL	ch)		EŌ	0.1544	0.1617	0.1724	0.1921	0.2202	0.2518	0.2708	0.2839	0.2718	0.2514	0.1860		
DIMEN	Dial Readings (inch)		EOP	0.1544	0.1610	0.1712	0.1905	0.2172	0.2493	0.2682	0.2823	0.2726	0.2526	0.1890		
ONE	Dial R		nitia	0.1544	0.1544	0.1621	0.1732	0.1932	0.2217	0.2515	0.2707	0.2826	0.2710	0.2492		
		Effective Stress (tsf)		0	0.410	0.810	1.625	3.250	6.500	9.750	13.000	3.250	0.810	0.410		

EOP = End of Primary Consolidation	EOI= End of load increment (typically 24 hrs +/-)		Specific Gravity 2.7431	Ring Diameter (in) 1.9990	Ring weight (g) 62.53	Height of Solids (in) 0.3836	Weight of Dry Soil (g) 54.12
		0.7050	30.4	121.5	93.2	99.5	0.8378
nital	Conditions	0.7500	33.9	117.3	87.6	97.4	0.9551
		Height (in)	Wc (%)	γ t (pcf)	yd (bal)	Saturation (%)	Void ratio, e
	Oyster Bayou	12-80-3741	B-14	33-35 B1 (33.75)			
	Project Name:	File Number:	Boring Number:	Depth:			



SAMPLE DATA	
BORING NO.:	B-15
SAMPLE NO.:	
DEPTH (FEET):	13.75
DESCRIPTION:	Gray CLAY (CH)
	w/silt
INDEX PROPERTIES	
LIQUID LIMIT (%):	90
PLASTIC LIMIT (%):	25
PLASTICITY INDEX (%):	65
SPECIFIC GRAVITY:	2.75

INITIAL	FINAL
85.3	54.8
52.0	71.2
2.31	1.41
	85.3 52.0

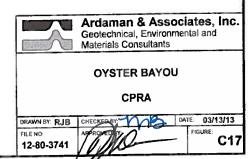
CONSOLIDATION PARAMETERS

EFFECTIVE OVERBURDEN STRESS, o'vo (tsf):	0.226
PRECONSOLIDATION PRESSURE, o'p (tsf):	0.36
VIRGIN COMPRESSION RATIO, CR:	0.28
RECOMPRESSION RATIO, RR:	0.025

INCREMENTAL CONSOLIDATION TEST RESULTS

Confidential Information. Privileged & Confidential Work Product

-200(%):



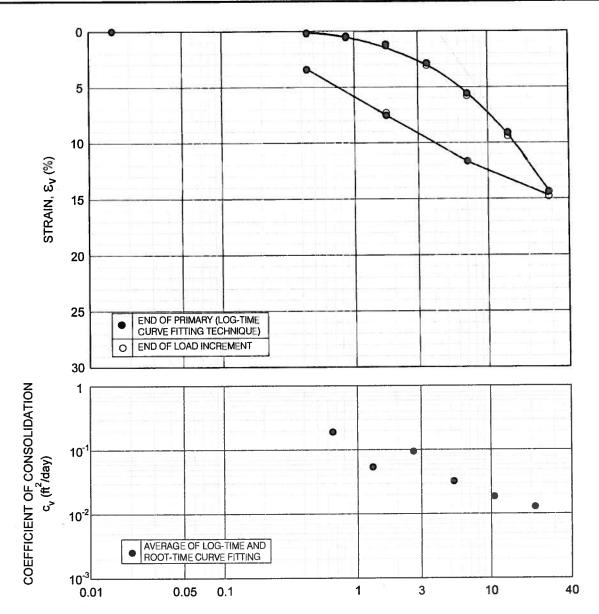
		SIONAL	INCRE INCRE	MENIA	ONE-DIMENSIONAL INCREMENTAL LOADING CONSOLIDATION TEST SUMMARY	200 200 200 200 200 200 200 200 200 200	SOLIDA	NO	באו אם	MIMA	Y SHEEL		
ia F	Dial Readings (inch)	ਓ											
Initial	EOP	EOI	Time, t ₁₀₀ (sec)	Method (L=log, S=sq rt)	Cv (ft²/day)	Average Effective Stress (tsf)	Height at EOP (inch)	Height at EOI (inch)	Void Ratio at EOP	Void Ratio at EOI	Strain at EOP (%)	Strain at EOI (%)	0 0
0.0320	0.0320	0.0320				,	0.7510	0.7510	2.3056	2.3056	00.0	00.00	
0.0320	0.0335	0.0340			•	0.025	0.7495	0.7490	2.2988	2.2966	0.21	0.27	-
0.0340	0.0351	0.0360	120	_	1.38E-01	0.063	0.7478	0.7469	2.2914	2.2876	0.43	0.55	
0.0367	0.0411	0.0442	228	_	7.21E-02	0.093	0.7425	0.7395	2.2682	2.2548	1.13	1.54	0.00205
0.0442	0.0465	0.0488	900	_	2.69E-02	0.135	0.7372	0.7349	2.2446	2.2345	1.84	2.15	
0.0490	0.0558	0.0591	900		2.64E-02	0.130	0.7281	0.7248	2.2046	2.1903		3.49	1
0.0589	0.0619	0.0653	480	_	3.23E-02	0.275	0.7218	0.7185	2.1771	2.1623		4.33	1
0.0655	0.0794	0.0860	840	_	1.79E-02	0.385	0.7046	0.6980	2.1011	2.0723	6.19	7.06	0.01025
0.0869	0.1125	0.1212	720	_	1.93E-02	0.550	0.6724	0.6637	1.9596	1.9213	10.47		0.01062
0.1218	0.1380	0.1471	480	_	2.65E-02	0.765	0.6475	0.6384	1.8498	_			0.00832
0.1461		0.1442	36	_	3.36E-01	0.655	0.6398	0.6403	1.8163	1.8183		14.74	-
0.1436	0.1414	0.1407	150	_	8.13E-02	0.330	0.6425	0.6433	1.8280	_			
0.1407	0.1340	0.1333	999	_	1.88E-02	0.165	0.6500	0.6507	1.8608				
0.1333	0.1330	0.1333				0.135	0.6510	0.6507	1.8652	_			-
0.1330	0.1340	0.1341				0.190	0.6497	0.6496	1.8595	1.8593	13.50	13.50	
0.1341	0.1344	0.1346				0.275	0.6493	0.6491	1.8577	1.8569			1
0.1349	0.1358	0.1365	9	_	2.08E-01	0.385	0.6481	0.6474	1.8527	1.8496		13.79	
0.1370	0.1408	0.1426	108	_	1.14E-01	0.550	0.6436	0.6418	1.8326	1.8249		14.54	0.00131
0.1430	0.1525	0.1576	270	_	4.46E-02	0.765	0.6323	0.6272	1.7829	_			0.00451
0.1577	0.1790	0.1828	1170	ب	9.63E-03	1.090	0.6058	0.6021	1.6665	1.6500		19.83	0.00626
0.1833	0.2070	0.2156	540		1.91E-02	1.525	0.5784	0.5698	1.5457	1.5080			0.01134
0.2162	0.2745	0.2817	540	_	1.60E-02	2.625	0.5115	0.5044	1.2514	1.2199			0.00903
0.2814	0.2744	0.2735	144	_	5.31E-02	2.410	0.5114	0.5123	1.2508	1.2549			1
0,2728	0.2654	0.2636	480	_	1.64E-02	0.985	0.5197	0.5215	1.2873	_			1
0.2626	0.2504	0.2497	1500	_	5.50E-03	0.495	0.5337	0.5344	_	_			1
0.2494	0.2448	0.2425				0.245	0.5389	0.5413		1.3826			1
0.2425	0,2326	0.2314				0.118	0.5512	0.5525	1.4261	1.4317	26.61	26.44	

0.118 0.5512 0.5525 1.4261 1.4317 26.61 26.44	EOP= End of Primary Consolidation	EOI= End of load increment (typically 24 hrs +/-)		Specific Gravity 2.7522) 2.0000) 62.57	0.2272	32.19
26.61	ary Cons	ncremen		c Gravity	neter (in	Ring weight (g)	olids (in	y Soil (g
1.4317	d of Prim	of load in		Specifi	Ring Diameter (in)	Ring	Height of Solids (in)	Neight of Dry Soil (g)
1.4261	:0P= Enc	:OI= End			_		Ĭ	Wei
0.5525								
0.5512	Fina	Conditions	0.5524	54.8	109.4	70.7	105.3	1.4314
0.118		m						
	Initial	Conditions	0.7510	85.3	96.3	52.0	101.8	2.3056
			Height (in)	Wc (%)	γt (pcf)	7d (pct)	Saturation (%)	Void ratio, e
0.2314		ayon	741		3.75)			
0.2326		Oyster Bayon	12-80-3741	B-15	12-14 (13.75)	•		
0.075 0.2425		mi	Ŀ	ber.				
0.075		Project Name	File Number:	Boring Number	Depth:			

ARDAMAN & ASSOCIATES, INC GEOTECHNICAL TESTING LABORATORY ONE-DIMENSIONAL INCREMENTAL LOADING CONSOLIDATION TEST SUMMARY SHEET

ſ						9				25	62	32					_		36	31	5	97	8	8					7
		Cae			Ι.	0.00205	l	1	1_			0.00832	1	1	1	1		1						0.00903	1	1		1	1
		Strain at EOI (%)	0.00	0.27	0.52	1.52	2.13	3.48	4.32	7.17					-	13.57													26.49
		Strain at EOP (%)	00.0	0.21		1.13					11.06	13.76		14.63	13.93	`													26.66
VIAIN		Void Ratio at EOI	2.3056	2.2966	2.2886	2.2553	2.2351	2.1904	2.1629	2.0685	1.9157	1.8042	1.8128	1.8244	1.8572	1.8570	1.8524	1.8499	1.8438	1.8194	1.7551	1.6351	_	1.2148	1.2498	<u> </u>	1.3508	_	1.4300
200		Void Ratio at EOP	2.3056	2.2988	2.2924	2.2683	2.2474			2.1070	1.9400	1.8506	1.8103	1.8220	1.8451	1.8570	1.8526	1.8508	_		_	1.6597	_	1.2903	_	_	1.3389	_	1.4245
		Height at EOI (inch)	0.7510	0.7490	0.7471	0.7396	0.7350	0.7248	0.7186	0.6971	0.6624	0.6371	0.6390	0.6417	0.6491	0.6491	0.6480	0.6475	0.6461	0.6405	0.6259	0.5987	0.5671	0.5032	0.5111	0.5204	0.5341	0.5410	0.5521
SOLIDA		Height at EOP (inch)	0.7510	0.7495	0.7480	0.7425	0.7378	0.7294	0.7219	0.7059	0.6679	0.6476	0.6385	0.6411	0.6464	0.6491	0.6481	0.6477	0.6467	0.6430	0.6318	0.6043	0.5809	0.5203	0.5100	0.5162	0.5314	0.5386	0.5508
500 S		Average Effective Stress (tsf)		0.025	0.063	0.093	0.135	0.190	0.275	0.385	0.550	0.765	0.655	0.330	0.165	0.135	0.190	0.275	0,385	0.550	0.765	1.090	1.525	2.625	2.410	0.985	0.495	0.245	0.118
-DIMENSIONAL INCREMENTAL LOADING CONSOLIDATION TEST SOMMANT STEE		Cv (ft²/day)			9.19E-02	6.69E-02	7.25E-02	4.56E-02	4.12E-02	2.55E-02	1.63E-02	2.91E-02	3,37E-01	4.30E-02	5.00E-02				1.32E-01	1.83E-01	5.66E-02	1.39E-02	3.21E-02	2.73E-02	5.33E-02	4.33E-02	8.34E-03	6.00E-03	3,19E-03
MENIA		Method (L=log, S=sq rt)			S	S	တ	တ	S	S	S	S	S	S	S				Ø	ဟ	S		S	v	S	S	S		S
INCRE		Time, t ₁₀₀ (sec)			778	1058	960	1500	1622	2535	3650	1881	154	1215	1058				406	290	913	3466	1382	1382	614	778	4234	6120	11929
SICINAL	ch)	EOI	0.0320	0.0340	0.0360	0.0442	0.0488	0.0591	0.0653	0.0860	0.1212	0.1471	0.1442	0.1407	0.1333	0.1333	0.1341	0.1346	0.1365	0.1426	0.1576	0.1828				0.2636	0.2497		
	eadings (inch)	EOP	0.0320	0.0335	0.0351	0.0412	0.0460	0.0545	0.0619	0.0772	0.1157	0.1365	0.1447	0.1412	0.1360	0.1333	0.1340	0.1344	0.1359	0.1401	0.1517	0.1772	0.2018	0.2645	0.2746	0.2677	0.2524	0.2448	0.2326
Ü O S C	Dial R	Initial	0.0320	0.0320	0.0342	0.0366	0.0442	0.0489	0.0290	0.0645	0.0865	0.1217	0.1461	0.1433	0.1407	0.1333	0.1330	0.1341	0.1351	0.1370	0.1430	0.1555	0.1840	0.2177	0.2814	0.2728	0.2634	0.2494	0.2424
		Effective Stress (tsf)	c	0.050	0.075	0.110	0.160	0.220	0.330	0.440	0.660	0.870	0.440	0.220	0.110	0.160	0.220	0.330	0.440	0.660	0.870	1.310	1.740	3.510	1,310	0,660	0.330	0.160	0.075

EOP= End of Primary Consolidation EOI= End of load increment (typically 24 hrs +/-)	Specific Gravity 2.7522	Ring Diameter (in) 2.0000	Ring weight (g) 62.57	Height of Solids (in) 0.2272	
Final Conditions	0.5480 54.8	110.2	71.2	106.7	1.4121
Initial Conditions	0.7510 85.3	96.3	52.0	101.8	2,3056
	Height (in)	yt (pcf)	yd (pct)	Saturation (%)	Void ratio, e
Oyster Bayou	12-80-3741 B-15	12-14 (13.75)			
Project Name:	File Number: Boring Number:	Depth:			



VERTICAL EFFECTIVE STRESS, $\sigma^{\iota}_{\,\,\nu c}$ (tsf)

BORING NO.:	B-16
SAMPLE NO.: DEPTH (FEET):	34.0
DESCRIPTION	Tan and gray CLAY (CH) w/silt layers
INDEX PROPERTIES	2969 1 40
LIQUID LIMIT (%):	67
PLASTIC LIMIT (%):	25
PLASTICITY INDEX (%):	42
SPECIFIC GRAVITY	2.76

SAMPLE DATA

-200(%):

SPECIMEN CONDITIONS	INITIAL	FINAL
MOISTURE CONTENT (%):	36.8	36.4
DRY DENSITY (lb/ft3):	84.2	87.2
VOID RATIO:	1.05	0.98

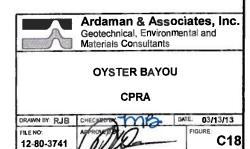
CONSOLIDATION PARAMETERS

EFFECTIVE OVERBURDEN STRESS, σ_{vo}^{\prime} (tsf):	0.81
PRECONSOLIDATION PRESSURE, o', (tsf):	6.2
VIRGIN COMPRESSION RATIO, CR:	0.174

INCREMENTAL CONSOLIDATION TEST RESULTS

100

Confidential Information: Privileged & Confidential Work Product



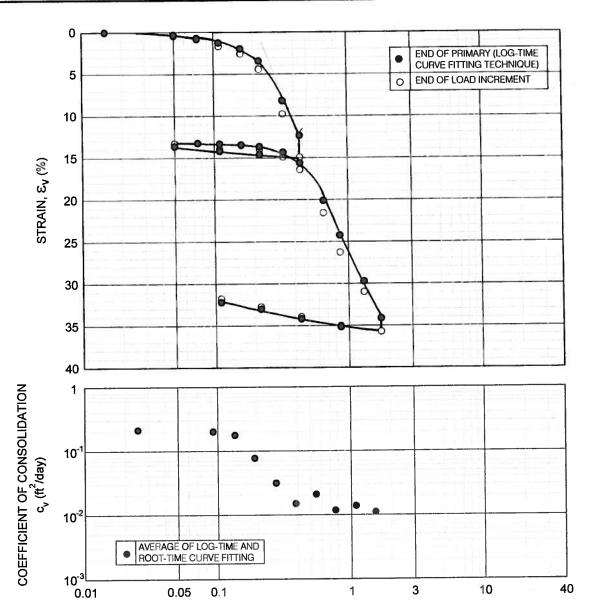
		C O	ľ	-	1		0.00090	29100.0	0.00220		2990.0						 			
		Strain at EOI (%)					_				•			3.46						
SY SHE		Strain at EOP (%)										<u> </u>		3.43					_	
MMAF		Void Ratio at EOI			`									0.9758						
ST SU		Void Ratio at EOP		1.0466	1.0436	1.0369	1.0225	0.9878			0.7523	0.8082		0.9765						
TION		Height at EOI (inch)		0.7500	0.7484	0.7457	0.7402	0.7269	0.7065	0.6795	0.6390	0.6627	0.6953	0.7241				 		11
SOLIDA		Height at EOP (inch)		0.7500	0.7489	0.7465	0.7412	0.7285	0.7082	0.6818	0.6422	0.6627	0.6935	0.7243			 			
NG CON		Average Effective Stress (tsf)			0.220	0.655	1.305	2.625	5.275	10.570	21.230	17.700	4.390	1.090						
ONE-DIMENSIONAL INCREMENTAL LOADING CONSOLIDATION TEST SUMMARY SHEEL		Cv (ft²/day)				1.38E-01	4.55E-02	6.06E-02	1.70E-02	1.19E-02	9.38E-03		3.25E-03	1.78E-03						
MENTA		Method (L=log, S=sq rt)				_			_1	_				_				 	-	
INCRE		Time,				120				_	•		4200							
SIONAL	ch)		Ē	0.0420	0.0436	0.0468	0.0541	0.0688	0.0920	0.1223			0.1082							
DIMEN	Dial Readings (inch)		EOP	0.0420	0.0431	0.0460	0.0531	0.0672	0000	0 1200	0.1635	0.1430	0 1100	0.0780)	-				
ONE	Dial R		Initial	0.0420	0.0420	0.00	0.0486	0.0555	0.0215	0.053	0.000	0.1667								
		Effective Stress		c	0 440	0.410	1 740	3.510	7 0.0	14 100	28.360	7.040	1 740	0.440						

EOP= End of Primary Consolidation EOI= End of load increment (typically 24 hrs +/-)				Height of Solids (in) 0.3665	Weight of Dry Soil (g) 52.07
Final Conditions	0.7243 36.4	118.9	87.2	102.9	0.9765
Initial Conditions	0.7500 36.8	115.1	84.2	6'96	1.0466
	Height (in) w _c (%)	yt (pal)	γ d (pct)	Saturation (%)	Void ratio. e
Oyster Bayou	12-80-3741 B-16	33-35 (34.0)	•		
Project Name:	File Number:	Depth:	-		

ONE-DIMENSIONAL INCREMENTAL LOADING CONSOLIDATION TEST SUMMARY SHEET

		Ουe			0.00090	0.00162	0.00226	0.00406	0.00552	1			
		Strain at EOI (%)	0.00	0.56	1.29	3.06		9.39				3.37	
		Strain at EOP (%)		0.15	1.07	2.48			•	_	7.63	3.79	e .
		Void Ratio at EOI	1.0466	1.0422		0.9840	0.9282	0.8545		0.8087	0.8982	0.9777	
		Void Ratio at EOP	ľ	1.0436	1.0248	0.9958	0.9488	0.8777	0.7737	0.8087	0.8905	0.9691	
		Height at EOI (inch)	0.7500	0.7484	0.7403	0.7271	0.7066	0.6796	0.6392	0.6628	0.6956	0.7248	
נו נו		Height at EOP (inch)	0.7500	0.7489	0.7420	0.7314	0.7142	0.6881	0.6500	0.6628	0.6928	0.7216	
		Average Effective Stress (tsf)	•	0.220	1.305	2.625	5.275	10.570	21.230	17.700	4.390	1.090	
		Cv (ft²/day)		70 197	6.36E-02	1.28E-01	4.80E-02	2.52E-02	1.63E-02		2.89E-03	2,33E-03	
		Method (L=log, S=sq rt)		ď	ာဟ	တ	တ	ဟ	S		ဟ	တ	
1		Time, t _{im} (sec)			1110		1380	2460	3465		20300	27478	
1771	ich)	EOI	0.0420	0.0436	0.0541	0.0688	0.0920	0.1223	0.1667	0.1430	0.1082	0.0783	
SINE-DIMENOISIA	Dial Readings (inch)	EOP	0.0420	0.0431	0.0524	0.0644	0.0844	0.1138	0.1558				
	Dial R	Initial	0.0420	0.0420	0.0486	0.0555	0.0715	0.0953	0.1262	0.1667	0.1410	0.1074	
	-1	Effective Stress (tsf)	0	0.440	1.740	3.510	7.040	14.100	28.360	7.040	1.740	0.440	

EOP= End of Primary Consolidation	EOI= End of load increment (typically 24 hrs +/-)			Ring Diameter (in) 2.0000	Ring weight (g) 62.62	_	Weight of Dry Soil (g) 52.07
Final	Conditions	0.7243	36.4	118.9	87.2	102.9	0.9765
Initial	Conditions	0.7500	36.8	115.1	84.2	6'96	1.0466
		Height (in)	Wc (%)		√d (pcf)	Saturation (%)	Void ratio, e
	Oyster Bayou	12-80-3741	B-16	33-35 (34.0)			
	Project Name:	File Number:	Boring Number:	Depth:			



B-17
3.75
Gray CLAY (CH)
w/trace silt
119
29
90
2.76

SPECIMEN CONDITIONS	INITIAL	FINAL
MOISTURE CONTENT (%):	130.4	79.5
DRY DENSITY (Ib/ft3)	37.3	54.6
VOID RATIO:	3.62	2.15

CONSOLIDATION PARAMETERS

EFFECTIVE OVERBURDEN STRESS, σ'vo (tsf):	0,062
PRECONSOLIDATION PRESSURE, o'p (Isf):	0.25
VIRGIN COMPRESSION RATIO, CR:	0.40
RECOMPRESSION RATIO, RR	0.035

INCREMENTAL CONSOLIDATION TEST RESULTS

Ardaman & Associates, Inc. Geotechnical, Environmental and Materials Consultants

OYSTER BAYOU

CPRA

DRAWN BY RJB

APPROPRIEST TOPS

DATE: 03/13/13

Confidential Information. Privileged & Confidential Work Product

-200(%)

12-80-3741

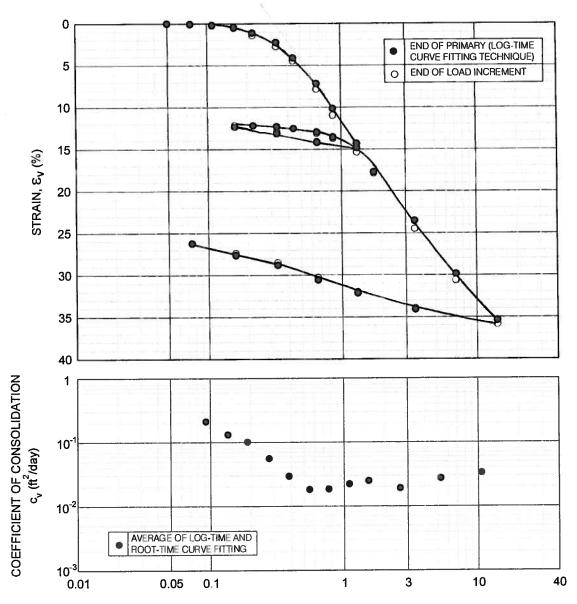
C19

•		 1			_	_	_											7	<u>ი</u>	က	2	က	_					
		CAE	1	1	1		0.00181	1	0.01183	1	1	1	1	•		1				_			0.01347	1		1	-	
F		Strain at EOI (%)	0.00	0.45	0.87	1.69	2.57	4.39	9.75	14.92	14.54	13.97	13.26	13.23	13.36	13.50	13.95	14.91	16.42	21.57	26.27	30.99	35.72	35.02	33.96	32.76	31.75	
YSHEE		Strain at EOP (%)	00.00	0.30 30	0.74	1.25	1.97	3.43	8.18	12.32	14.62	14.19	13.61	13.23	13.33	13.45	13.66	14.34	15.61			29.72	34.14	35.15	34.19	33.01	32.19	
MMAR		Void Ratio at EOI	i .			3.5381	3.4974			2.9273	2.9450			3.0056			2.9719			2.6204	2.4033	2.1854	1.9674	1.9995		2.1038	2.1502	
ST SU		Void Ratio at EOP	3.6161	3.6020	3.5818	3.5583	3.5253	3.4577	3,2385	3.0471	2.9411	2.9609	2.9878		3.0007	2.9953	2.9857	2.9542	2.8955	2.6886	2.4972	2.2444	2.0402	1.9937	2.0377	2.0925	2.1299	
TION T		Height at EOI (inch)	0.7550	0.7516	0.7485	0.7423	0.7356	0.7219	0.6814	0.6424	0.6453	0.6496	0.6549	0.6552	0.6541	0.6531	0.6497	0.6425	0.6310	0.5922	0.5567	0.5210	0.4854	0.4906	0.4986	0.5077	0.5153	
SOLIDA		Height at EOP (inch)	0.7550	0.7527	0.7494	0.7456	0.7402	0.7291	0.6933	0.6620	0.6446	0.6479	0.6523	0.6552	0.6544	0.6535	0.6519	0.6468	0.6372	0.6033	0.5720	0.5307	0.4973	0.4897	0.4969	0.5058	0.5119	
4G CON		Average Effective Stress (tsf)		0.025	0.063	0.093	0.135	0.190	0.275	0.385	0.330	0.165	0.080	0.063	0.093	0.135	0.190	0.275	0.385	0.550	0.765	1.090	1.525	1.305	0.655	0.330	0.165	
DIMENSIONAL INCREMENTAL LOADING CONSOLIDATION TEST SUMMARY SHEET		Cv (ft²/day)		2.81E-01		2.12E-01	1.81E-01	7.95E-02	2.60E-02	5.62E-03	2.05E-01	5.90E-02	6.98E-02			2.82E-01	2.10E-01	9.89E-02	5.78E-02	1.64E-02	8.81E-03	1.39E-02	9.49E-03	5.87E-02	2.19E-02	6.23E-03	ii	
MENTA		Method (L=log, S=sq rt)		_		_	_	_	_	_	_	٦				ر		_	_	_	_	_	_	_	_	_		
INCRE		Time, t ₁₀₀ (sec)		8	•	78	06	200	570	2381	9	210	180			45	9	126	210	069	1140	630	810	120	330	1200		
SIONAL	ch)	EOI	0.0502	0.0536	0.0568	0.0638	0.0704	0.0842	0.1249	0.1639	0.1608	0.1559	0.1506	0.1503	0.1512	0.1524	0.1559	0.1632	0.1748	0.2142	0.2499	0.2857	0.3213	0.3156	0.3075	0.2982	0.2906	
DIMEN	Dial Readings (inch)	EOP	0.0497	0.0525	0.0558	0.0605	0.0659	0.0769	0.1130	0.1443	0.1614	0.1576	0.1532	0.1503	0.1509	0.1520	0.1536	0.1589	0.1687	0.2030	0.2345	0.2760	0.3094	0.3165	0.3092	0.3000	0.2939	
ONE-I	Dial R	Initial	0.0490	0.0502	0.0536	0.0576	0.0638	0.0704	0.0844	0.1249	0.1637	0.1602	0.1559	0.1506	0.1502	0.1514	0.1525	0.1560	0.1634	0.1753	0.2144	0.2500	0.2857	0.3208	0.3155	0.3072	0.2982	
		Effective Stress (tsf)	0	0.050	0.075	0.110	0.160	0.220	0.330	0.440	0.220	0.110	0.050	0.075	0.110	0.160	0.220	0.330	0.440	0.660	0.870	1.310	1.740	0.870	0.440	0.220	0.110	

EOP= End of Primary Consolidation	EOI= End of load increment (typically 24 hrs +/-)		Specific Gravity 2.76	Ring Diameter (in) 2.0000	Ring weight (g) 62.60	Height of Solids (in) 0.1636	Weight of Dry Soil (g) 23.24
Final	Conditions	0.5159	79.5	98.0	54.6	101.8	2.1542
Initial	Conditions	0.7550	130.4	86.0	37.3	99.5	3.6161
		Height (in)	w _c (%)	7t (pcf)	λd (bct)	Saturation (%)	Void ratio, e
	Oyster Bayon	12-80-3741	B-17	2-4 (3.75)	•		
	Project Name:	File Number:	Boring Number:	Depth:	ò		

		Coe		1	1	0.00141	0.00181	1	0.01183	ı	1		1	Ť	1	1		0.00222	0.00479	0.01643	0.01625	0.01203	0.01347	1	1	ı	1	
<u>_</u>		Strain at EOI (%)	0.00	0.45	0.87	1.69	2.56	4.32	9.74	14.90	14.52	13.91	13.21	13.17	13.26	13.40	13.85	14.80	16.32	21.54	26.26	30.98	35.70	34.95	33.88	32.64	31.64	
Y SHEE		Strain at (EOP (%)	0.00	0.33	0.74	1.25	1.97	3.28	7.63	12.30	14.62	14.21	13.57	13.17	13.22	13.34	13.55	14.23	15,38	19.34				35.18			32.08	
MMAR		Void Ratio at EOI	3.6161	3.5953	3.5760	3.5381	3.4977	3.4167	3.1667	2,9282	2.9457	2.9738	3.0065	3.0080	3.0040	2.9976	2.9768	2.9328		2.6219		2.1860	1.9683		2.0521	2.1093	2.1557	
ST SU		Void Ratio at EOP	3.6161	3.6008	3.5818	3.5583	3.5253	3.4647	3.2639	3.0481	2.9411	2.9603	2.9897	3.0080	3.0056	3.0002	2,9906	2.9591	2.9059	2.7231	2.4862	2.2407	2,0411	1.9922	2.0341	2.0827	2.1354	
TION TE		Height at EOI (inch)	0.7550	0.7516	0.7485	0.7423	0.7357	0.7224	0.6815	0.6425	0.6454	0.6500	0.6553	0.6556	0.6549	0.6539	0.6505	0.6433	0.6318	0.5924	0.5568	0.5211	0.4855	0.4912	0.4992	0.5086	0.5162	
SOLIDA		Height at EOP (inch)	0.7550	0.7525	0.7494	0.7456	0.7402	0.7303	0.6974	0.6621	0.6446	0.6478	0.6526	0.6556	0.6552	0.6543	0.6527	0.6476	0,6389	0.6090	0.5702	0.5301	0.4974	0.4894	0.4963	0.5042	0.5128	
IG CON		Average Effective Stress (tsf)		0.025	0.063	0.093	0.135	0.190	0.275	0.385	0.330	0.165	0.080	0.063	0.093	0.135	0.190	0.275	0,385	0.550	0.765	1.090	1,525	1.305	0.655	0.330	0.165	
-DIMENSIONAL INCREMENTAL LOADING CONSOLIDATION TEST SUMMARY SHEET		Cv (ft²/day)		1.45E-01	1	1.90E-01	1.73E-01	7.51E-02	3.68E-02	2.42E-02	1.99E-01	9.88E-02	8.59E-02			3.16E-01	2.81E-01	1.85E-01	7,14E-02	2.52E-02	1.47E-02	1.36E-02	1.27E-02	1.05E-01	3.24E-02	1.84E-02	5.13E-03	
MENTA		Method (L=log, S=sq rt)		S		s	တ	S	S	S	ဟ	ဟ	ဟ			S	တ	S	S	ဟ	S	S	Ø	ဟ	S	S	တ	
INCRE		Time,		200		375	406	913	1750	2381	265	540	630			173	194	290	735	1949	2940	2774	2614	290	960	1750	6489	
SIONAL	일	EO	0.0502	0.0536	0.0568	0.0638	0.0704	0.0842	0.1249	0.1639	0.1608	0.1559	0.1506	0.1503	0.1512	0.1524	0.1559	0.1632	0.1748	0.2142	0.2499	0.2857	0.3213	0.3156	0.3075	0.2982	0.2906	
DIMEN	(eadings (inch)	EOP	0.0497	0.0527	0.0558	0.0605	0.0659	0.0763	0.1090	0.1443	0.1615	0.1581	0.1533	0.1503	0.1509	0.1520	0.1536	0.1589	0.1677	0.1976	0.2364	0.2767	0.3094	0.3173	0.3104	0.3025	0.2939	
ONE	Dial Re	Initial	0.0490	0.0502	0.0536	0.0576	0.0638	0.0709	0.0840	0.1249	0.1636	0.1605	0.1559	0.1506	0.1506	0.1514	0.1525	0.1560	0.1633	0.1748	0.2142	0.2500	0.2857	0.3212	0.3155	0.3075	0.2982	
		Effective Stress (tsf)	0	0.050	0.075	0.110	0.160	0.220	0.330	0.440	0.220	0.110	0.050	0.075	0.110	0.160	0.220	0.330	0.440	0.660	0.870	1.310	1.740	0.870	0.440	0.220	0.110	
		# o														-												

	24 hrs +/-)		"			10	
EOP= End of Primary Consolidation	EOI= End of load increment (typically		Specific Gravity 2.76	Ring Diameter (in) 2.0000	Ring weight (g) 62.60	Height of Solids (in) 0.1636	
Final	Conditions	0,5159	79.5	98.0	54.6	101.8	2.1542
Initial	Conditions	0.7550	130.4	86.0	37.3	99.5	3.6161
		Height (in)	(%) M	yt (pct)	yd (pct)	Saturation (%)	Void ratio e
	Ovster Bayou	12-80-3741	B-17	2-4 (3.75)	()		
	Project Name:	File Number	Boring Number	Depth:			



SAMPLE DATA	
BORING NO.:	B-19
SAMPLE NO.:	
DEPTH (FEET):	19.75
DESCRIPTION:	Gray CLAY (CH)

		40.5
INDEX PROPERTIES		
LIQUID LIMIT (%):	98	
PLASTIC LIMIT (%):	19	
PLASTICITY INDEX (%):	79	
SPECIFIC GRAVITY:	2.75	

SPECIMEN CONDITIONS	INITIAL	FINAL
MOISTURE CONTENT (%):	67.6	40.7
MOISTURE CONTENT (%): DRY DENSITY (lb/ft³):	60.5	81.9
VOID RATIO:	1.84	1.10

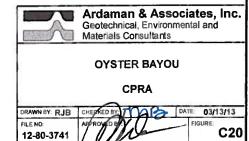
CONSOLIDATION PARAMETERS

EFFECTIVE OVERBURDEN STRESS, σ'_{vo} (tsf):	0.376
PRECONSOLIDATION PRESSURE, o', (tsf):	0.45
VIRGIN COMPRESSION RATIO, CR:	0.26
RECOMPRESSION RATIO, RR:	0.043

INCREMENTAL CONSOLIDATION TEST RESULTS

Confidential Information, Privileged & Confidential Work Product

-200(%):



ARDAMAN & ASSOCIATES, INC
GEOTECHNICAL TESTING LABORATORY
INCREMENTAL LOADING CONSOLIDATION TEST SLIMMARY SHEET

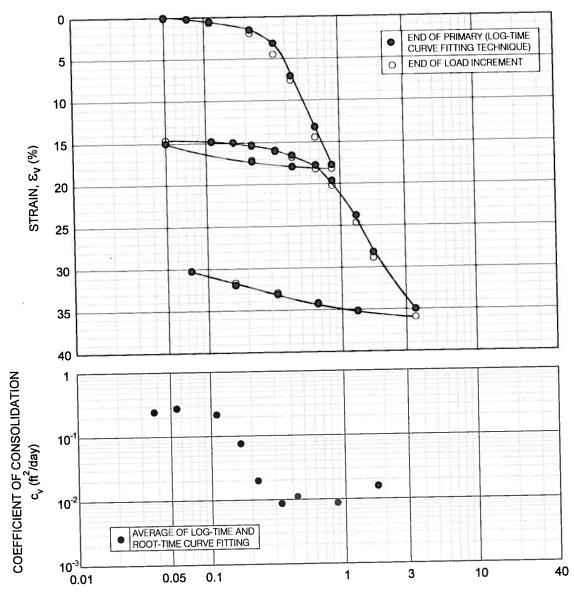
		Cae		1	1	0.00070	0.00192	0.00410		0.00811	0.00793	0.01025		1	1	1	1	1	0.00000	0.00124	0.00397	1	0.00816	0.00693	0.00433	-		i	1	1	1	
_		Strain at EOI (%)	0.00	0.07	0.25	0.54	1.41	2.75	4.47	7.84	10.97	14.73	14.08	12.90	12.15	12.19	12.35	12.55	13.10	13.71	15.37	17.86	24.44	30.64	35.86	33.97	31.99	30.25	28.49	27.39	26.21	1
Y SHE		Strain at EOP (%)	00.00	0.05	0.16	0.42	1.1	2.24	4.10	7.18	10.15	14.31	14.20	13.13	12.32	12.18	12.29	12.52	12.94	13.54	14.83	17.72	23.51	29.85	35.36	34.08	32.14	30,56	28.78	27.61	26.21	
MMAK		Void Ratio at EOI	1.8413	_	_	_	_	_	_	•	~	_	_	_	_	•	_	1.4848	-	-	_	_	•	_	0.8223	_	0.9324	0.9817	1.0319	1.0631	1.0967	
EST SL		Void Ratio at EOP	1.8413	_	1.8368	_	_	_	_	_	_	_	1.4377	_	_	<u> </u>	_	1.4856		_	1.4200	_	•	0.9930	0.8367	0.8728	0.9282	0.9731	Ψ-	1.0567	1.0967	
NO		Height at EOI (inch)	0.7540	0.7535	0.7521	0.7499	0.7434	0.7333	0.7203	0.6949	0.6713	0.6429	0.6478	0.6567	0.6624	0.6621	0.6609	0.6594	0.6552	0.6506	0.6381	0.6193	0.5697	0.5230	0.4836	0.4979	0.5128	0.5259	0.5392	0.5475	0.5564	
SOLIDA		Height at EOP (inch)	0.7540	0.7537	0.7528	0.7509	0.7456	0.7371	0.7231	0.6999	0.6775	0.6461	0.6469	0.6550	0.6611	0.6622	0.6613	0.6596	0.6564	0.6519	0.6422	0.6204	0.5767	0.5289	0.4874	0.4970	0.5117	0.5236	0.5370	0.5458	0.5564	
NG CON		Average Effective Stress (tsf)		0.038	0.093	0.135	0.190	0.275	0.385	0.550	0.765	1.090	0.985	0.495	0.245	0.190	0.275	0.385	0.550	0.765	1.090	1.525	2,625	5.275	10.570	8.805	2.410	0.985	0.495	0.245	0.118	
ONE-DIMENSIONAL INCREMENTAL LOADING CONSOLIDATION TEST SUMMARY SHEET		Cv (ft²/day)		•	1.75E-01	9.30E-02	8.63E-02	5.01E-02	2.02E-02	1.22E-02	1.29E-02	1.26E-02	1.14E-01	3.49E-02	1.79E-02		2.16E-01	3.59E-02	8.56E-02	7.04E-02	4.92E-02	9.78E-03	1.86E-02	2.13E-02	2.43E-02	5.40E-02	8.39E-03	4.42E-03	2.68E-03	į	•	
MENTA		(L=log, S=sq rt)			_	_	_	_	_	_	_	_	ب	_	_			_	_				_	ب	_		_	_	_			
INCRE		Time, t ₁₀₀ (sec)			96	180	192	324	780	1230	1080	1020	108	360	720		9	360	150	180	252	1200	570	420	312	132	006	1800	3120			
SIONAL	с 1)	EO .	0.1570	0.1575	0.1596	0.1620	0.1690	0.1796	0.1925	0.2180	0.2424	0.2702	0,2652	0,2563	0.2504	0.2507	0.2518	0.2537	0.2582	0.2629	0.2757	0.2946	0.3450	0.3929	0.4336	0.4181	0.4022	0.3883	0.3748	0.3663	0.3573	-
DIMENS	Dial Readings (inch)	EOP	0.1568	0.1574	0.1589	0.1611	0.1668	0.1758	0.1897	0.2130	0.2362	0.2670	0.2661	0.2580	0.2517	0.2506	0.2514	0.2535	0.2570	0.2616	0.2716	0.2935	0.3380	0.3870	0.4298	0.4190	0.4033	0.3906	0.3770	0.3680	0.3573	
ONE	Dial R	Initial	0.1565	0.1570	0.1582	0.1598	0.1625	0.1695	0.1795	0.1926	0.2188	0.2418	0.2701	0.2652	0,2561	0.2504	0.2506	0.2522	0.2540	0.2583	0.2632	0.2758	0.2954	0.3462	0.3942	0.4324	0.4171	0.4014	0.3881	0.3746	0,3662	
	1	Effective Stress (tsf)	٥	0.075	0.110	0.160	0.220	0.330	0.440	0.660	0.870	1.310	0.660	0.330	0.160	0.220	0.330	0.440	0.660	0.870	1.310	1.740	3.510	7.040	14.100	3.510	1,310	0.660	0.330	0.160	0.075	

EOP= End of Primary Consolidation EOI= End of load increment (typically 24 hrs +/-)		Specific Gravity 2.7522	Ring Diameter (in) 2.0000	Ring weight (g) 62.49	Height of Solids (in) 0.2654 Weight of Dry Soil (g) 37.60
Final	0.5565	40.7	115.3	81.9	102.0 1.0970
Initial Conditions	0.7540	9.79	101,4	60.5	1,8413
	Height (in)	Wc (%)	√t (pct)	yd (pct)	Saturation (%) Void ratio, e
Oyster Bayou	12-80-3741	B-19	18-20 (19.75)		
Project Name:	File Number:	Boring Number:	Depth:		

ARDAMAN & ASSOCIATES, INC GEOTECHNICAL TESTING LABORATORY ONE-DIMENSIONAL INCREMENTAL LOADING CONSOLIDATION TEST SUMMARY SHEET

ſ		Cae			1	0.00070	0.00192	0.00410		0.00811	0.00793	0.01025	-	1	1	1		1		0.00124	0.00397	1			0.00433			1	1	1		
_		Strain at EOI (%)	0.00	0.07	0.28	0.59	1.45	2.79	4.50	7.88	11.04	14.73	14.06	12.92	12.14	12.18	12.33	12.55	13.14	13.74	15.40										26.18	
Y SHE		Strain at EOP (%)	00.00	0.05	0.19	0.43	1.07	2.22	3.73	6.78	9.66	13.16	14.38	13.23	12.42	•															26.18	
MMAK		Void Ratio at EOI	1.8413		_	Ξ.	_	_	_	_	-	1.4228															0.9309	0.9825	1.0326	1.0639	1.0974	
באו אר		Void Ratio at EOP	1.8413	<u>-</u>	_	_	_	_	_		1.5668	1.4673	1.4326	1.4654	1.4884		_	_	1.4727	_	_	`_	1.1775		_	0.8498	0.9116	0.9701	1.0243	1.0575	· _	
Z O		Height at EOI (inch)	0.7540	0.7535	0.7519	0.7496	0.7431	0.7330	0.7201	0.6946	0.6708	0.6430	0.6480	0.6566	0.6625	0.6622	0.6611	0.6594	0.6549	0.6504	0.6379	0.6183	0.5688	0.5228	0.4832	0.4975	0.5124	0.5261	0.5394	0.5477	0.5566	
SOLIDA		Height at EOP (inch)	0.7540	0.7537	0.7526	0.7507	0.7460	0.7373	0.7259	0.7029	0.6812	0.6548	0.6456	0.6543	0.6604	0.6623	0.6614	0.6603	0.6562	0.6521	0.6431	0.6272	0.5779	0.5355	0.4950	0.4909	0.5073	0.5228	0.5372	0.5460	0.5566	
200		Average Effective Stress (tsf)		0.038	0.093	0.135	0.190	0.275	0.385	0.550	0.765	1.090	0.985	0.495	0.245	0.190	0.275	0.385	0.550	0.765	1,090	1,525	2.625	5.275	10.570	8.805	2.410	0.985	0,495	0.245	0.118	
ONE-DIMENSIONAL INCREMENTAL LOADING CONSOLIDATION LEST SUMMARY SHEE		Cv (ft²/day)			2.50E-01	1.72E-01	1.16E-01	6.02E-02	3.88E-02	2.47E-02	2.46E-02	3.20E-02	3.44E-01	3.61E-02	2.94E-02		1.28E-01	1.92E-01	9.20E-02	8.88E-02	6.16E-02	4.02E-02	1.98E-02	3.35E-02	4.25E-02	2.57E-01	2.06E-02	6.45E-03	•			
MENIA		Method (L=log, S=sq rt)			v	တ	S	S	တ	S	တ	တ	ဟ	s	တ		S	S	s	S	S	S	S	ဟ	ဟ	S	S	v				
NCKE		Time,			290	420	614	1162	1750	2614	2458	1750	15	1500	1882		437	290	900	614	866	1270	2306	1162	778	118	1561	5302				
SIONAL	ਓ	EOI	0.1570	0.1575	0.1596	0.1620	0.1690	0.1796	0.1925	0,2180	0.2424	0.2702	0.2652	0.2563	0.2504	0.2507	0.2518	0.2537	0.2582	0.2629	0.2757	0.2946	0.3450	0.3929	0,4336	0.4181	0.4022	0.3883	0.3748	0.3663	0.3573	
DIMEN	Dial Readings (inch)	EOP	0.1568	0.1574	0.1589	0.1608	0.1661	0.1753	0.1867	0.2097	0.2320	0.2584	0.2676	0.2586	0.2525	0,2506	0.2515	0.2528	0.2569	0.2612	0.2705	0.2857	0.3359	0.3802	0.4218	0.4247	0.4073	0.3916	0.3770	0.3680	0.3573	
ONE	Dial R	Initial	0.1565	0.1570	0.1580	0.1597	0.1625	0.1695	0.1796	0.1925	0.2186	0.2424	0.2702	0.2649	0.2563	0.2504	0.2507	0.2520	0.2538	0.2584	0.2632	0.2750	0.2955	0.3469	0.3940	0.4324	0.4171	0.4020	0.3881	0.3746	0.3662	
		Effective Stress (tsf)	٥	0.075	0.110	0.160	0.220	0.330	0.440	0.660	0.870	1.310	0.660	0.330	0.160	0.220	0.330	0.440	0.660	0.870	1.310	1.740	3.510	7.040	14.100	3.510	1.310	0.660	0.330	0.160	0.075	

EOP= End of Primary Consolidation EOI= End of load increment (typically 24 hrs +/-)	Specific Gravity 2.7522			Height of Solids (in) 0.2654 Weight of Dry Soil (g) 37.60
Final Conditions	0.5565	115.3	81.9	102.0 1.0970
Initial	0,7540 67.6	101.4	60.5	101.1 1.8413
	Height (in) w _c (%)	yt (pct)	/d (pct)	Saturation (%) Void ratio, e
Oyster Bayon	12-80-3741 B-19	18-20 (19.75)	•	
Project Name	File Number: Boring Number:	Depth:		



SAMPLE DATA	
BORING NO.:	B-05
SAMPLE NO .:	
DEPTH (FEET):	5,5
DESCRIPTION:	Gray CLAY (CH)
INDEX PROPERTIES	
LIQUID LIMIT (%):	87
PLASTIC LIMIT (%):	22
PLASTICITY INDEX (%):	65
SPECIFIC GRAVITY:	2.72
-200(%):	95
ORGANIC CONTENT (%):	6.6

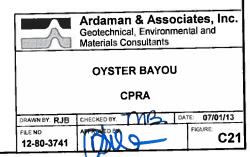
SPECIMEN CONDITIONS	INITIAL	FINAL
MOISTURE CONTENT (%):	86.5	49.4
DRY DENSITY (lb/ft³):	51.3	73.8
VOID RATIO:	2.31	1.30

CONSOLIDATION PARAMETERS

EFFECTIVE OVERBURDEN STRESS, σ'vo (tsf):	0.09
PRECONSOLIDATION PRESSURE, σ'p (tsf):	0.31
VIRGIN COMPRESSION RATIO, CR:	0.36
RECOMPRESSION RATIO, RR:	0.035

INCREMENTAL CONSOLIDATION TEST RESULTS

Confidential Information: Privileged & Confidential Work Product



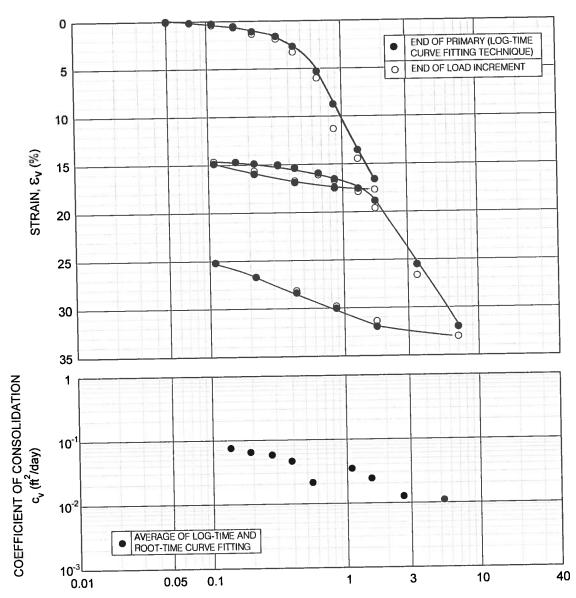
		C D e		1		-				0.01070	1	1	1	-	1	1	1		0.00168	0.00333	0.00590	0.01449		0.00993	1	-			1		
		Strain at EOI (%)	0.00	0.11	0.22	99.0	1.97	4.48	7.58	14.42	18.20	17.86	17.10	·	_					18.23	3 20.21		9 28.85	35.95	1 35.12	34.16	32.92		2 30.22		;
Y SHE		Strain at EOP (%)	0.00	0.00	0.17	0.50	1.54	3.17	7.07	13.20	17.74	17.93	17.26		•					_				35.00		34.30			7 30.22		
MMAR		Void Ratio at EOI	2.3114	2.3078	2.3039	2.2894	2.2461	2.1629	2.0604	1.8337							_						_								
ST SU		Void Ratio at EOP	2,3114	23114	2 3057	2.2948	2 2604	2.2064	2.0772					- `		•	•														
NOI TE		Height at EOI (inch)	0.7500	0 7492	0.7483	0.7450	0.7352	0 7164	0.6932	0.6418	0.6135	0.00	0.00	0.0210	0.040	0.6304			0.0290												
OLIDAT	3	Height at EOP (inch)	0.7500	0.7500	0.7.00	0.7463	0.7385	0.7.06.0	0.6970	0.6510	0.00	0.00	0.0133	0.6200								0.0020						_			
G CONS		Average Effective Stress (tsf)		, 0	0.020	0000	0.00	0.00	0 0	0.220	0.00	0.450	0.220	0.110	0.025	0.055	0.080	0.110	0.165	0.220	0.330	0.435							0.000	200	
ONE-DIMENSIONAL INCREMENTAL LOADING CONSOLIDATION TEST SUMMARY SHEET		Cv (ft²/day)		1		2.4/E-U1	1.84E-01	1.30E-01.	6.60E-02	1.12E-02	8.59E-U3	6.52E-03	1.87E-01	6.30E-02	1.45E-02	1.44E-01	1.12E-01	6.67E-02	4.70E-02	5.26E-02	5.01E-02	2.03E-02	1.60E-02	7.16E-03	1.29E-02	5.37E-02	1.48E-02	6.12E-03	4.68E-03		
IENTAI		Method (L=log, S=sq rt)	1	,	,	· ω		٠.	 	<u>.</u>	٠ ـ	_		_	_	_		_1	_	_				_	_						
NCREN		Time, t ₁₀₀ (sec)				290	06	120	240	1320	1560	1800	9	180	810	8	108	180	252	222	228	240	636	1260	009	129			8669		
IONAL I	£	EOI		0.0618	0.0626	0.0636	0.0677	0.0781	0.0972	0.1203	0.1719	0.2004	0.1972	0.1910	0.4720	0.1740	0.1753	0.1783	0.1837	0.1891	0.2001	0,2150	0.2487	0.2802	0.3357	0.3281	0.3203	_		0,2896	
DIMENS	Dial Readings (inch)	EOP		0.0618	0.0618	0.0632	0.0665	0.0748	0.0873	0.1165	0.1627	0.1970	0.1977	0.1922	0.1747	0.1735	0.1747	0.1774	0.1827	0.1871	0.1965	0.2107	0.2420	0.2752	0.3285	0.3287	0.3214	0.3118	0.3031	0.2896	
ONE-E	Dial Re	Initial		0.0618	0.0618	0.0627	0.0644	0.0683	0.0783	0.0971	0.1206	0.1721	0.1998	0.1967	0.1903	0.1724	0.1741	0.1755	0.1786	0.1838	0.1893	0.2002	0,2153	0.2488	0.2824	0.3343	0.3276	0.3198	0.3102	0.3005	
		Effective Stress (tsf)		0	0.050	0.075	0.110	0.220	0.330	0.440	099'0	0.870	0.440	0.220	0 0 0	0.110	0 160	0.220	0.330	0.440	0,660	0.870	1.310	1.740	3.510	1,310	0.660	0.330	0,160	0.075	

EOP= End of Primary Consolidation EOI= End of load increment (typically 24 hrs +/-)	Specific Gravity 2.7195 Ring Diameter (in) 2.0000 Ring weight (g) 62.57	Weight of Dry Soil (g) 31.71
Final Conditions	0,5210 49.4 110,3 73.8	103.3 1.3003
Initial	0,7500 86.5 95.6 51.3	101.8
	Height (in) w _c (%) γ1 (pcf) γ4 (pcf)	Saturation (%) Void ratio, e
I Over a section of	12-80-3741 12-80-3741 B-05 4-6 (5.5)	-200 = 95 OC = 6.6
	Project Name: File Number: Boring Number: Depth:	LL = 87 PI = 65

ARDAMAN & ASSOCIATES, INC GEOTECHNICAL TESTING LABORATORY NSIONAL INCREMENTAL LOADING CONSOLIDATION TEST SUMMARY SHEET

_							0 0	<u>, , , , , , , , , , , , , , , , , , , </u>	, ,	_					_			_	0 0	2 6	0	2 9	2 6	_	_				_	7
		O O	-	1	1				0.00942			1	1		1	1		1		0.00333					1					
		Strain at EOI (%)	0.00	0.11	0.22	0.66	2.01	4. t	7.07	4. 6	18.28	17.83	71.71	0/4/	14.92	15.08	15.47	16.15	16.84			24.30							30.22	
		Strain at EOP (%)	0.00	0.0	0.17	44.0	1.36	3.08	9, 9	13.30	16.76	18.02	17.50	15.52	14.80	14.98	15.30	15.88	16.52										30.22	
l	_	Void Ratio at EOI	2.3114	2.3078	2,3039	2.2894	2.2448	2.1609	2.0589	1.8320	1.7061	1.7176		`_	`_	·	_	_		<u>`</u> _		` .	`		`_			_	1,3107	
		Void Ratio at EOP	2.3114	2.3114	2.3057	2,2969	2.2664	2.2090	2.1039	1.8690	1.7565	Τ.	_	1,7975	1.8211	_		1.7854	1.7642		_	`	_	_	Τ.		_	`	1.3107	
		Height at EOI (inch)	0.7500	0.7492	0.7483	0.7450	0.7349	0.7159	0.6928	0.6414	0.6129	0.6155	0.6212	0.6397	0.6381	0.6369	0.6340	0.6289	0.6237	0.6130	0.5982	0.5657	0.5342		0.4867		0.5032	0.5125	0.5234	
		Height at EOP (inch)	0.7500	0.7500	0.7487	0.7467	0.7398	0.7268	0.7030	0.6498	0.6243	0.6148	0.6187	0.6336	0.6390	0.6377	0.6353	0.6309	0.6261	0.6171	0.6061				0.4848		0.5001	0.5103	0.5234	
	-	Average Effective Stress (tsf)	ā	0.025	0.063	0.093	0.165	0.275	0.385	0.550	0.765	0.655	0.330	0.135	0.080	0.135	0.190	0.275	0.385	0.550	0.765	1.090	1.525	2.625	2.410	0.985	0.495	0.245	0.118	
-DIMENSIONAL INCREMENTAL FORDING		Cv (ft²/day)			2.47E-01	3.68E-01	2.93E-01	8.76E-02	2.79E-02	8.53E-03	1.56E-02	2.22E-01	1.20E-01	2.33E-02	3.39E-01	2.68E-01	1.02E-01	8 31E-02	7.24E-02	6.31E-02	5.19E-02	8.88E-02	1.02E-02	1.85E-02	8.59E-02	2.75E-02	1.07E-02	4.68E-03		
		Method (L=log, S=sq rt)	1		· ·	o or	, v	S	S	S	v	S	S	S	· v	ص د	S	v.	o v	o vo	S					ဟ	_			
		Time, t ₁₀₀ (sec)			290	194	240	778	2306	6742	3286	217	406	2160	154	8	505	614	894	778	913	505	3840	1815	346	1109	2940	6998		
	(ر	EOI	0.0040	0.00.0	0.0020	0.0000	0.007	0.0972	0.1203	0.1717	0 2004	0 1972	0 1910	0.1720	0 1740	0.1753	0.1783	0 4 8 2 7	2000	0 1999	0.2150	0.2479	0.2802	0.3357	0.3281	0.3203	0 3105	03000	0.2806	0.505.0
DIMENO	Readings (inch)	EOP	0,000	0.00	0.00	0.0032	0.0000	0.0863	0 1101	0 1633	1800	0 1070	0.1935	24787	0.170	0 1745	0 1770	7 7 7	0.00	0.1000	0.2071	0 2265	0 2704	0.3242	00880	0.3229				
ONE-I	Dial Re	Initial	0,00	0.0618	0.0010	0.0027	0.0044	0.0000	0.000	1203	01710	0 0 0 0	0.1330	0.190	0.1905	0.1744	0 1754	0.17.04	0.1786	0.1838	0.002	0.2154	0.2487	0.2420	0.2020	0.3343	0.70	0.5180	0.3102	0.3005
		Effective Stress (tsf)		0.000	0.050	0.00	0.110	0.220	0.330	0.440	0.000	0.00	0.44.0	0.220	0.050	0.10	0.100	0.220	0.330	0.440	0.820	1 310	1 740	3 540	0.00	0.5.0	0000	0.330	0.160	0.075

EOP= End of Primary Consolidation EOI= End of load increment (typically 24 hrs +/-)		Height of Solids (in) 0.2265 Weight of Dry Soil (g) 31.71
Final	0,5210 49.4 110.3 73.8	103.3 1.3003
Initial Conditions	0.7500 86.5 95.6 51.3	101.8
	Height (in) w _c (%) yt (pcf)	Saturation (%) Void ratio, e
Oveter Bayou	12-80-3741 B-05 4-6 (5.5)	-200 = 95 OC = 6.6
Desired Name	Fige Number: Boring Number: Depth:	LL = 87



SAM	1PL	E DA	IA

BORING NO.: SAMPLE NO.: B-13

2.72

DEPTH (FEET): DESCRIPTION:

9.75 Gray CLAY (CH)

INDEX PROPERTIES

LIQUID LIMIT (%):
PLASTIC LIMIT (%):
PLASTICITY INDEX (%):
SPECIFIC GRAVITY:
-200(%):
ORGANIC CONTENT (%):

CONS

CONSOLIDATION PARAMETERS

SPECIMEN CONDITIONS

MOISTURE CONTENT (%):

DRY DENSITY (lb/ft3):

VOID RATIO:

INCREMENTAL CONSOLIDATION TEST RESULTS

Confidential Information: Privileged & Confidential Work Product



INITIAL

64.7

616

1.75

Ardaman & Associates, Inc. Geotechnical, Environmental and Materials Consultants

OYSTER BAYOU

FINAL

41,5

81.3

1.09

CPRA

FILE NO: 12-80-3741

DATE: 07/01/13

APPROVIDEY C

GEOTECHNICAL TESTING LABORATORY

GEOTECHNICAL TESTING LABORATORY

GEOTECHNICAL TESTING LABORATORY

GEOTECHNICAL TESTING LABORATION TEST SUMMARY SHEET

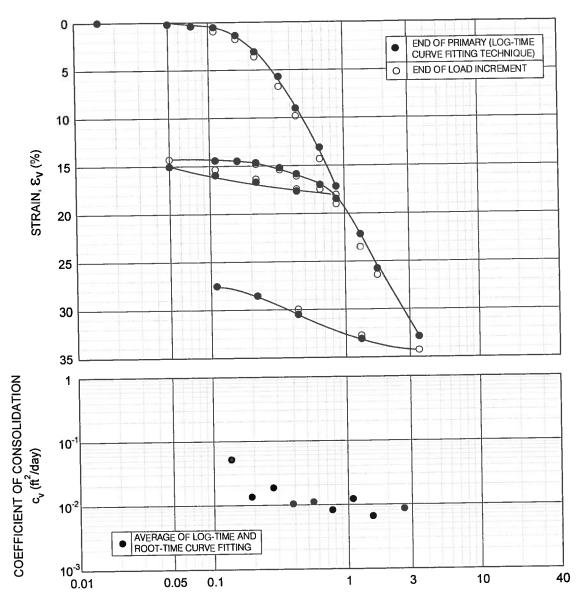
			_	_	_		_																												
_		Strain at C ne EOI (%)	00:00	0.09	0.14	0.40	0.68	1.35	1.88	3.28	00'9	11.31	14.45																					53.10	:
SHEE		Strain at EOP (%)	0.00	0.00	0.15	0.25	0.54	1.09	1.60	2.68	5.31	8.73	13.52	16.58	17 48	88 91	, o. o.	20.0																25.18	
MMAR		Void Ratio at EOI	1.7527	1.7504	17489	1.7418	1,7341	1,7157	1,7009	1,6626	1.5875	1 4415	•						1.0497				_ '	1.3030			•						`	7 1.0597	
STSU		Void Ratio at EOP	1.7527	1.7527	1 7487	1 7460	1 7378	1 7228	1 7086	1 6790	1 6067	_	•	•	- •			•				_								_	_	_	•	1.0597	
ION TE		Height at EOI (inch)	0.7540	0.7534	0.7530	0.7510	0.7489	07430	0.7398	0 7293	0.7088	0.6888	0.0000	0.00	0.0203	0.6229	0.6280	0.6361	0.6436	0.6433	0.6419	0.6401					_							0.5642	
SOLIDAT		Height at EOP (inch)	0.7540	0.7540	0.75.0	0.7522	0.7400	0.7450	0.7430	0.74.0	0.730	00000			_				_												0.5276	5 0.5401		5 0.5642	
NG CON		Average Effective Stress (tsf)		200	0.023	0.000	20.00	0.130	0.190	0.27.0	0.00	0.00	0.765	1.090	1.525	1.305				0.135					_				5.275	4.390	1,305	3 0.655	0.330	0.165	
ONE-DIMENSIONAL INCREMENTAL LOADING CONSOLIDATION TEST SUMMARY SHEE!		Cv (ft²/day)		e			L	7.49E-02	6.43E-02	3.035-02	4.625-02	2.14E-02	3.216-01	3.43E-02	2.40E-02	1.78E-01	4.71E-02	2.13E-02	9.83E-03			8.55E-02	4.29E-02	4.44E-02	4.00E-02	4.49E-02	3.98E-02	1.26E-02	1.10E-02	4.25E-02	6.57E-03	2.97E-03			
MENTA		Method (L=log, S=sq rt)	T				n (so I	ທ .	، ر	so (n	S	S	S	ဟ		S						w											
NCREN		Time,					217	096	1109	540	1500	3110	194	1622	2160	277	1058	2381	5302			614	1215	1162	1270	1109	1215	3466			ч,	-			
IONAL I	h)	EOI		0.0726	0.0733	0.0739	0.0769	0.0794	0.0848	0.0892	0.1002	0.1230	0.1675	0.1957	0.2229	0.2206	0.2146	0.2063	0.1984	0.1989	0.2005	0.2030	0.2057	0.2112	0.2163	0.2261	0.2413				(0				_
DIMENS	Dial Readings (inch)	EOP		0.0726	0.0726	0.0739	0.0757	0.0784	0.0828	0.0871	0.0957	0.1177	0.1481	0.1887	0.2148	0.2212	0.2158	0.2087	0.2000	0.1989	0.2005	0 2022	0.2049	0,2099	0,2150	0.2234	0.2355	0.2894							_
ONE-I	Dial Re	Initial		0.0726	0.0726	0.0735	0.0749	0.0773	0.0797	0.0851	0.0897	0.1024	0.1275	0.1720	0.1987	0.2225	0 2197	0.2143	0.2059	0.1986	0.1991	0 2012	0.2033	0.2061											
		Effective Stress (tsf)		0.000	0.050	0.075	0.110	0.160	0.220	0,330	0.440	0.660	0.870	1.310	1.740	0.870	0.840	0.220	0.110	0.160	0.220	0 330	0.440	0.660	0.870	1.310	1 740	3 510	1 0	7.040	1,40	0,870	0.440	0.220	0.110

EOP= End of Primary Consolidation EOI= End of load increment (typically 24 hrs +/-)	Specific Gravity 2.7182 Ring Diameter (in) 2.0000 Ring weight (g) 62.53	Weight of Dry Soil (g) 38.33
Final	0.5720 41.5 115.0 81.3	103.7
Initial	0.7540 64.7 101.5 61.6	1.7527
	Height (in) w _c (%) 74 (pcf) 74 (pcf)	Saturation (%) Void ratio, e
Oveter Bayou	12-80-3741 B-13 8-10 (9.75)	-200 = 97.2 OC = N/A
A de cinado	Project Name: File Number: Boring Number: Depth:	LL = N/A PI = N/A

ARDAMAN & ASSOCIATES, INC GEOTECHNICAL TESTING LABORATORY CPEMENTAL I OADING CONSOLIDATION TEST SUMMARY SHEET

				_	
 | | | | |
 | | | | |
 | | | | |
 | | | | |
 | | | | |
 | | |
|-------------|---|--|---|--|--
--	--	--	--
--	--	--	--
--	---	--	--
---	---	--	--
--	---	--	---
---	--	--	--
	at C ne	00:	60
 | .35 | .93 | 28 | .01 | .23
 | .37 | .58 | .33 | 65 |
 | | - 64 | 1 83 | 5.05 | 5 34
 | 9,00 | 6.61 | 7.81 | 9.52 | 6.52
 | 2.90 | 1.26 | 99.68 | 8.03 | 6.58
 | 5.07 | |
| | Strain (9) | L | | | | _
 | | | | | ·
 | | | | | | |
 | | | | |
 | | | | |
 | | | | |
 | | |
| | Strain a
EOP (% | 0.0 | 0.0 | 0. | |
 | | | | | _
 | | Ċ | | |
 | | | | |
 | | | | |
 | | | | |
 | | 1 |
| _ | Void
Ratio at
EOI | 1.7527 | 1.7504 | 1.7487 | 1 7414 | 1 7338
 | 1 7155 | • | | | •
 | | | | | | |
 | _ ` | | | |
 | | | • | • |
 | | | | |
 | | |
| | Void
Ratio at
EOP | 1.7527 | 1.7527 | 1 7487 | |
 | | | | |
 | | | | |
 | | | | |
 | | | | | •
 | | | | |
 | | Ŀ |
| | Height at
EOI
(inch) | 0.7540 | 0.7534 | 0.7529 | 0.7509 | 0.7488
 | 0.7438 | 0.7305 | 7203 | 0.7087 | 000
 | 0.0034 | 0.045 | 0.6213 | 0.0234 | 0.0283
 | 0.6365 | | | 0.6422 |
 | | | | |
 | _ | | | |
 | | |
| | Height at EOP (inch) | 0.7540 | 0.7540 | 0.75.20 | 0.7534 | 0.720
 | 0.7450 | 0.7437 | 0.7414 | 0.7330 | 0.7 140
 | 0.6881 | _ | | |
 | | | | | _
 | | | | |
 | | | | |
 | | |
| | Average
Effective
Stress
(tsf) | | 100 | 0.00 | 20.00 | 2000
 | 0.133 | 0.190 | 0.2/3 | 0.385 | 0.000
 | 0.765 | 1.090 | 1.525 | 1.305 | 0.655
 | 0.330 | 0.165 | 0.135 | 0.190 | 0.275
 | | | | |
 | | | _ | |
 | 0.33 | 0.10 |
| | Cv
(ft²/day) | | 1 | | L | 3.33E-01
 | 7.49E-02 | 6.43E-02 | 8.5/E-02 | 4.61E-02 | 2.14E-02
 | 3.21E-01 | 3.44E-02 | 2.40E-02 | 1.78E-01 | 4.72E-02
 | 2.14E-02 | 9.84E-03 | | | 8.56E-02
 | 4.30E-02 | 4.45E-02 | 4.01E-02 | 4.50E-02 | 3.99E-02
 | 1.26E-02 | 1.11E-02 | 4.27E-02 | 6.60E-03 | 2.98E-03
 | | |
| | Method
(L≃log,
S=sq rt) | 1 | . (| ח | s o | S
 | တ | S | s
S | s · | S
 | S | S | S | |
 | | | ω | ဟ |
 | | | | |
 | | | | _ |
 | σ · | s |
| | | | • | | | 217
 | 960 | 1109 | 821 | 1500 | 3110
 | 194 | 1622 | 2160 | 277 | 1058
 | 2381 | 5302 | | | 614
 | 1215 | 1162 | 1270 | <u> </u> |
 | | | | | _
 | | |
| h) | EOI | | 0.0726 | 0.0733 | 0.0739 | 0.0769
 | 0.0794 | 0.0847 | 0.0892 | 0.0999 | 0.1230
 | 0.1668 | 0.1957 | 0.2229 | 0.2206 | 0.2146
 | 0.2063 | 0.1984 | 0.1989 | 0.2005 | 0.2028
 | 0.2055 | 0.2111 | 0.2163 | |
 | | | | |
 | | 0.2854 |
| adings (inc | EOP | | 0.0726 | 0.0726 | 0.0739 | 0.0757
 | 0.0784 | 0.0828 | 0.0872 | 0.0957 | 0.1177
 | 0.1481 | 0.1887 | 0.2148 | 0.2212 | 0.2158
 | 0.2087 | 0.2000 | 0.1989 | 0,2005 | 0.2022
 | 0.2049 | 0.2099 | 0.2150 | 0.2234 | 0,2355
 | | | _ | | 0
 | | 0.2854 |
| Dial Re | Initial | | 0.0726 | 0.0726 | 0.0735 | 0.0749
 | 0.0773 | 0.0797 | 0.0849 | 7680.0 | 0.1024
 | 0.1275 | 0.1720 | 0.1987 | 0.2225 | 0.2197
 | 0.2143 | 0.2059 | 0.1986 | 0.1991 |
 | | | 0.2117 | 0.2171 | 0.2284
 | | | | |
 | | 0.2968 |
| | Effective
Stress
(tsf) | | 0.000 | 0.050 | 0.075 | 0.110
 | 0.160 | 0.220 | 0.330 | 0.440 | 0.660
 | 0.870 | 1.310 | 1.740 | 0.870 | 0 440
 | 0.220 | 0.110 | 0.160 | 0.220 | 0.330
 | 0.440 | 0.660 | 0.870 | 1,310 | 1.740
 | 3,510 | 7.040 | 1.740 | 0.870 | 0.440
 | 0.220 | 0.110 |
| | | Dial Readings (inch) Time, Method Cv Effective EOP EOI to (sec) Time, Columbda Col | Dial Readings (inch) Time. Method Time. Method Cv Effective EOP EO From (1=log.) Stress (inch) (inch) EOP EO From (1=log.) Stress (inch) (inch) EOP EO EO (%) | Dial Readings (inch) Time, Method Cv Effective EOP EOI Retion at Retion at EOP EOI Retion at EOI Retion at EOP EOI Retion at EOP EOI Retion at EOP EOI Retion at EOP EOI Retion at EOP EOI Retion at EOI R | Dial Readings (inch) Height at Height at Height at Height at Height at Height at Height at Height at Height at Strain at Strai | Dial Readings (inch) Height at Height at Height at Height at Height at Height at Height at Height at Height at Height at Height at Strain at
Strain at Strai | Dial Readings (inch) Time, Method Cv Effective EOP Ratio at Ratio at EOP Ratio at EOP Ratio at EOP EOI Ratio at EOP EOI Ratio at EOP EOI Ratio at EOP EOI Ratio at EOP EOI Ratio at EOP EOI Ratio at EOP EOI Ratio at EOP Ratio at EOP EOI Ratio at EOP Ratio at EOP EOI Ratio at EOP EOI EOI Ratio at EOP EOI E | Dial Readings (inch) Time, Method Cv Effective EOP Ratio at Ratio at EOP Ratio at EOP EO Ratio at EOP EO Ratio at EOP EO Ratio at EOP EO Ratio at EOP EO Ratio at EOP EO Ratio at EOP EO Ratio at EOP EOI Ratio at EOP EOI Ratio at EOP EOI Ratio at EOP Ratio at EOP EOI Ratio at EOP EOI Ratio at EOP EOI | Dial Readings (inch) Time, Method Cv Effective EOP Ratio at Ratio at EOP EO Ratio at EOP EO Ratio at EOP EO Ratio at EOP EO Ratio at EOP EO (%) E | Time, Method Cv Effective EOP Ratio at Ratio at Ratio at Cop FOI Ratio at Ratio at EOP FOI Ratio at EOP FOI Ratio at EOP FOI Ratio at EOP FOI FOI EOP EOP EOP EOP EOP EOP EOP EOP FOI EOP EO | Dial Readings (inch) Time, Method Cv Effective EOP Folial at Height at Void Void Strain at Strain at EOP Folial at EOP EO (inch) EOP
EO (inch) EOP EO (inch) EO (inch) EOP EO (inch) EO (inch) EOP EO (inch) EO (inch) EOP EO (inch) EO (inch) EOP EO (inch) EO | Dial Readings (inch) Time, Method Cv Effective EOP Height at Height at Height at Cop EO Ratio at EOP EO EO Ratio at EOP EO | Dial Readings (inch) Time, Method Cv Effective EOP Height at Height at Cop EO Ratio at EOP EO EO Ratio at EOP EO EO Ratio at EOP EO EO EO Ratio at EOP EO | Time EOP EO Friedrings (inch) Time Time Method Cv Effective EOP Ratio at Ratio at EOP Ratio at EOP Ratio at EOP EO Ratio at EOP EO Ratio at EOP EO Ratio at EOP EO Ratio at EOP EO Ratio at EOP EO Ratio at EOP EO Ratio at EOP EO Ratio at EOP Ratio at EOP EO Ratio at EOP EOI Ratio at EOP Ratio at EOP Ratio at EOP Ratio at EOP EOI Ratio at EOP Ratio at EOP EOI Ratio at EOP EOI Ratio at EOP EOI Ratio at EOP EOI Ratio at EOP EOI EOI Ratio at EOP EOI EOI Ratio at EOP EOI Ratio at EOP EOI EOI EOI Ratio at EOP EOI | Dial Readings (Inch) Time, Method Cv Effective EOP Ratio at Ratio at EOP Ratio at EOP Ratio at EOP EO Ratio at EOP EO Ratio at EOP EO Ratio at EOP EO Ratio at EOP EO Ratio at EOP EO Ratio at EOP EO Ratio at EOP EOI Ratio at EOP Ratio at EOP Ratio at EOP Ratio at EOP EOI EOI Ratio at EOP EOI EOI Ratio at EOP EOI E | Dial Readings (Inch) Time, Method Cv Effective EOP Ratio at Ratio at Ratio at EOP FOI Ratio at EOP FOI Ratio at EOP FOI Ratio at EOP FOI Ratio at EOP FOI Ratio at EOP FOI Ratio at EOP FOI Ratio at EOP FOI Ratio at EOP FOI Ratio at EOP FOI EOP FOI EOP FOI EOP FOI EOP FOI EOP FOI EOP FOI EOP FOI EOP FOI EOP FOI EOP FOI EOP FOI EOP FOI EOP FOI EOP FOI EOP FOI EOP FOI EOP
 EOP E | Diel Readings (inct) Time, Method Cv Effective EOP EOI Ratio at Ratio at Ratio at Ratio at Ratio at Roll EOP EOI Ratio at Ratio at Ratio at Roll EOP EOI Ratio at Ratio at Roll EOP EOI Ratio at Ratio at Roll EOP EOI EOI EOI (inch) (inch) EOP EOI | Dial Readings (inch) Time, Method Cv Effective EOP Feight at Height at Height at Height at Height at Void Ratio at EOP Fe OI Ratio at EOP Fe OI Ratio at EOP Fe OI Ratio at EOP Fe OI Ratio at EOP Fe OI Ratio at EOP Fe OI Ratio at EOP Fe OI Ratio at EOP Fe OI Ratio at EOP Fe OI Ratio at EOP Fe OI Fe OI EOP Fe OI Fe OI EOI Fe OI EOI Fe OI EOI Fe OI EO | Dial Readings (inch) Time, Method Cv Effective EOP EO Ratio at Ratio at EOP EO Ratio at EOP EO Ratio at EOP EO Ratio at EOP EO Ratio at EOP EO Ratio at EOP EO EOP (%) EO (%) EO (%) EOP EO EOP EO EOP EO EOP EO EOP EO EOP (%) EOP EO EOP EOP EOP EO EOP EOP EOP EOP EOP EOP EOP EOP EOP EOP EOP EOP EOP | Diel Readings (inch) Time Method Cv Effective EOP Fleght at Height at He | Dial Readings (inch) Time, Method Cv Effective EOP
EOP E | Diel Readings (inch) Time, Method Cv Effective EOP EOI Ratio at Ratio at Ratio at Ratio EOP EOI Ratio at Ratio EOP EOI Ratio at Ratio EOP EOI Ratio at Ratio EOP EOI Ratio at Ratio EOP EOI Ratio EOP EOI Ratio EOP EOI Ratio EOP EOI Ratio EOP EOI Ratio EOP EOI Ratio EOP EOI | Dial Readings (Inch) Time, Method Cv Effective EOP EO Ratio at Ratio at EOP EO Region at Ratio at EOP EO Ratio at EOP EO Ratio at EOP EO Ratio at EOP EO Ratio at EOP EO Ratio at EOP EO Ratio at EOP EO Ratio at EOP EO Ratio at EOP EO Ratio at EOP EO Ratio at EOP EO Ratio at EOP EO Ratio at EOP EO Ratio at EOP EO Ratio at EOP EO Ratio at EOP EO EO Ratio at EOP EO EO Ratio at EOP EO EO Ratio at EOP EO EO Ratio at EOP EO | Dial Readings (Inch) Dial Readings (Inch) Dial Readings (Inch) Cv Effective EOP EO | Dial Readings (Inch) Dial Readings (Inch) Cv Effective ECD ECD ECD ECD ECD (Inch) ECD ECD ECD (Inch) ECD ECD ECD (Inch) ECD (Inch) ECD (Inch) ECD (Inch) ECD ECD (Inch) ECD (In | Dial Readings (inch) Time, Method Cv Effective EOP EOI Ratio at Ratio
at Ratio at Rati | Dial Readings (inch) Time, wethod Cv Effective EOP EOI Ratio at Ratio | Time Cov Effective Cov Effective EOp | Digit Readfly Strain of Line Time, Method Cv Effective EOp EOl Foot Chical | Diel Readings (inch) Trume, (ii_elog) Trume, | Diel Readings (inch) Trime, (L=log) Heritod CV Effective EOP EO EO Ratio at Ratio at Ratio at Ratio at Ratio at Ratio at Ratio at Ratio at Ratio at Ratio at Ratio at Ratio at Ratio at Ratio at Ratio at EOP (%) EO (%)
EO (%) EO (% | Dist Residings (inch) Time | Dist Resolvings (inch) Time Cov Filestive EOP EOI Ratio at Ra |

EOP= End of Primary Consolidation EOI= End of load increment (typically 24 hrs +/-) Specific Gravity 2.7182 Ring Diameter (in) 2.0000 Ring weight (g) 62.53 Height of Solids (in) 0.2739 Weight of Dry Soil (g) 38.33
Final Conditions 0.5720 41.5 115.0 81.3 103.7 1.0883
Initial Conditions 0.7540 64.7 101.5 61.6 100.4
Height (in) w _c (%) 7t (pcf) 7d (pcf) Saturation (%) Void ratio, e
Oyster Bayou 12-80-3741 B-13 8-10 (9.75) -200 = 97.2 OC = N/A
Project Name: File Number: Boring Number: Depth: LL = N/A Pl = N/A



SPECIMEN CONDITIONS

VIRGIN COMPRESSION RATIO, CR: RECOMPRESSION RATIO, RR:

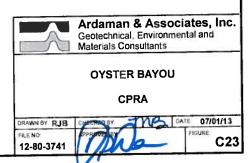
SAMPLE DATA	
BORING NO.:	B-09
SAMPLE NO.:	44.75
DEPTH (FEET):	11,75
DESCRIPTION:	Gray CLAY (CH) w/silt
INDEX PROPERTIES	
LIQUID LIMIT (%):	99
PLASTIC LIMIT (%):	27
PLASTICITY INDEX (%):	72
SPECIFIC GRAVITY	2.78
-200(%):	99

MOISTURE CONTENT (%): DRY DENSITY (lb/tt ³): VOID RATIO:	93.0 48.5 2.58	58.5 66.9 1.59
CONSOLIDATION PARAMETE	ERS	
EFFECTIVE OVERBURDEN STRE	SS, o'vo (tsf):	0.19
PRECONSOLIDATION PRESSURI	E, σ', (tsf):	0.29

INITIAL

INCREMENTAL CONSOLIDATION TEST RESULTS

Confidential Information: Privileged & Confidential Work Product



0.03

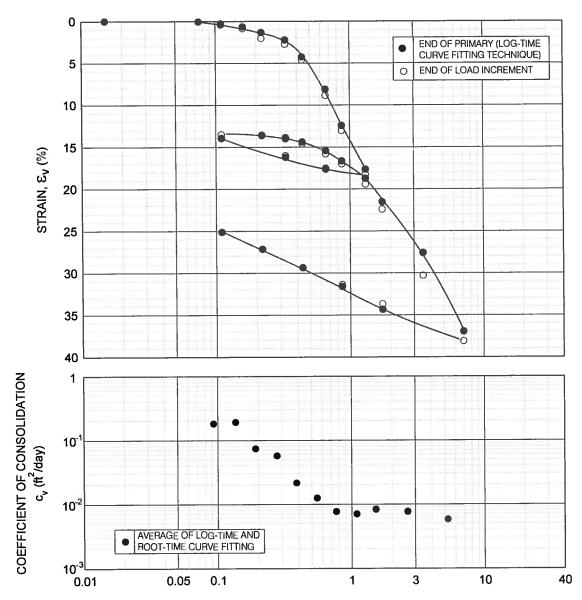
FINAL

ARDAMAN & ASSOCIATES, INC GEOTECHNICAL TESTING LABORATORY INCREMENTAL I OADING CONSOLIDATION TEST SUMMARY SHEET

		Cne	ı	ı	ı	1	1	1	I	1						1	ı	1	1	1	1	1	1	1	1	1	1	1				1	1	١	1	
		Strain at EOI (%)	00.0	-0.01	0 19	0.40	760	1.78				•					_		_	_	`	15.41		17.47	19.01	23.52							1 27.51			
ו משבנו		Strain at EOP (%)	00.0	000	0	0.0	0.50	1.38												14.45	14.65	15.21		16.99							30.50					
MINIAR		Void Ratio at EOI	25818	2 5821	25750	2.37.30	2 5 4 0 4	25181				2.2303								2.0621	2.0509	2.0299		1.9559	Ľ						_	1.5597	1.5966			
21 20		Void Ratio at EOP	2 5818	2 0 0	2.00.0	2.5750	4.0074	2.3032	2,743	2.47.13	20/02	2.2593	2.1121	1.9666						2.0642										_	_	1.5597	_			
NO.		Height at EOI (inch)	0.7590	0 0	0.730	0.7556	0.730	0.7509	0.7440	0.7300	0.707	0.6836							0.6488	0.6480											0.5308	0.5417				
SOLIDA		Height at EOP (inch)	0 1500	0.7.00	0.7380	0.7566	0.7550	0.7541	0.7470	0.7346	0.7149	0.6898	0.6586	0.6278	0.6243	0.6316	0.6372	0.6440	0.6488	0.6485	0.6469	0.6427						_		0.5073	0.5268	0.5417				
SCONS		Average Effective Stress (tsf)		,	0.008	0.033	0.063	0.093	0.13	0.190	0.275	0.385	0.550	0.765	0.655	0.330	0.165	0.080	0.080	0.135	0.190	0.275	0.285							2.410	0.875	0330	0.000	·-		
ONE-DIMENSIONAL INCREMENTAL LOADING CONSOLIDATION IEST SUMMARY SHEET		CV (ft²/day)		,				1.10E+00	6.77E-02	1.32E-02	1,83E-02	1.04E-02	1.11E-02	8.18E-03	1.05E-01	4.15E-02	5.37E-02	6.78E-02		2 49E.01	2.4351-0	3.005-02	3.140-02	2.425-02	3.70=02	1.50E-02	1.20E-02	6.54E-03	8,57E-03	2.54E-02	7.06E-03	!				
MENTA		Method (L=log, S=sq rt)						s	S	v	S	S	S	ဟ	S	S	S	S)	U		_	ם מ							_				_		
NCREN		Time,						99	1058	5302	3650	0009	5189	6365	470	1215	096	778	-	15.4	\$0.00 0.00	8001	1685	0912	1382	3286	3840	6365	4234	1270						
IONAL	F)	EO		0.0463	0.0462	0.0476	0.0492	0.0535	0.0599	0.0738	0.0976	0.1211	0.1552	0.1835	0.1786	0.1705	0.1627	0.1545	0.1557	0.100	0.1565	0.1590	0.1640	0.1692	0.1800	0.1918	0.2260	0.2480	0.3096	0.2970	0.2759			0,2567		
SNEWS	Dial Readings (inch)	EOP		0.0463	0.0463	0.0476	0.0492	0,0503	0.0568	0.0698	0.0897	0.1149	0.1461	0.1769	0 1802	1727	0.1671	1601	0 4 6 6	0.1337	0.1560	0.1577	0.1624	0.1675	0.1763	0.1877	0.2156	0.2429	0.2988	0 2006	0.2700	0.2733	0.2649	0.2567		
ONE-E	Dial Re	Initial		0.0463	0.0463	0.0461	0.0476	0.0494	0.0535	0.0599	0.0740	92600	0 1211	0.1552	0 1832	0.1284	720	40.104	0.1023	0.1540	0.1557	0.1566	0.1595	0.1641	0.1694	0.1801	0.1918	0.2260	0 2500	7805.0	9000			0.2645		
		Effective Stress (tsf)		000.0	0.015	0.050	0.075	0.110	0.160	0.220	0.330	0 440	0.860	0.870	0.000	0.00	0.220	0.0	0.020	0.110	0.160	0.220	0.330	0.440	099'0	0.870	1.310	1.740	3.510		0 2 2	0.440	0.220	0.110		

EOP≂ End of Primary Consolidation EOI= End of load increment (typically 24 hrs +/-)	Specific Gravity 2.78118	King Diameter (iii) 2.000	Congression (9) 0.2116	weight of Dry Spil (a) 30.30	
Final					
Initial Conditions	0.7580 93.0	93.6	48.5	100.2	2.5818
	Height (in) w _c (%)	yt (pct)	yd (pal)	Saturation (%)	Void ratio, e
Oyster Bayou	12-80-3741 B-09	10-12 (11.75)		-200 = 99,4	OC = NA
Project Name:	File Number: Bodna Number:	Depth;	0	1.L = 99	PI = 72

Г		61																																
		O O	1		1			1		1	1				١	1	1			1	1	1		9	1	1	1	6	9	9	1	1	1	
		Strain at EOI (%)	0.00	-0.01	0.18	0.35	0.89	1.64	3.48	6.59	69.6	•					•		14.42	14.65	15.23		17.30	18.85	23.37	26.27	34,12							
JUL I		Strain at EOP (%)	0.00	0.00	0.18	0.35	0.47	1.33	2.95	5.55	8.87	12.99	17.05	17,53	16.56	15.84	14.94	14.31	14.35	14.56	15.03	15.68	16.82	18.31	21.99						27.43			
MINIAR		Void Ratio at EOI	2.5818	2.5821	2.5755	2.5693	2.5499	2.5230	2.4573	2.3458	2.2348	2.0736	1.9359	1.9616			2:0732	2.0691	2.0654	2.0570		2.0122	1.9621		1.7449			,	- *	•				
		Void Ratio at EOP	2.5818	2.5818	2.5755	2.5693	2.5651	2.5344	2,4762	2.3831	2.2641	2.1166	1.9711	1.9541	1.9886	2.0146	2.0467	2.0691	2.0677						•				•					
NO		Height at EOI (inch)	0.7580	0.7581	0.7567	0.7554	0.7513	0.7456	0.7317	0.7081	0.6846	0.6505	0.6222	0.6268	0.6347	0.6424	0.6504	0.6495	0.6487	0.6469	0.6425	0.6374	0.6268	0.6151	0.5809	0.5589	0.4993	200			0.5423	0.000		
OLIDA		Height at EOP (inch)	0.7580	0.7580	0.7567	0.7554	0.7545	0.7480	0.7357	0.7160	0.6908	0.6596	0.6288	0.6252	0.6325	0.6380	0.6448	0.6495	0.6492	0.6476	0.0440	0.6391	0.6305	0.6192	0 5913	0.5540	2000	0.00	0.5064	0.5278	0.5423	L066.0		
G CONS		Average Ffective Stress (tsf)	1	800	0000	0.00	200.0	0.135	0.190	0.275	0.385	0.550	0,765	0.655	0.330	0.165	0.080	080	0 135	2 6	0.130	285	0.00	0.000	1000	2000	25.0			0.875	0.330	0.165		
ONE-DIMENSIONAL INCREMENTAL LOADING CONSOLIDATION TEST SUMMARY SHEET		Cv (ft²/day)					1 105 100	3.55F-02	1.32E-02	1 83E-02	1.04E-02	1.11E-02	8.20E-03	1.06E-01	4 16E-02	5.38E-02	6 79F-02		2 40E 04	3.43E-01	5.07 = 0.2	3. 10E-02	2.435-02	3.7 10-02	1.015-02	7.212.0	6.57 E-03	8.61E-03	2.55E-02	7.08E-03				
ENTAL		Method (L=log, S=sq π)	1				ď	n u	o or	· ·	S	· v	S	v.	· v	y c	ď	•		n c	n c	ם מ	n c	ח נו		n c								
NCREI		Time,	1				0	20.48	5302	3650	0009	5189	6365	470	1215	090	778		, 2,	40	1058	1685	2000	1382	3280	3840	6365	4234	1270	4860		_		
ONAL	(2)	EOI	00,00	0.0463	0.0462	0.0476	0.0489	0.0030	20000	9700.0	0.121	0 1552	0.1835	0.1786	0.1705	0.1607	7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	. O	0.1330	0,1565	0.1584	0.1639	0.1692	0.1800	0.1918	0.2260	0.2480	0.3096	0.2971	0.2761	0,2651	0.2567		
IMENS	Dial Readings (inch)	EOP		0.0463	0.0463	0.0476	0.0489	0.0503	0.000	0.0000	0.0037	2464	0.1769	2 0	0.1002	0.1727		0.1001	0.1330	0.1560	0.1577	0.1624	0.1675	0.1763	0.1877	0.2156	0.2429	0.2988	0.2996	0.2799	0.2651	0.2567		
ONE-L	Dial Rea	Initial		0.0463	0.0463	0.0462	0.0476	0.0494	0.0535	0.0399	0.0740	0.0970	0.15.0	0.00	0.1032	0.1784	0.1704	0.1625	0.1548	0.1557	0.1566	0.1595	0.1641	0.1694	0.1801	0.1918	0.2260	0.2500	0.3087	0.2968	0.2758	0.2645	8	
		Effective Stress (tsf)		0.000	0.015	0.050	0.075	0.110	0.160	0.220	0.330	0.440	0.000	0.070	0.440	0.220	0.1.0	0.050	0.110	0.160	0.220	0.330	0.440	0.660	0.870	1.310	1,740	3.510	1.310	0.440	0.220	0.110	0.000	



VERTICAL EFFECTIVE STRESS, σ'_{vc} (tsf)

SAMPLE DATA	
BORING NO.:	B-14
SAMPLE NO.:	
DEPTH (FEET):	5.75
DESCRIPTION:	Gray CLAY (CH)
INDEX PROPERTIES	
LIQUID LIMIT (%):	107
PLASTIC LIMIT (%):	27
PLASTICITY INDEX (%):	80
SPECIFIC GRAVITY:	2.71
-200(%):	99
ORGANIC CONTENT (%):	5.4

SPECIMEN CONDITIONS	INITIAL	<u>FINAL</u>
MOISTURE CONTENT (%):	92.2	61.5
DRY DENSITY (lb/ft3):	48.6	66.0
VOID RATIO:	2.47	1.56

CONSOLIDATION PARAMETERS

0.09
0.41
0.36
0.045

INCREMENTAL CONSOLIDATION TEST RESULTS

Confidential Information Privileged & Confidential Work Product

	Ardaman & Ass Geotechnical, Environmentals Consultant	nmental and
	OYSTER BAYO	ou
	CPRA	
DRAWNBY: RJB	CHECKED AY	DATE 07/01/13
FILE NO. 12-80-3741	1770Ve	FIGURE C24

ARDAMAN & ASSOCIATES, INC GEOTECHNICAL TESTING LABORATORY CDEMAENTAL LOADING CONSOLIDATION TEST SUMMARY SHEET

Average Height at Height at Effective EOP EOI Stress (inch) (inch)	Method Cv (L=log, (ff²/day)	Time, Meth		
Stress (tsf)			lime	-
			Š	EOI to
0.7500		1	1	0 0700
0 008 0.7500				0.0762
				0.0741
				0.00
1.63E-01 0.093 0.7480	1.63	102	,-	0.080.0
7.86E-02 0.135 0.7451	7.86	210	• • •	0.0836
0.190	L 5.44	300		0.0929
0,275	P 9.66	240	- 4	0.0982
0.385	L 1,29	1200	-	0.1128
0.550	1.08	1350	-	0.1392 0.1447
0.765	L 6.53	2040	Ñ	0.1720 0.1766
1.090	L 6.43	1860	_	
0.985	L 3.74	300		
0.495				0.1998 0.1984
0.220			ω	0.1826 0.1793
0.220			-	0.1802 0.1807
0.275	5.56	096		_
0.385		1750	—	0.1865 0.1882
0.550	_	2018	O	0.1944 0.1973
		2693	·V	0.2064
000.	_	3025	.,	
1.525	8.2	5530		
2.023		2302	••	
3.273		5415	-,	
4.390	_	2774	• •	0.3477 0.3429
	_	11426	÷	0.3269 0.3253
	_			0.3097 0.3097
				0.2929 0.2929
0.165 0.5617	.,-			2776 0.2776

EOP= End of Primary Consolid	EOI= End of load increment (ly Specific Gravity Ring Diameter (in)	Ring weight (g)	Height of Solids (In) Weight of Dry Soil (g)
Final	Conditions 0.5520 61.5 106.6	0.99	106.8 1.5572
Initial	Conditions 0.7500 92.2	48.6	100.8
	Height (in) We (%)	7d (pct)	Saturation (%) Void ratio, e
	Oyster Bayou 12-80-3741 B-14	4-6 (5.75)	-200 = 99 OC = 5.4
	Project Name: File Number: Boring Number:	Depth:	LL = 107 PI = 80

2.705 2.0000 62.57 0.2159 30.06

ARDAMAN & ASSOCIATES, INC GEOTECHNICAL TESTING LABORATORY INCREMENTAL LOADING CONSOLIDATION TEST SUMMARY SHEET

	O O e	ı	1			-	F	1	 I	1	0.000		0.01190	0.01200	1	1		1	ı	ı	l				. 1		1	ı	1	1	I	1	
	Strain at EOI (%)	0.00	-0.28	2 4	3 6	90.0	0.49	0.93	2.12	<u> </u>				0.40 0.10	17.67	7.0.4	20.00	2 00	2 7	14.77	10.37	10.55	22.50	20.42	20.72	2 6	33.82	31.50	29.47	27.27	25.29		
	Strain at St EOP (%) E0	0.00	0	3 6	0.00	90.0	0.32	0.65	1.32	2.37	3.91	7.77	12.28	17.47	17.92	16.57	14.09	13.73	20.41	4.74	00.0	70.01	10.00	27.73	27.73	D. / C	34.46	31.71	29.47	27.27	25.29		
	Void S Ratio at E	2 4745	2 40 40	2.4042	2.4/63	2.4717	2.4573	2.4421	2.4008	2.3777	2.3110	2.1641	2.0163	•			٠	•	•			•						_	_	1.5269	1.5959		
	Void Ratio at EOP	2 4745	2 1 1 0	2.4/45	2.4763	2.4717	2.4634	2.4518	2.4286	2.3920			•••	•	_	٠.	•	_	_	_	_		•			•	_	1.3726	1.4504	1.5269	1.5959		
	Height at EOI (inch)	0.7500	200	0.7521	0.7504	0.7494	0.7463	0.7430	0.7341	0.7291	0.7147	0.6830	0.6511	0.6116	0.6175	0.6287	0.6476						_					0.5138	0.5290	0.5455			
	Height at EOP (inch)	0 7500	0.7300	0.7500	0.7504	0.7494	0.7476	0.7451	0.7401	0.7322	0.7207	0.6917	0.6579	0.6190	0.6156	0.6257	0.6443	0.6470	0.6448	0.6410	0.6332	0.6239	0.6084	0.5875	0.5421	0.4719	0.4916	0.5122	0.5290	0.5455			
	Average Effective Stress (tsf)	1	•	0.008	0.033	0.063	0.093	0.135	0.190	0.275	0.385	0.550	0.765	1.090	0.985	0.495	0.220	0.220	0.275	0.385	0.550	0.765	1.090	1.525	2.625	5.275	4.390	1.305	0.655	0.330	0 165		
-	Cv (ft²/day)	1					1.91E-01	2.96E-01	9.02E-02	4.57E-02	2.91E-02	1.36E-02	8.51E-03	7.36E-03	6.54E-02	1.89E-02	7.97E-03	5.05E-02	5.54E-02	3.01E-02	2.56E-02	1.86E-02	1.59E-02	8.18E-03	7.59E-03	5.82E-03	1.05E-02	2 84E-03					
	Method (L=log, S=sq rt)	1	•				v.	· v	· v	S	S	S	S	v	S	S	s	S	s	s	S	S		S	တ								
	Time,				-		375	240	778	1500	2306	4646	6742	6998	735	2614	6490	1058	960	1750	2018	2693	3025	5530	5302	5415		•	-				
Ð	EOI		0.0762	0.0741	0.0758	0.0769	0000	0.000	00000	0.0982	0.1128	0 1445	0.1766	0 2161	0.2099	0.1984	0.1793	0.1807	0.1838	0.1882	0.1973	0.2064	0.2245	0.2471	0.3071	0.3676	0 3429	0.0753	0.000	0.5097	0.2829	0.2778	
Dial Readings (inch)	EOP		0.0762	0.0762	0.0758	0.00	0.0	0.0709	2 00 0	0.000	0.000	0 1358	0 1698	0.2087	0.218	0 2014	0.1826	0.1802	0 1826	0.1865	0 1944	0.2038	0.2195	0.2406	0.2869	0.3590	0.3477	2000	0.3203	0.3097	0.2929	0.2779	
Dial Re	Initial		0.0762	0.0762	0.0741	0.07	0.0739	0.00	0.0000	0.0040	0.0932	0.00	0.1447	0.4766	0.1700	2006	1082	0.1796	1809	1839	0.1883	0 1974	0 2066	0.2247	0.2480	0 3000	0.3030	0.57.00	0.3427	0.3249	0.3094	0.2928	
	Effective Stress (tsf)		0.000	0.015	0 0	0.000	0.075	0.110	0.190	0.220	0.330	0.440	0.000	7	0.5.0	0.000	0.55	0.1.0	0.330	0.330	0.440	0.870	1310	1 740	3 5 10	0.00	145	1.740	0.8/0	0.440	0.220	0.110	

EOI= End of load increment (typically 24 hrs +/-)	Specific Gravity 2.705 Ring Diameter (in) 2.0000 Ring weight (g) 62.57	Weight of Dry Soil (g) 30.06
Conditions	0,5520 61.5 106.6 66.0	106.8 1.5572
Conditions	0.7500 92.2 93.4 48.6	100.8
	Height (in) W _e (%) yt (pcf) yd (pcf)	Saturation (%) Void ratio, e
Greeter Ravou	12-80-3741 12-80-3741 18-14 4-6 (5.75)	-200 = 99 OC = 5.4
	Figet, Name: File Number: Boring Number: Depth:	LL= 107 PI= 80

APPENDIX D. UNCONSOLIDATED UNDRAINED TRIAXIAL COMPRESSION TEST RESULTS

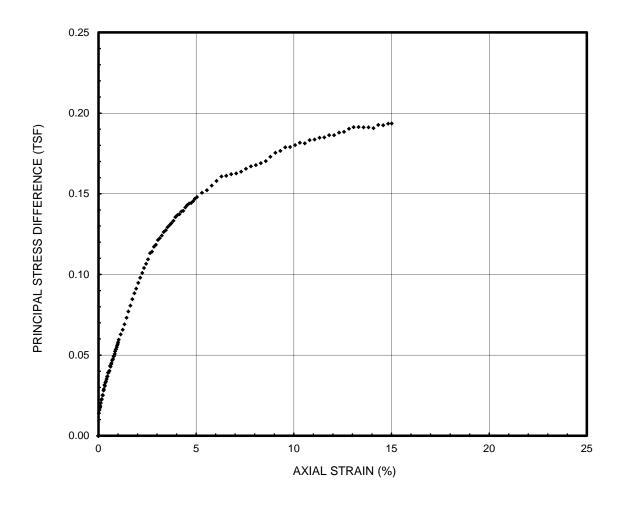
This Appendix contains the following:

• Unconsolidated Undrained Compressive Strength – Stress Strain Curve

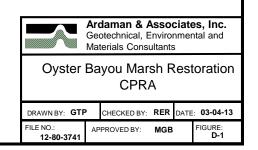


Ardaman & Associates, Inc.

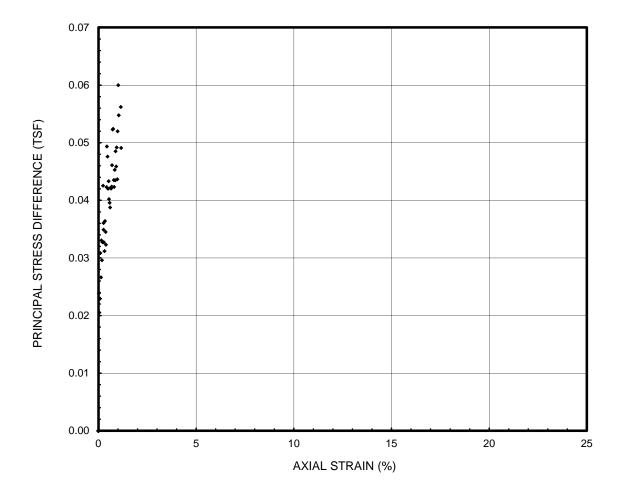
Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-01
Depth 0-2 ft



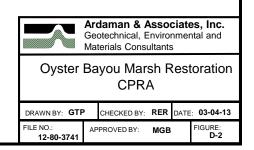
Initial Height	5.810	in	Cell Pressure	1.00	lb/in ²
Initial Diameter	2.810	in	Strain Rate	1.0	%/min
Dry Density	49.3	lb/ft ³	Peak Stress	0.194	ton/ft ²
Water Content	89.7	%	Strain at Peak Stress	15.01	%
Saturation	101	%	Failure Type	Bulging	



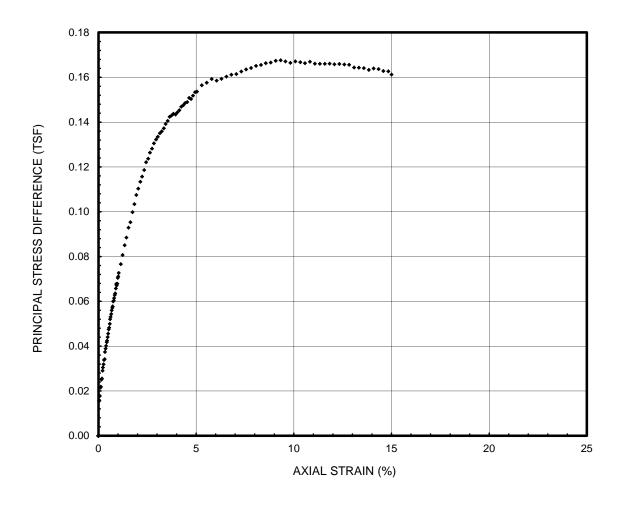
Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-01
Depth 4-6 ft



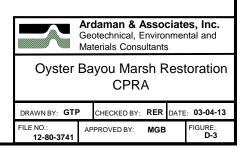
Initial Height	2.793	in	Cell Pressure	2.00	lb/in ²
Initial Diameter	1.389	in	Strain Rate	1.0	%/min
Dry Density	59.5	lb/ft ³	Peak Stress	0.06	ton/ft ²
Water Content	68.6	%	Strain at Peak Stress	1.02	%
Saturation	102	%	Failure Type	Diagona	l Plane



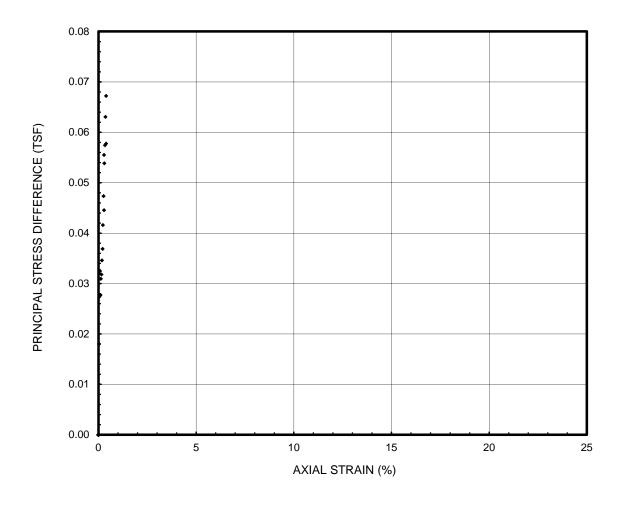
Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-01
Depth 8-10 ft



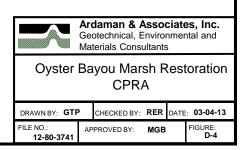
Initial Height Initial Diameter	5.754 2.793	in in	Cell Pressure Strain Rate	4.00 1.0	lb/in ² %/min
Dry Density	54.6	lb/ft ³	Peak Stress	0.168	ton/ft ²
Water Content	82.7	%	Strain at Peak Stress	9.32	%
Saturation	108	%	Failure Type	Bulging	



Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-01
Depth 12-14 ft



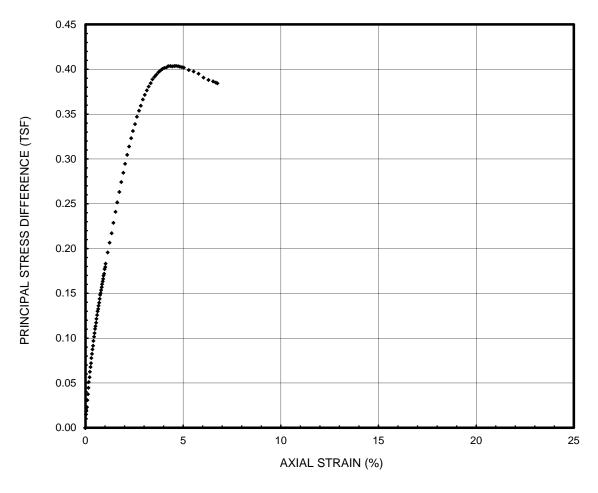
Initial Height	2.788	in	Cell Pressure	6.00	lb/in ²
Initial Diameter	1.330	in	Strain Rate	1.0	%/min
Dry Density	60.4	lb/ft ³	Peak Stress	0.067	ton/ft ²
Water Content	68.0	%	Strain at Peak Stress	0.39	%
Saturation	104	%	Failure Type	Combina	ıtion



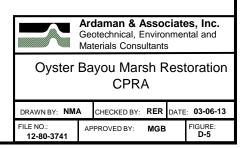
Project NameOyster BayouProject Number12-80-3741Sample NameB-01

Depth 16-18 ft

Description Gray CLAY (CH) w/ organics



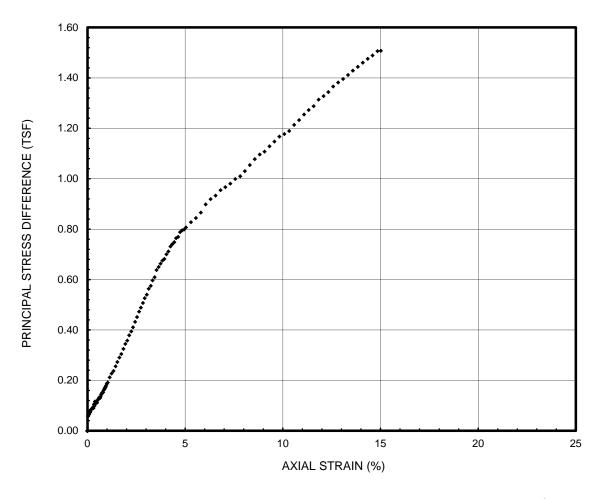
lb/in² **Cell Pressure** 7.00 **Initial Height** 5.583 in **Initial Diameter** 2.819 Strain Rate 1.0 %/min in lb/ft³ ton/ft² **Dry Density** 35.1 **Peak Stress** 0.404 **Water Content** 140.8 % **Strain at Peak Stress** 4.64 Saturation 100 % **Failure Type** Combination



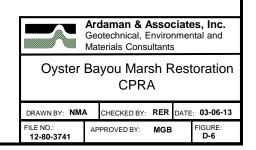
Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-01

Depth 18-20 ft

Description Gray SILTY CLAY (CL) w/ sand



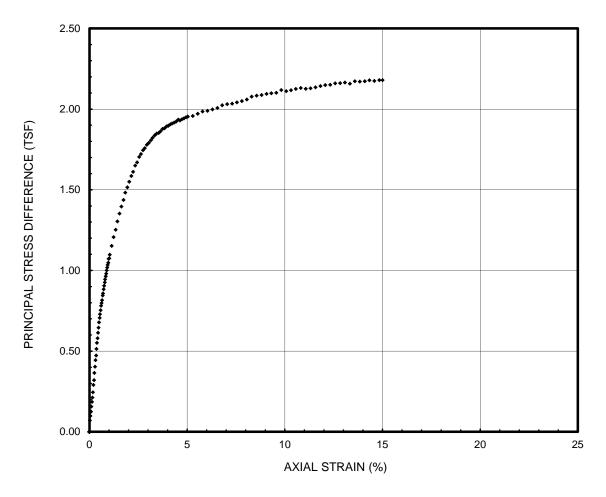
Initial Height	2.572	in	Cell Pressure	8.00	lb/in ²
Initial Diameter	1.393	in	Strain Rate	1.0	%/min
Dry Density	120.2	lb/ft ³	Peak Stress	1.508	ton/ft ²
Water Content	17.9	%	Strain at Peak Stress	15.02	%
Saturation	126	%	Failure Type	Bulging	



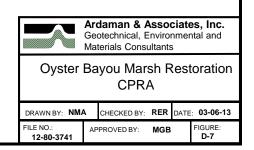
Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-01

Depth 23-25 ft

Description Gray SILTY CLAY (CL)



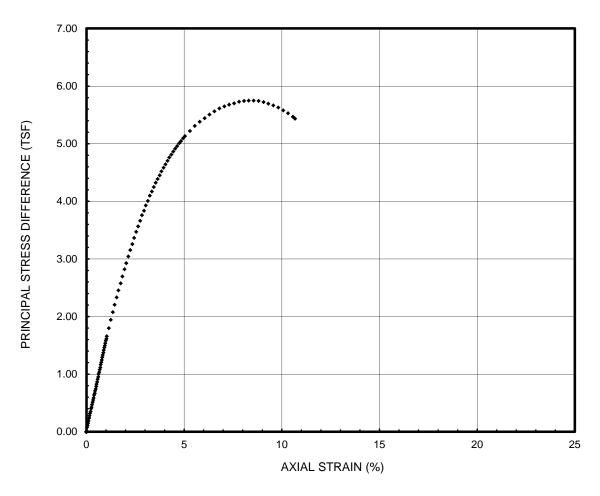
Initial Height Initial Diameter	2.801 1.414	in in	Cell Pressure Strain Rate	10.00 1.0	lb/in² %/min
Dry Density	107.7	lb/ft ³	Peak Stress	2.180	ton/ft ²
Water Content	19.7	%	Strain at Peak Stress	15.01	%
Saturation	97	%	Failure Type	Combination	



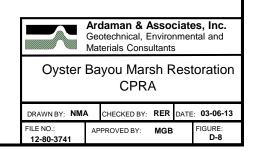
Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-01

Depth 33-35 ft

Description Gray SILTY SAND (SM) w/ trace clay

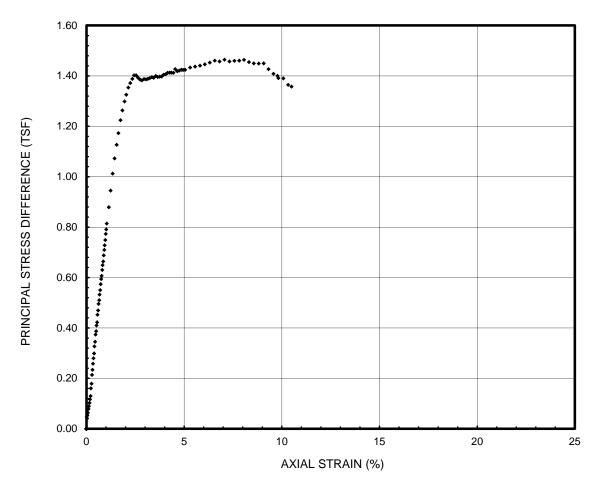


Initial Height Initial Diameter	2.801 1.400	in in	Cell Pressure Strain Rate	14.00 1.0	lb/in ² %/min
Dry Density	101.3	lb/ft ³	Peak Stress	5.748	ton/ft ²
Water Content	24.4	%	Strain at Peak Stress	8.31	%
Saturation	102	%	Failure Type	Bulging	

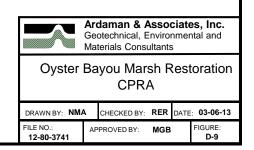


Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-01
Depth 38-40 ff

Description Brown and gray CLAY (CH) w/ silty sand layers



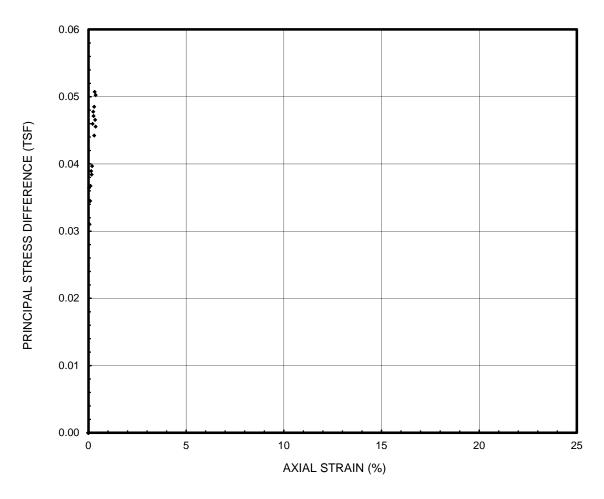
Initial Height	2.463	in	Cell Pressure	16.00	lb/in ²
Initial Diameter	1.438	in	Strain Rate	1.0	%/min
Dry Density	88.0	lb/ft ³	Peak Stress	1.464	ton/ft ²
Water Content	32.2	%	Strain at Peak Stress	7.07	%
Saturation	97	%	Failure Type	Combination	



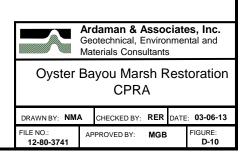
Project NameOyster BayouProject Number12-80-3741Sample NameB-02

Depth 2-4 ft

Description Gray CLAY (CH) w/ silt and trace organics



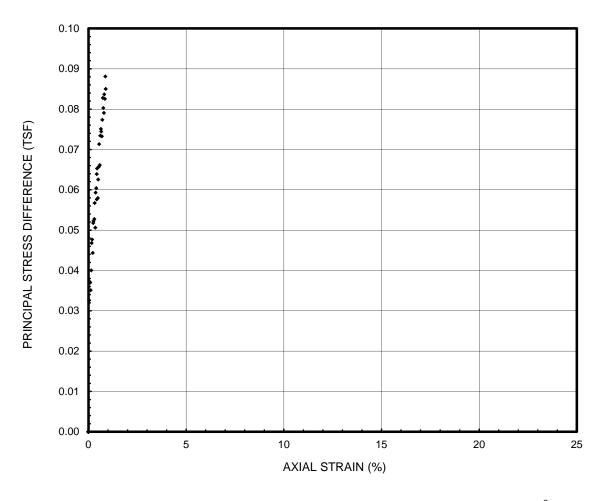
Initial Height	2.785	in	Cell Pressure	2.00	lb/in ²
Initial Diameter	1.354	in	Strain Rate	1.0	%/min
Dry Density	71.3	lb/ft ³	Peak Stress	0.051	ton/ft ²
Water Content	51.9	%	Strain at Peak Stress	0.31	%
Saturation	104	%	Failure Type	Combination	



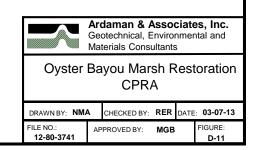
Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-02

Depth 4-6 ft

Description Gray CLAY (CH) w/ silt, trace organics, and



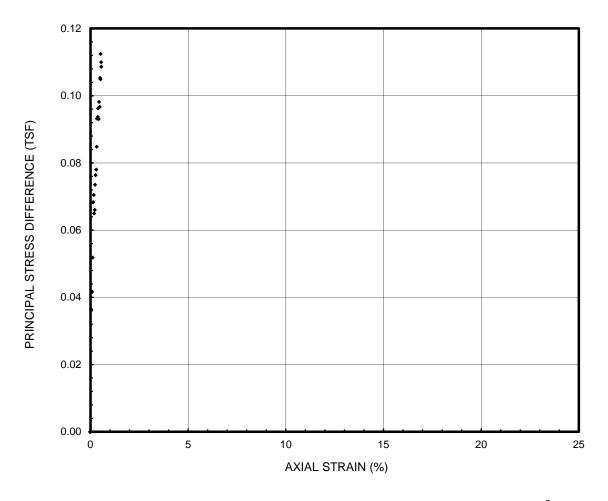
Initial Height	2.837	in	Cell Pressure	2.00	lb/in ²
Initial Diameter	1.394	in	Strain Rate	1.0	%/min
Dry Density	57.2	lb/ft ³	Peak Stress	0.088	ton/ft ²
Water Content	72.5	%	Strain at Peak Stress	0.87	%
Saturation	101	%	Failure Type	Diagonal Plane	



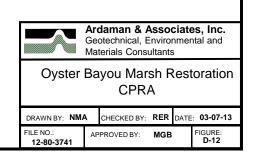
Project Name Oyster Bayou Project Number 12-80-3741 Sample Name B-02

Depth 8-10 ft

Description Gray CLAY (CH) w/ silt, trace organics, and



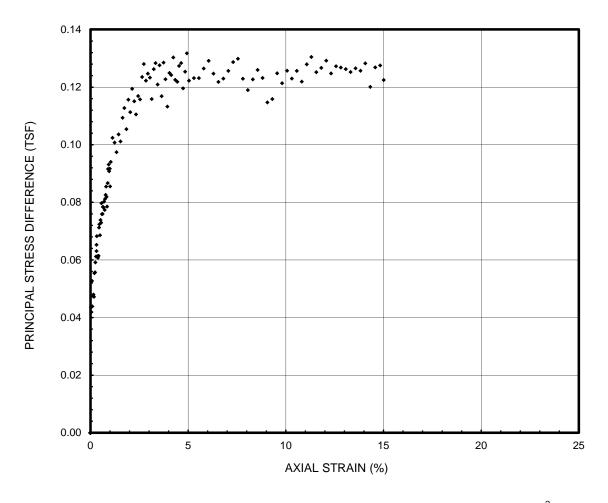
Initial Height	2.801	in	Cell Pressure	4.00	lb/in ²
Initial Diameter	1.346	in	Strain Rate	1.0	%/min
Dry Density	56.6	lb/ft ³	Peak Stress	0.112	ton/ft ²
Water Content	73.9	%	Strain at Peak Stress	0.52	%
Saturation	102	%	Failure Type	Bulging	



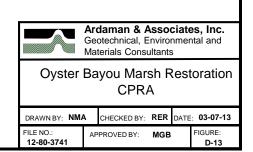
Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-02

Depth 10-12 ft

Description Gray CLAY (CH) w/ silt, trace organics, and



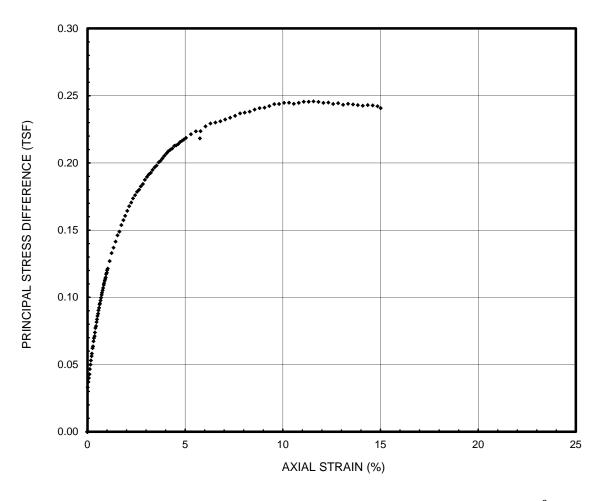
Initial Height	2.777	in	Cell Pressure	5.00	lb/in ²
Initial Diameter	1.363	in	Strain Rate	1.0	%/min
Dry Density	64.0	lb/ft ³	Peak Stress	0.132	ton/ft ²
Water Content	61.3	%	Strain at Peak Stress	4.94	%
Saturation	103	%	Failure Type	Combination	



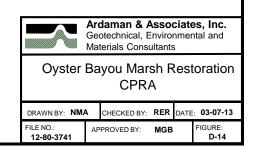
Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-02

Depth 14-16 ft

Description Gray CLAY (CH) w/ silt, trace organics, and



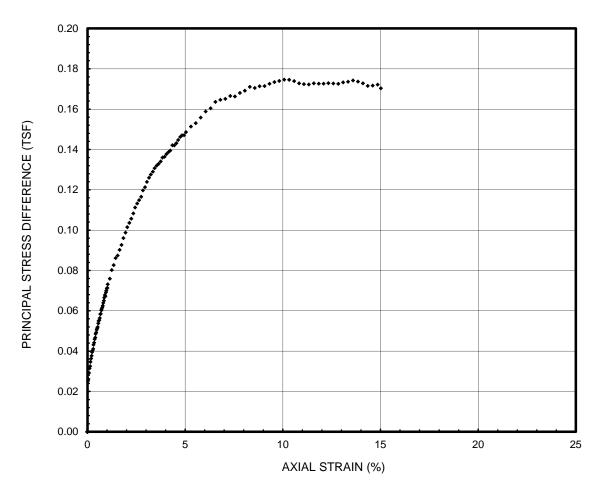
Initial Height	5.576	in	Cell Pressure	6.00	lb/in ²
Initial Diameter	2.789	in	Strain Rate	1.0	%/min
Dry Density	70.6	lb/ft ³	Peak Stress	0.246	ton/ft ²
Water Content	52.2	%	Strain at Peak Stress	11.57	%
Saturation	103	%	Failure Type	Bulging	



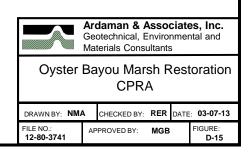
Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-02

Depth 18-20 ft

Description Gray SILTY CLAY (CL)



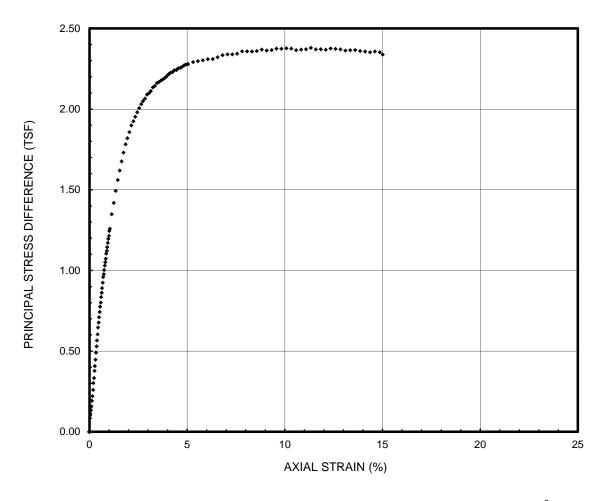
Initial Height Initial Diameter	5.801 2.788	in in	Cell Pressure Strain Rate	8.00 1.0	lb/in² %/min
Dry Density	74.4	lb/ft ³	Peak Stress	0.175	ton/ft ²
Water Content	50.0	%	Strain at Peak Stress	10.07	%
Saturation	108	%	Failure Type	Other	



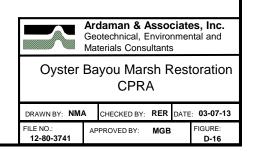
Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-02

Depth 28-30 ft

Description Gray SILTY CLAY (CL)



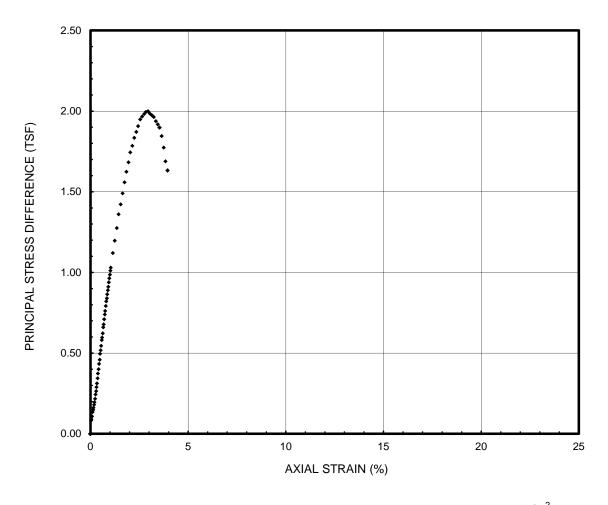
Initial Height	2.806	in	Cell Pressure	12.00	lb/in ²
Initial Diameter	1.387	in	Strain Rate	1.0	%/min
Dry Density	109.5	lb/ft ³	Peak Stress	2.380	ton/ft ²
Water Content	19.6	%	Strain at Peak Stress	11.34	%
Saturation	102	%	Failure Type	Bulging	



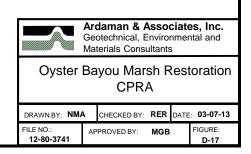
Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-02

Depth 43-45 ft

Description Gray CLAY (CH) w/ silt layers



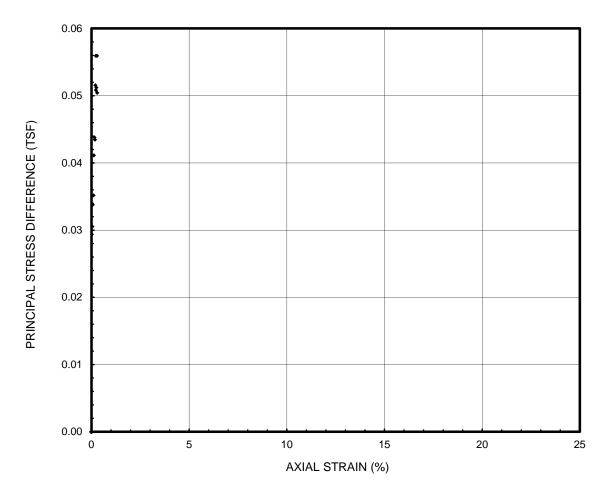
Initial Height	2.816	in	Cell Pressure	18.00	lb/in ²
Initial Diameter	1.423	in	Strain Rate	1.0	%/min
Dry Density	90.2	lb/ft ³	Peak Stress	1.999	ton/ft ²
Water Content	30.4	%	Strain at Peak Stress	2.95	%
Saturation	97	%	Failure Type	Other	



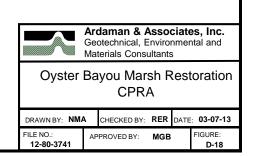
Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-03

Depth 0-2

Description Gray CLAY (CH) w/ silt

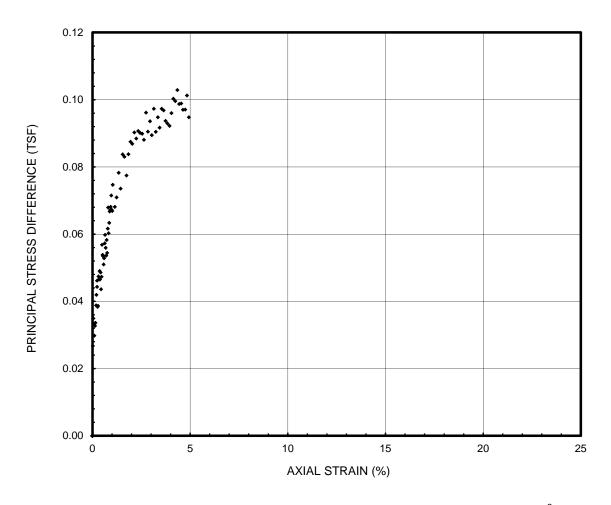


Initial Height	2.786	in	Cell Pressure	1.00	lb/in ²
Initial Diameter	1.346	in	Strain Rate	1.0	%/min
Dry Density	65.3	lb/ft ³	Peak Stress	0.056	ton/ft ²
Water Content	58.9	%	Strain at Peak Stress	0.23	%
Saturation	102	%	Failure Type	Bulging	

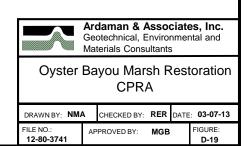


Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-03
Depth 2-4 ft

Description Gray SILTY CLAY (CL) w/ shells



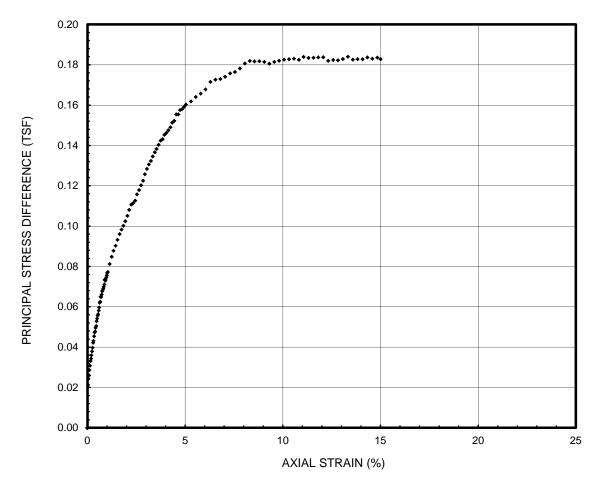
lb/in² **Cell Pressure Initial Height** 2.753 2.00 in **Initial Diameter** 1.371 Strain Rate 1.0 %/min in lb/ft³ ton/ft² **Dry Density** 72.0 **Peak Stress** 0.103 **Water Content** 50.5 % **Strain at Peak Stress** 4.34 Saturation 103 % **Failure Type** Combination



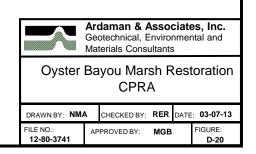
Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-03

Depth 6-8 ft

Description Gray SILTY CLAY (CL) w/ shells



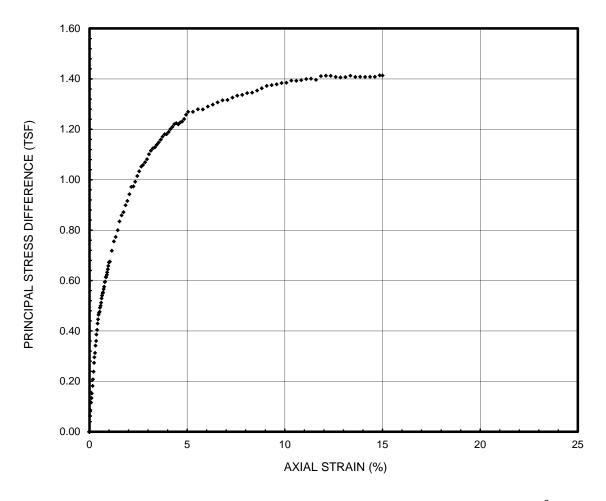
Initial Height Initial Diameter	5.805 2.800	in in	Cell Pressure Strain Rate	3.00 1.0	lb/in ² %/min
Dry Density	68.1	lb/ft ³	Peak Stress	0.184	ton/ft ²
Water Content	56.6	%	Strain at Peak Stress	13.33	%
Saturation	105	%	Failure Type	Combination	



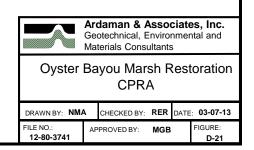
Project NameOyster BayouProject Number12-80-3741Sample NameB-03

Depth 16-18 ft

Description Gray SILTY CLAY (CL) w/ silt pockets

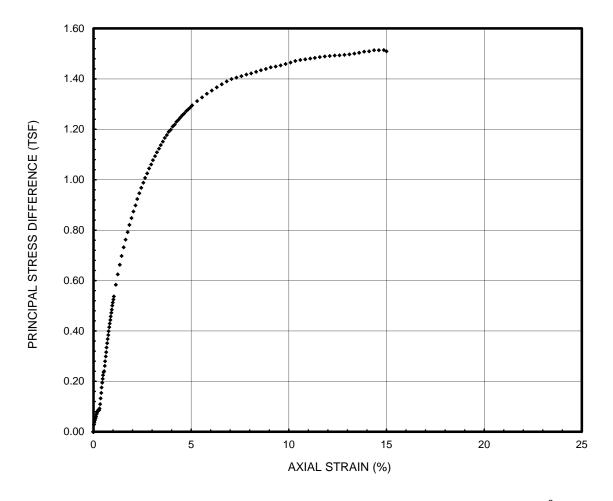


Initial Height	2.791	in	Cell Pressure	7.00	lb/in ²
Initial Diameter	1.372	in	Strain Rate	1.0	%/min
Dry Density	103.3	lb/ft ³	Peak Stress	1.414	ton/ft ²
Water Content	23.4	%	Strain at Peak Stress	14.85	%
Saturation	103	%	Failure Type	Combination	

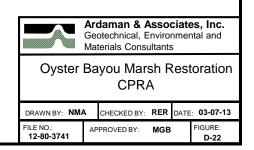


Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-03
Depth 18-20 ft

Description Gray SILTY CLAY (CL) w/ silt pockets



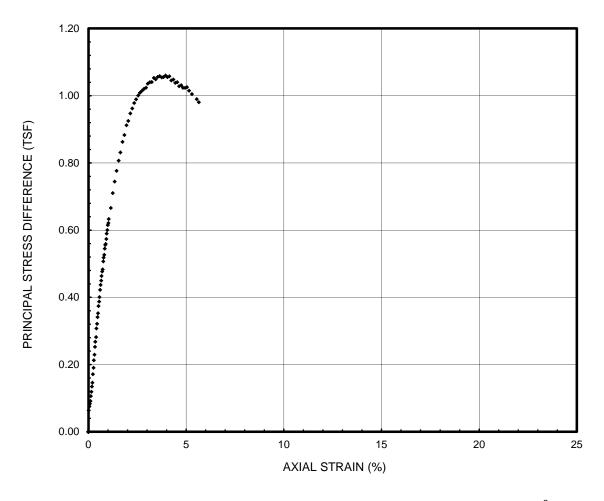
Initial Height	5.822	in	Cell Pressure	8.00	lb/in ²
Initial Diameter	2.833	in	Strain Rate	1.0	%/min
Dry Density	103.8	lb/ft ³	Peak Stress	1.514	ton/ft ²
Water Content	23.3	%	Strain at Peak Stress	14.86	%
Saturation	104	%	Failure Type	Bulging	



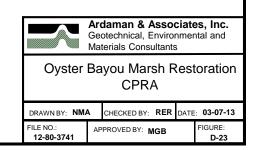
Project NameOyster BayouProject Number12-80-3741Sample NameB-03

Depth 33-35 ft

Description Light gray SILTY CLAY (CL)



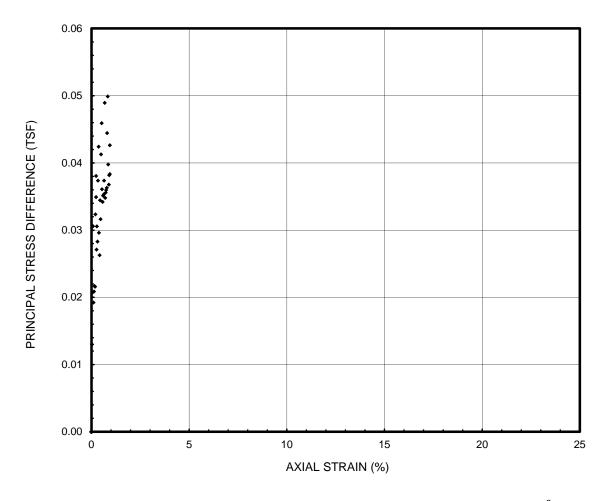
Initial Height	2.797	in	Cell Pressure	14.00	lb/in ²
Initial Diameter	1.391	in	Strain Rate	1.0	%/min
Dry Density	86.0	lb/ft ³	Peak Stress	1.060	ton/ft ²
Water Content	35.4	%	Strain at Peak Stress	3.95	%
Saturation	102	%	Failure Type	Combination	



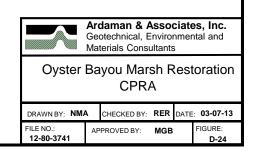
Project NameOyster BayouProject Number12-80-3741Sample NameB-04

Depth 2-4 ft

Description Gray CLAY (CH) w/ trace organics and shell

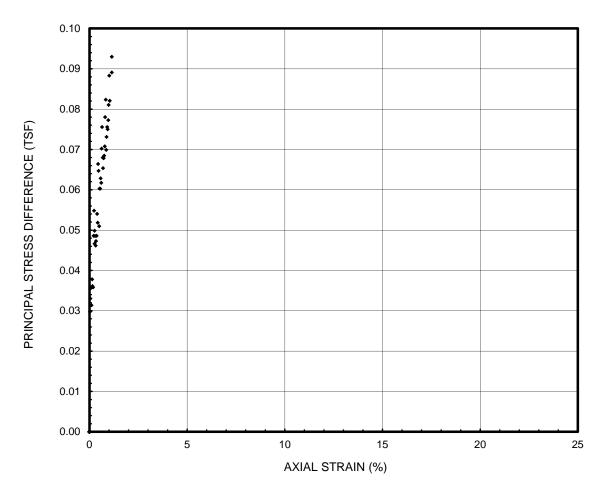


Initial Height	2.766	in	Cell Pressure	2.00	lb/in ²
Initial Diameter	1.373	in	Strain Rate	1.0	%/min
Dry Density	65.4	lb/ft ³	Peak Stress	0.050	ton/ft ²
Water Content	60.5	%	Strain at Peak Stress	0.84	%
Saturation	105	%	Failure Type	Diagonal Plane	

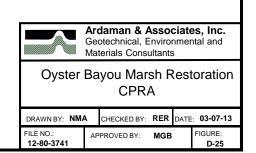


Project Name Oyster Bayou **Project Number** 12-80-3741 Sample Name B-04 Depth 6-8

Description Gray CLAY (CH) w/ trace organics and shell



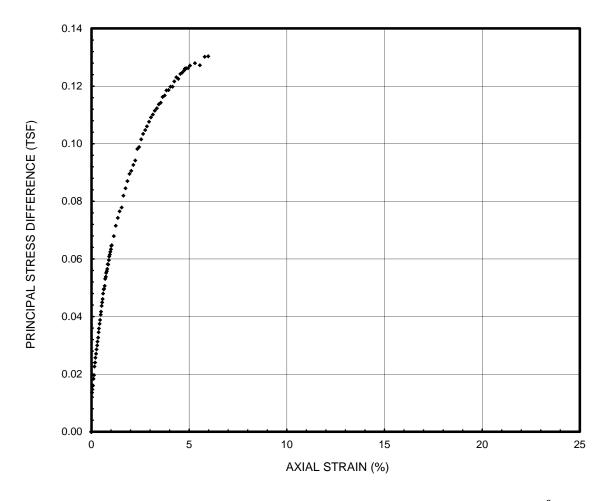
Initial Height Initial Diameter	2.770 1.370	in in	Cell Pressure Strain Rate	3.00 1.0	lb/in² %/min
Dry Density	52.9	lb/ft ³	Peak Stress	0.093	ton/ft ²
Water Content	80.9	%	Strain at Peak Stress	1.14	%
Saturation	101	%	Failure Type	Other	



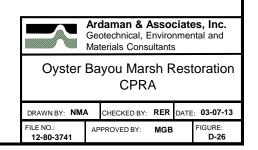
Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-04

Depth 8-10 ft

Description Gray CLAY (CH) w/ trace organics and shell

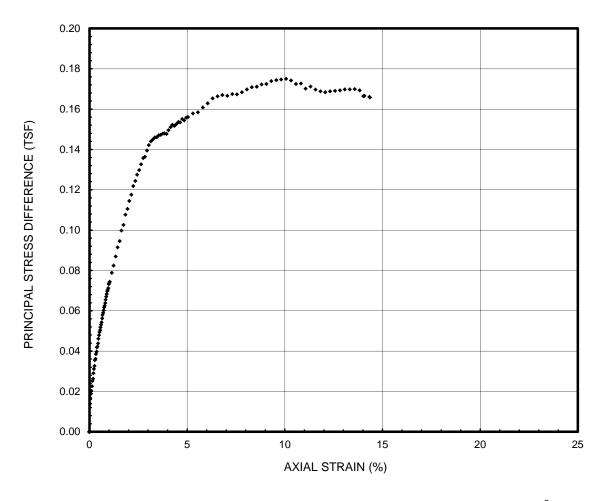


Initial Height	5.800	in	Cell Pressure	4.00	lb/in ²
Initial Diameter	2.801	in	Strain Rate	1.0	%/min
Dry Density	58.4	lb/ft ³	Peak Stress	0.130	ton/ft ²
Water Content	74.4	%	Strain at Peak Stress	5.98	%
Saturation	108	%	Failure Type	Combination	

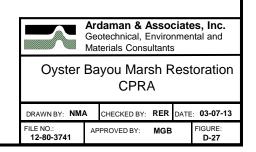


Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-04
Depth 12-14 ft

Description Gray CLAY (CH) w/ trace organics and shell



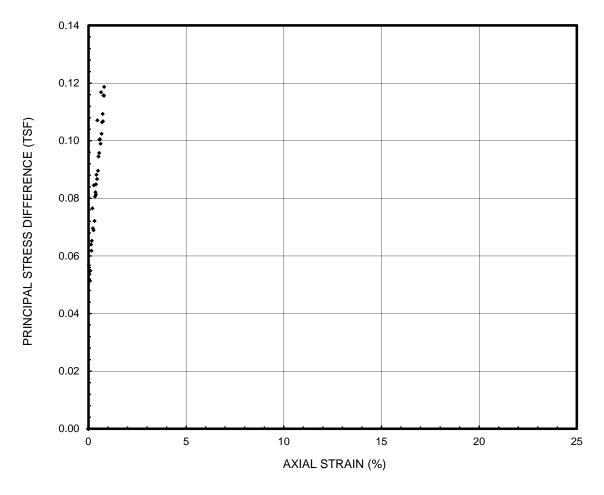
Initial Height	5.810	in	Cell Pressure	6.00	lb/in ²
Initial Diameter	2.787	in	Strain Rate	1.0	%/min
Dry Density	54.9	lb/ft ³	Peak Stress	0.175	ton/ft ²
Water Content	80.5	%	Strain at Peak Stress	10.07	%
Saturation	106	%	Failure Type	Combination	



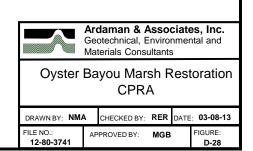
Project NameOyster BayouProject Number12-80-3741Sample NameB-04

Depth 16-18 ft

Description Gray SILTY CLAY (CL)



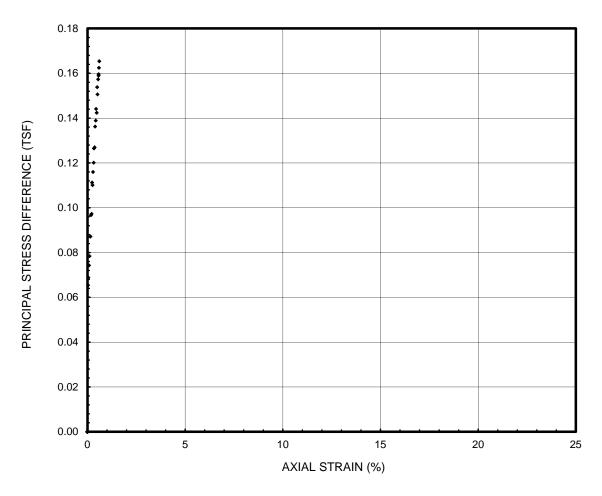
Initial Height	2.769	in	Cell Pressure	7.00	lb/in ²
Initial Diameter	1.394	in	Strain Rate	1.0	%/min
Dry Density	99.8	lb/ft ³	Peak Stress	0.119	ton/ft ²
Water Content	25.5	%	Strain at Peak Stress	0.80	%
Saturation	103	%	Failure Type	Bulging	



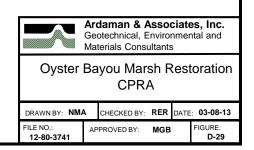
Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-04

Depth 18-20 ft

Description Gray SILTY CLAY (CL)

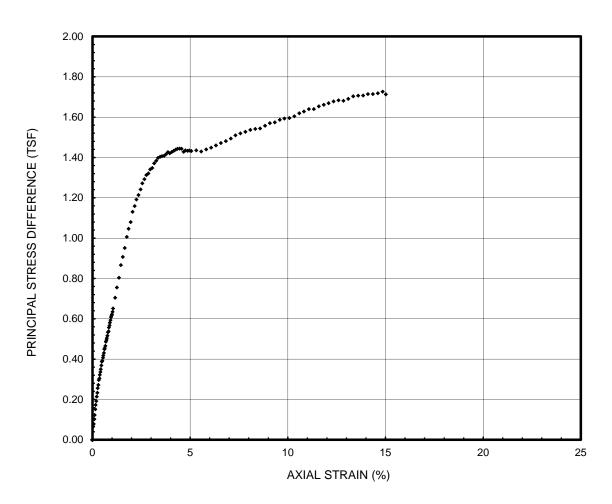


Initial Height	2.766	in	Cell Pressure	8.00	lb/in ²
Initial Diameter	1.340	in	Strain Rate	1.0	%/min
Dry Density	106.9	lb/ft ³	Peak Stress	0.165	ton/ft ²
Water Content	23.1	%	Strain at Peak Stress	0.60	%
Saturation	112	%	Failure Type	Bulging	

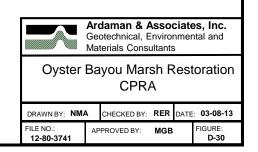


Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-04
Depth 23-25 ft

Description Gray SANDY CLAY (CL) w/ silt

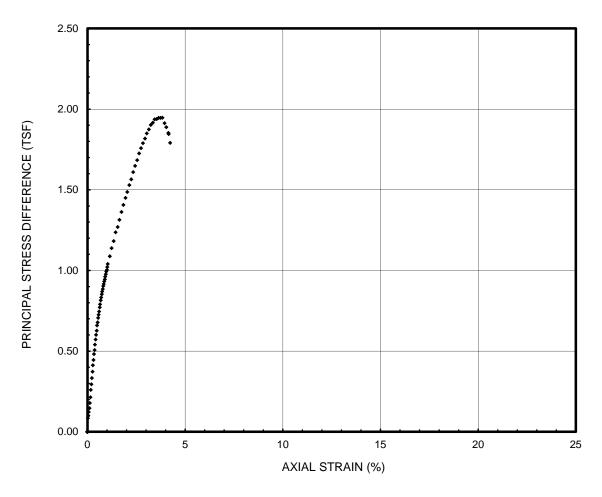


Initial Height Initial Diameter	2.804 1.392	in in	Cell Pressure Strain Rate	10.00 1.0	lb/in² %/min
Dry Density	109.2	lb/ft ³	Peak Stress	1.726	ton/ft ²
Water Content	19.7	%	Strain at Peak Stress	14.86	%
Saturation	101	%	Failure Type	Combination	

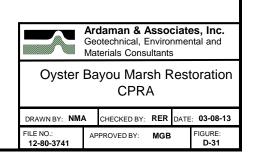


Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-04
Depth 33-35 ft

Description Tan and gray CLAY (CH) w/ silt layers

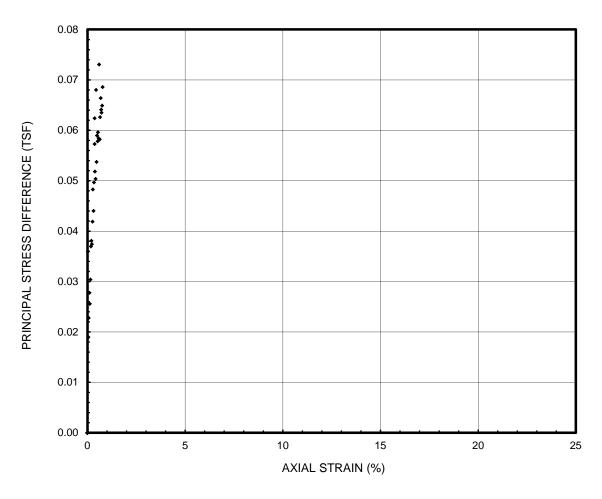


Initial Height Initial Diameter	2.811 1.401	in in	Cell Pressure Strain Rate	14.00 1.0	lb/in ² %/min
Dry Density	85.0	lb/ft ³	Peak Stress	1.947	ton/ft ²
Water Content	37.2	%	Strain at Peak Stress	3.84	%
Saturation	104	%	Failure Type	Diagonal Plane	

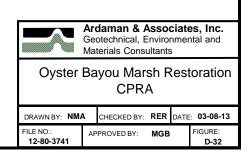


Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-05
Depth 4-6 ft

Description 4-6 ft Gray CLAY (CH)



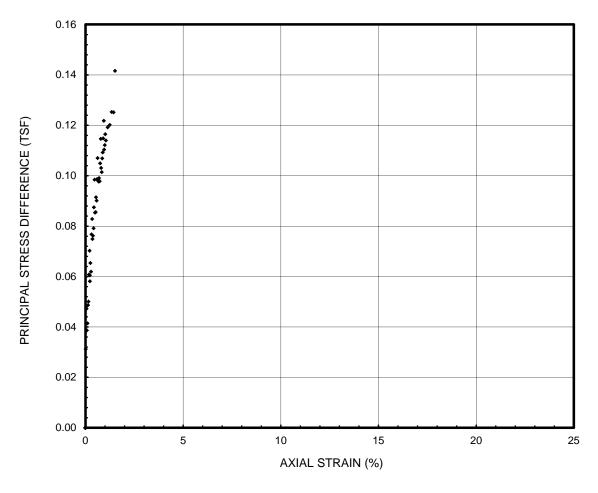
lb/in² **Cell Pressure Initial Height** 2.801 2.00 in **Initial Diameter** 1.375 Strain Rate 1.0 %/min in lb/ft³ ton/ft² **Dry Density** 49.4 **Peak Stress** 0.073 **Water Content** 93.4 % **Strain at Peak Stress** 0.59 Saturation 105 % **Failure Type** Diagonal Plane



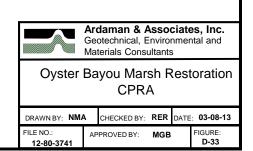
Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-05

Depth 8-10 ff

Description Gray CLAY (CH) with shells

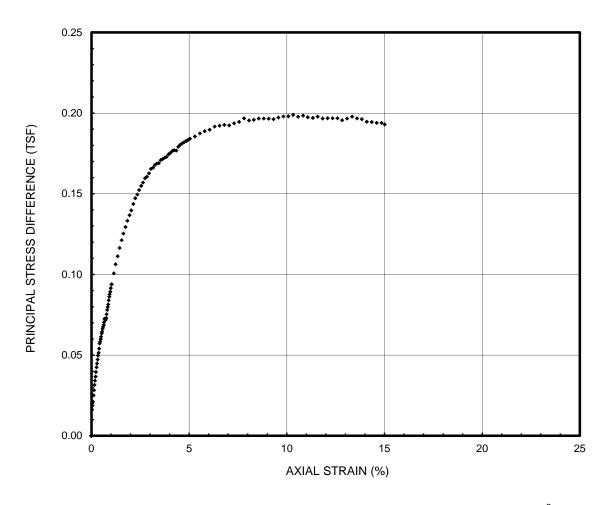


Initial Height Initial Diameter	2.781 1.397	in in	Cell Pressure Strain Rate	4.00 1.0	lb/in² %/min
Dry Density	53.0	lb/ft ³	Peak Stress	0.142	ton/ft ²
Water Content	82.9	%	Strain at Peak Stress	1.51	%
Saturation	104	%	Failure Type	Diagonal Plane	

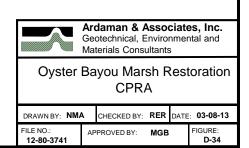


Project Name
Oyster Bayou
Project Number
12-80-3741
Sample Name
B-05
Depth
12-14
ft

Description 12-14 ft Gray CLAY (CH)

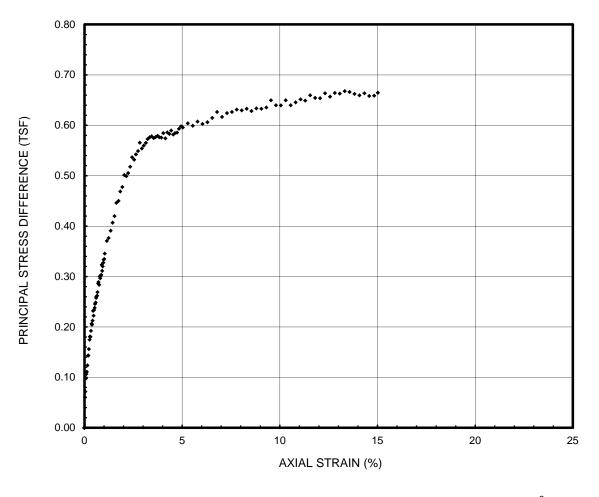


lb/in² **Cell Pressure Initial Height** 5.801 6.00 in **Initial Diameter** 2.831 Strain Rate 1.0 %/min in lb/ft³ ton/ft² **Dry Density** 56.6 **Peak Stress** 0.199 **Water Content** 73.5 % **Strain at Peak Stress** 10.33 % Saturation 101 % **Failure Type** Bulging

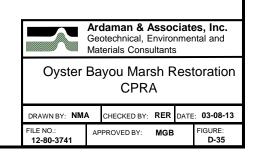


Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-05
Depth 16-18 ft

Description Brown and gray CLAY (CH) w/ silty sand

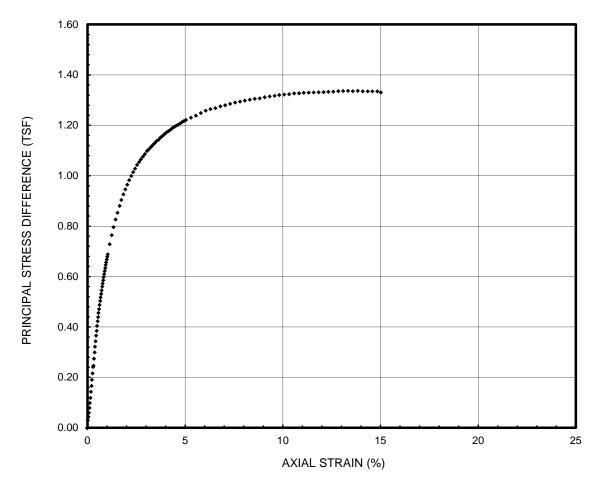


Initial Height	2.802	in	Cell Pressure	7.00	lb/in ²
Initial Diameter	1.390	in	Strain Rate	1.0	%/min
Dry Density	92.6	lb/ft ³	Peak Stress	0.668	ton/ft ²
Water Content	28.0	%	Strain at Peak Stress	13.32	%
Saturation	94	%	Failure Type	Bulging	

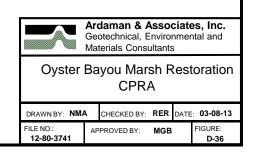


Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-05
Depth 18-20 ft

Description Brown and gray CLAY (CH) w/ silty sand



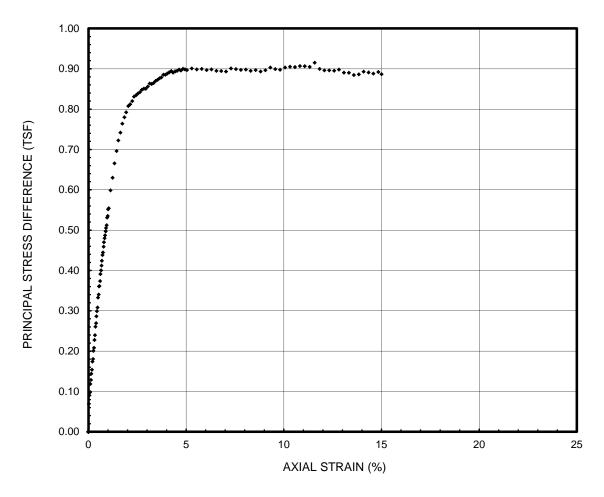
Initial Height	5.825	in	Cell Pressure	8.00	lb/in ²
Initial Diameter	2.837	in	Strain Rate	1.0	%/min
Dry Density	105.8	lb/ft ³	Peak Stress	1.337	ton/ft ²
Water Content	22.9	%	Strain at Peak Stress	13.34	%
Saturation	108	%	Failure Type	Combination	



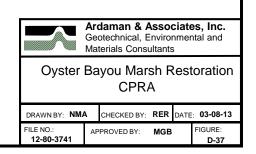
Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-05

Depth 28-30 ft

Description Gray SILTY CLAY (CL)

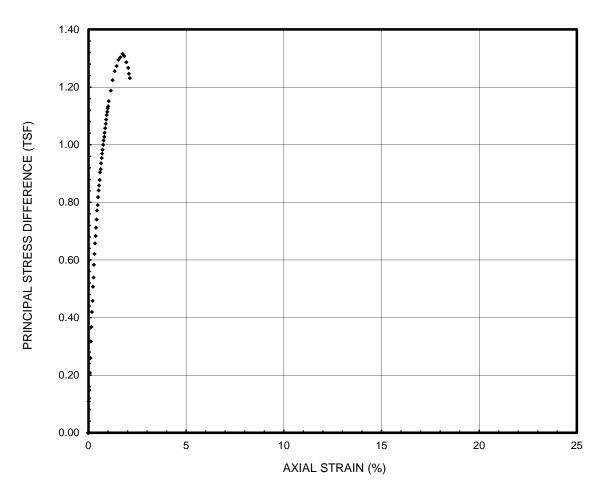


Initial Height Initial Diameter	2.804 1.369	in in	Cell Pressure Strain Rate	12.00 1.0	lb/in² %/min
Dry Density	90.1	lb/ft ³	Peak Stress	0.915	ton/ft ²
Water Content	33.0	%	Strain at Peak Stress	11.58	%
Saturation	105	%	Failure Type	Combination	

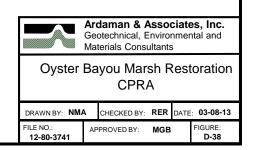


Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-05
Depth 38-40 ft

Description Tan and gray CLAY (CH) w/ silt layers

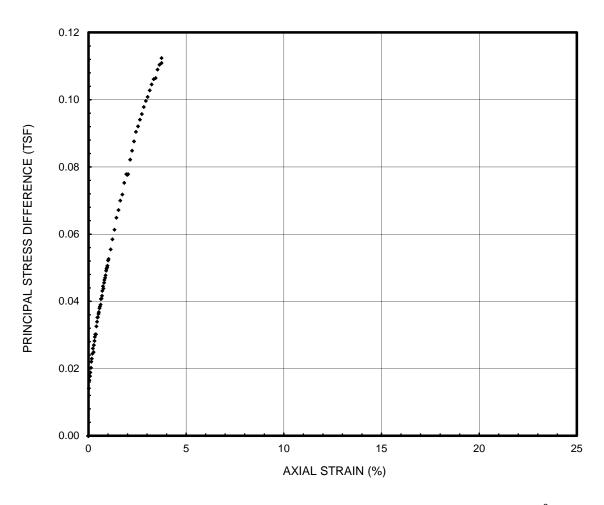


Initial Height	2.807	in	Cell Pressure	16.00	lb/in ²
Initial Diameter	1.368	in	Strain Rate	1.0	%/min
Dry Density	76.4	lb/ft ³	Peak Stress	1.316	ton/ft ²
Water Content	48.2	%	Strain at Peak Stress	1.74	%
Saturation	110	%	Failure Type	Diagonal Plane	

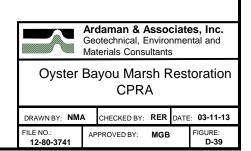


Project Name
Oyster Bayou
12-80-3741
Sample Name
B-06

Depth 2-4 ft **Description** Gray CLAY (CH)



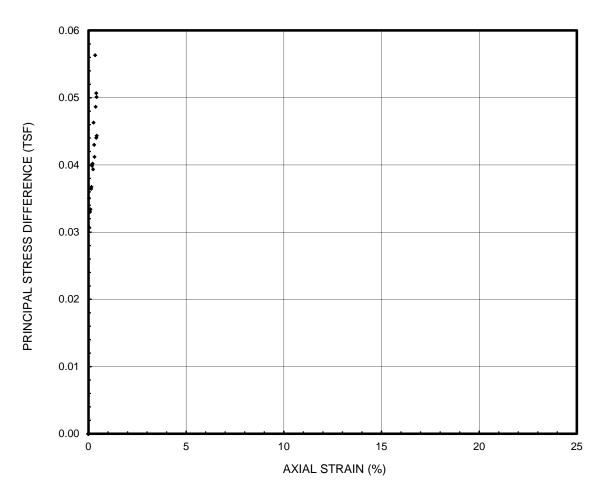
lb/in² **Cell Pressure Initial Height** 5.808 2.00 in **Initial Diameter** 2.795 Strain Rate 1.0 %/min in lb/ft³ ton/ft² **Dry Density** 52.6 **Peak Stress** 0.112 **Water Content** 86.4 % **Strain at Peak Stress** 3.74 % Saturation 107 % **Failure Type Bulging**



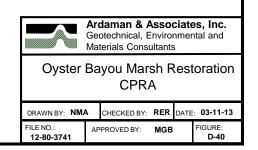
Project NameOyster BayouProject Number12-80-3741Sample NameB-06

Depth 4-6 ft

Description Gray CLAY (CH) with shells



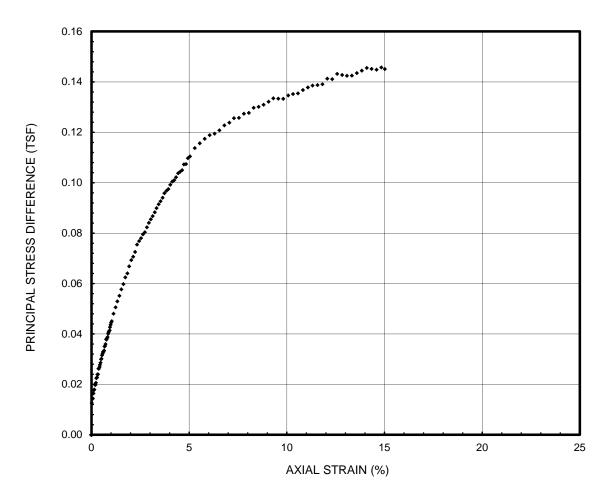
Initial Height	2.786	in	Cell Pressure	2.00	lb/in ²
Initial Diameter	1.339	in	Strain Rate	1.0	%/min
Dry Density	46.9	lb/ft ³	Peak Stress	0.056	ton/ft ²
Water Content	98.8	%	Strain at Peak Stress	0.34	%
Saturation	104	%	Failure Type	Bulging	



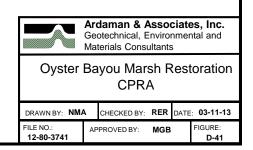
Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-06

Depth 8-10 f

Description Gray CLAY (CH) with shells

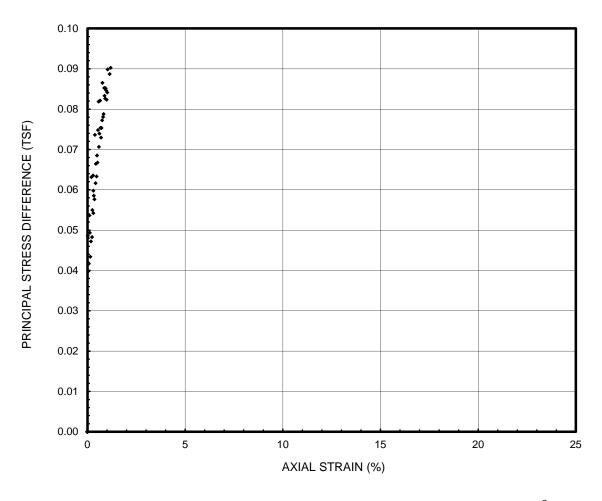


Initial Height	5.760	in	Cell Pressure	4.00	lb/in ²
Initial Diameter	2.810	in	Strain Rate	1.0	%/min
Dry Density	55.5	lb/ft ³	Peak Stress	0.146	ton/ft ²
Water Content	81.6	%	Strain at Peak Stress	14.84	%
Saturation	109	%	Failure Type	Combination	

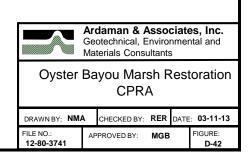


Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-06
Depth 12-14 ft

Description 12-14 ft Gray CLAY (CH)



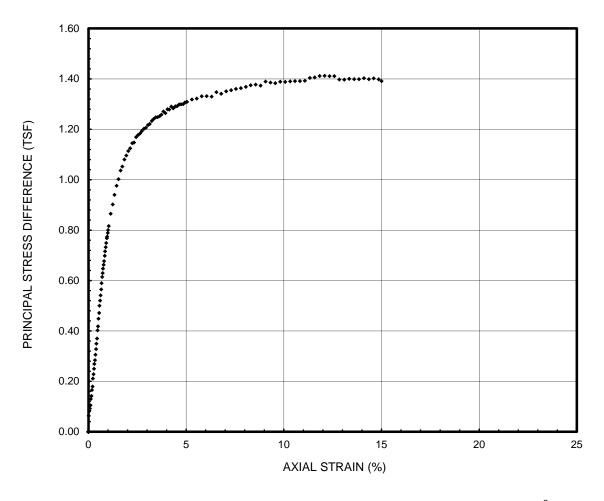
lb/in² **Cell Pressure Initial Height** 2.797 6.00 in **Initial Diameter** 1.394 Strain Rate 1.0 %/min in lb/ft³ ton/ft² **Dry Density** 48.1 **Peak Stress** 0.090 **Water Content** 91.7 % **Strain at Peak Stress** 1.18 % Saturation 100 % Filaure Type **Bulging**



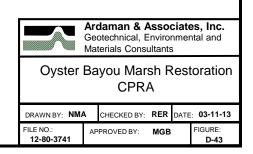
Project NameOyster BayouProject Number12-80-3741Sample NameB-06

Depth 16-18 ft

Description Gray SANDY CLAY (CL)

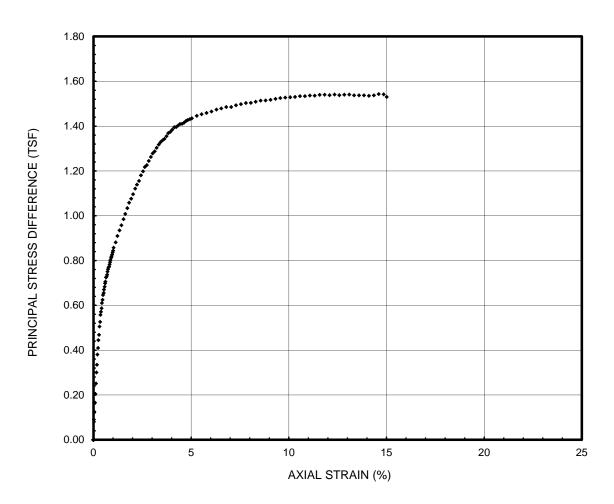


Initial Height	2.802	in	Cell Pressure	7.00	lb/in ²
Initial Diameter	1.379	in	Strain Rate	1.0	%/min
Dry Density	103.8	lb/ft ³	Peak Stress	1.412	ton/ft ²
Water Content	22.9	%	Strain at Peak Stress	12.09	%
Saturation	102	%	Failure Type	Bulging	

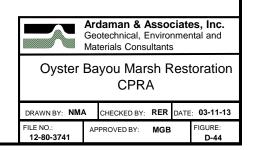


Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-06
Depth 24-25 ft

Description Gray CLAY (CH) w/ silt layers

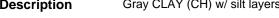


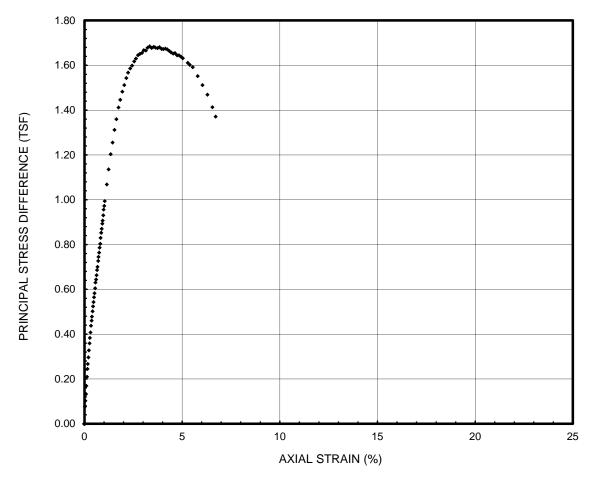
Initial Height Initial Diameter	2.799 1.366	in in	Cell Pressure Strain Rate	10.00 1.0	lb/in² %/min
Dry Density	104.0	lb/ft ³	Peak Stress	1.543	ton/ft ²
Water Content	23.0	%	Strain at Peak Stress	14.60	%
Saturation	103	%	Failure Type	Combination	



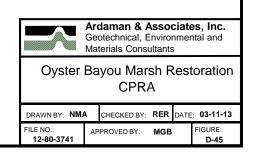
Project Name Oyster Bayou **Project Number** 12-80-3741 Sample Name B-06 Depth 48-50

Description Gray CLAY (CH) w/ silt layers





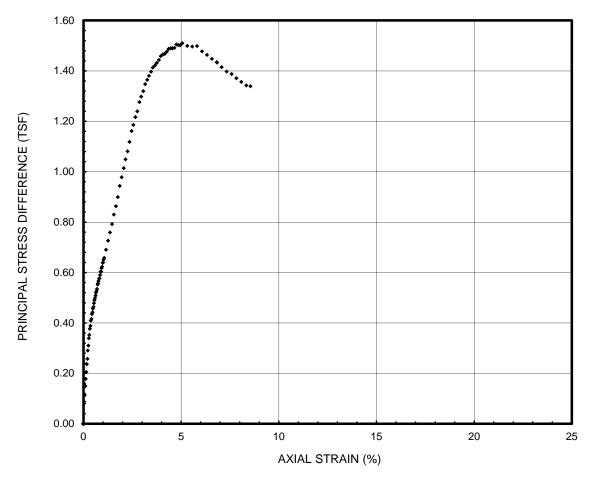
Initial Height Initial Diameter	2.817 1.406	in in	Cell Pressure Strain Rate	20.00 1.0	lb/in² %/min
Dry Density	82.1	lb/ft ³	Peak Stress	1.684	ton/ft ²
Water Content	39.4	%	Strain at Peak Stress	3.34	%
Saturation	103	%	Failure Type	Diagonal Plane	



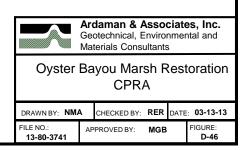
Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-06

Depth 53-55 ft

Description Gray CLAY (CH) w/ silt layers



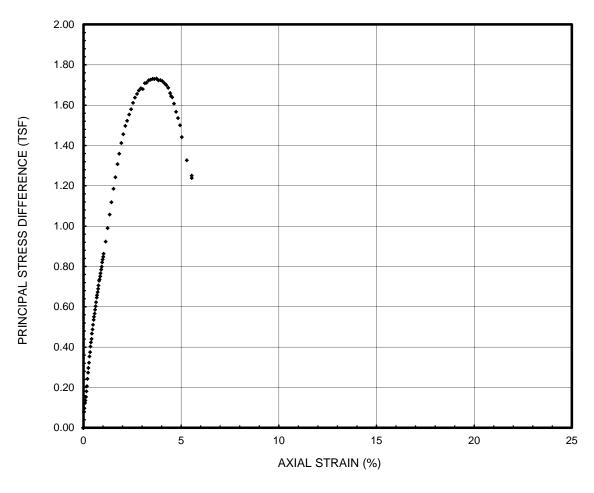
Initial Height Initial Diameter	2.799 1.382	in in	Cell Pressure Strain Rate	22.00 1.0	lb/in² %/min
Dry Density	83.1	lb/ft ³	Peak Stress	1.510	ton/ft ²
Water Content	38.5	%	Strain at Peak Stress	5.06	%
Saturation	103	%	Failure Type	Combination	



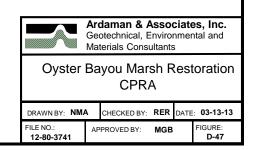
Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-06

Depth 58-60 ft

Description Gray CLAY (CH) w/ silt layers

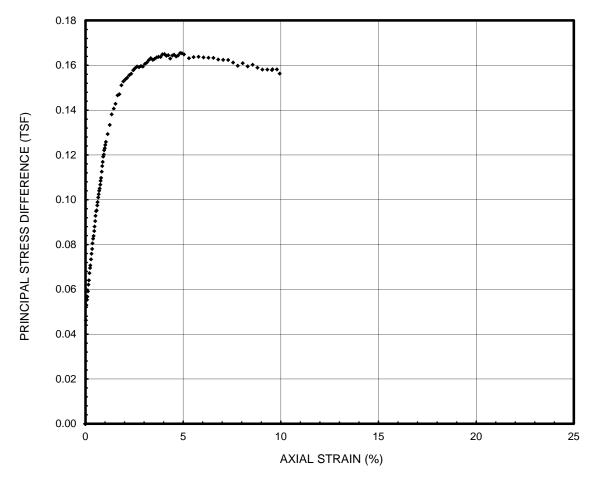


Initial Height Initial Diameter	2.792 1.389	in in	Cell Pressure Strain Rate	24.00 1.0	lb/in² %/min
Dry Density	75.8	lb/ft ³	Peak Stress	1.732	ton/ft ²
Water Content	45.9	%	Strain at Peak Stress	3.74	%
Saturation	103	%	Failure Type	Diagonal Plane	

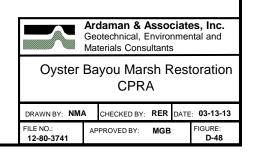


Project NameOyster BayouProject Number12-80-3741Sample NameB-07 (BL3)Depth8-10ft

Description Gray CLAY (CH) w/ silt and sand layers



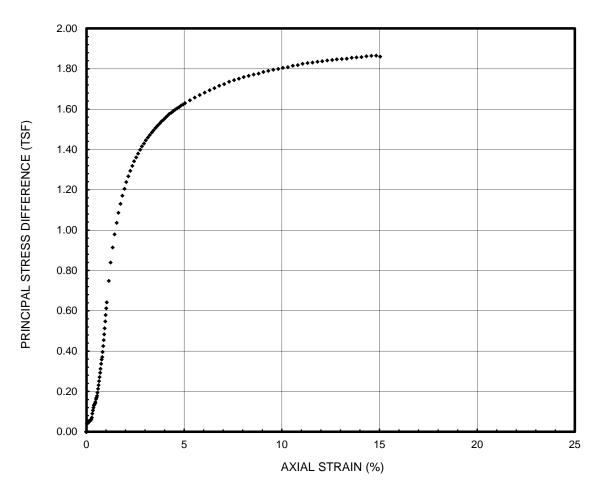
Initial Height Initial Diameter	2.771 1.323	in in	Cell Pressure Strain Rate	6.00 1.0	lb/in² %/min
Dry Density	63.9	lb/ft ³	Peak Stress	0.165	ton/ft ²
Water Content	65.6	%	Strain at Peak Stress	4.85	%
Saturation	109	%	Failure Type	Diagonal Plane	



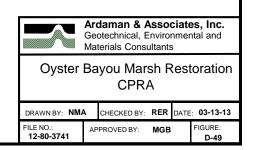
Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-07

Depth 23-25 ft

Description Gray SILTY CLAY (CL)



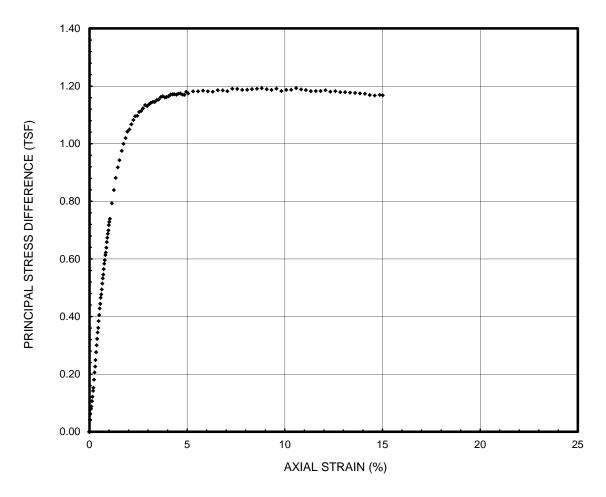
Initial Height Initial Diameter	5.749 2.849	in in	Cell Pressure Strain Rate	10.00 1.0	lb/in ² %/min
Dry Density	110.2	lb/ft ³	Peak Stress	1.865	ton/ft ²
Water Content	20.1	%	Strain at Peak Stress	14.83	%
Saturation	106	%	Failure Type	Bulging	



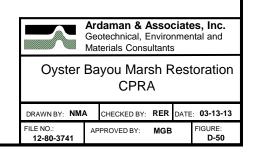
Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-07

Depth 33-35 ft

Description Gray SILTY CLAY (CL)

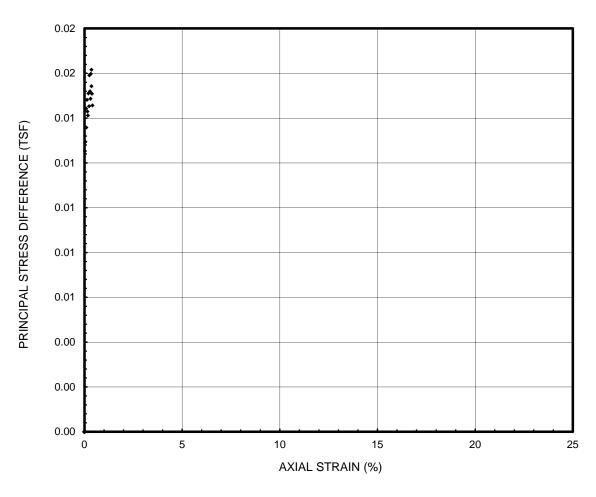


Initial Height Initial Diameter	2.800 1.406	in in	Cell Pressure Strain Rate	14.00 1.0	lb/in ² %/min
Dry Density	100.5	lb/ft ³	Peak Stress	1.193	ton/ft ²
Water Content	23.1	%	Strain at Peak Stress	10.58	%
Saturation	95	%	Failure Type	Combination	

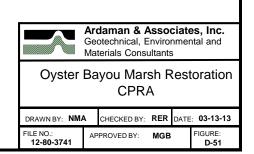


Project NameOyster BayouProject Number12-80-3741Sample NameB-07 (BL-1)Depth6-8ft

Description Gray CLAY (CH) w/ silt

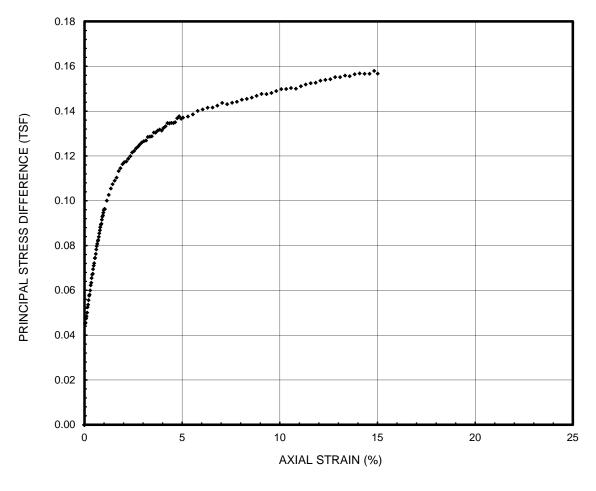


Initial Height	5.567	in	Cell Pressure	3.00	lb/in ²
Initial Diameter	2.826	in	Strain Rate	1.0	%/min
Dry Density	67.3	lb/ft ³	Peak Stress	0.016	ton/ft ²
Water Content	50.9	%	Strain at Peak Stress	0.36	%
Saturation	93	%	Failure Type	Bulging	

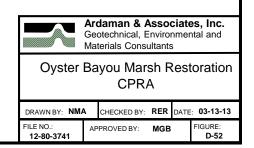


Project NameOyster BayouProject Number12-80-3741Sample NameB-07 (BL-1)Depth8-10

Description Gray CLAY (CH) w/ silt and sand layers

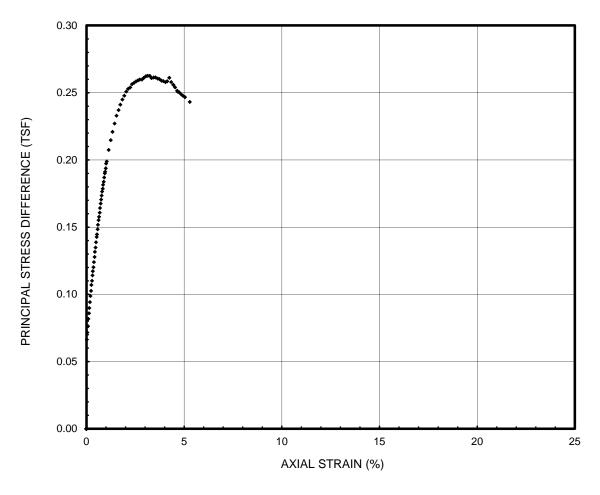


lb/in² **Cell Pressure Initial Height** 2.773 6.00 in **Initial Diameter** 1.374 Strain Rate 1.0 %/min in lb/ft³ ton/ft² **Dry Density** 51.6 **Peak Stress** 0.158 **Water Content** 85.2 % **Strain at Peak Stress** 14.83 Saturation 102 % **Failure Type** Combination

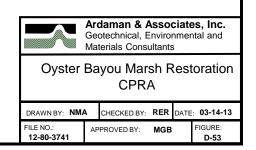


Project NameOyster BayouProject Number12-80-3741Sample NameB-07 (BL-1)Depth12-14

Description Gray CLAY (CH) w/ silt

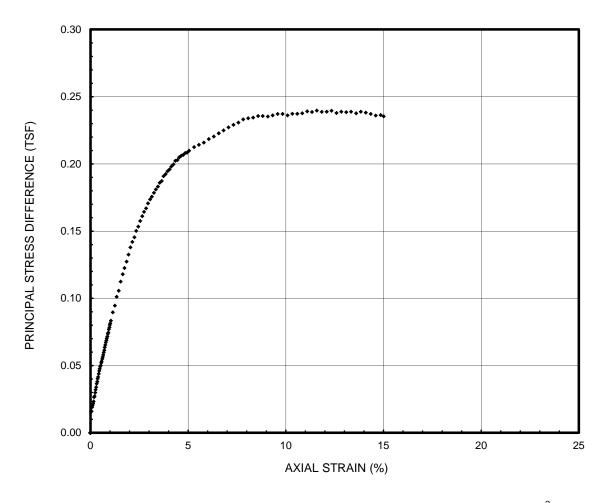


Initial Height	2.780	in	Cell Pressure	8.00	lb/in ²
Initial Diameter	1.325	in	Strain Rate	1.0	%/min
Dry Density	56.3	lb/ft ³	Peak Stress	0.263	ton/ft ²
Water Content	76.0	%	Strain at Peak Stress	3.14	%
Saturation	104	%	Failure Type	Diagonal Plane	

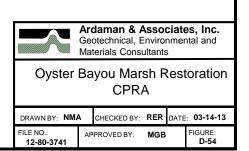


Project NameOyster BayouProject Number12-80-3741Sample NameB-07 (BL-1)Depth16-18

Description Gray CLAY (CH) w/ silt

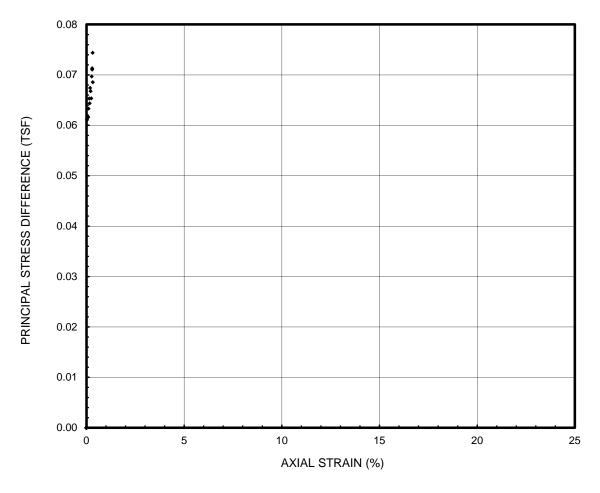


lb/in² **Cell Pressure** 7.00 **Initial Height** 5.740 in **Initial Diameter** 2.802 Strain Rate 1.0 %/min in lb/ft³ ton/ft² **Dry Density** 59.0 **Peak Stress** 0.24 **Water Content** 70.5 % **Strain at Peak Stress** 11.59 Saturation 104 % **Failure Type** Combination

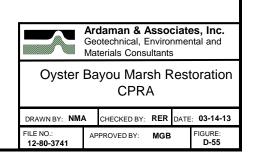


Project NameOyster BayouProject Number12-80-3741Sample NameB-07 (BL-1)Depth18-20

Description Gray CLAY (CH) w/ silt

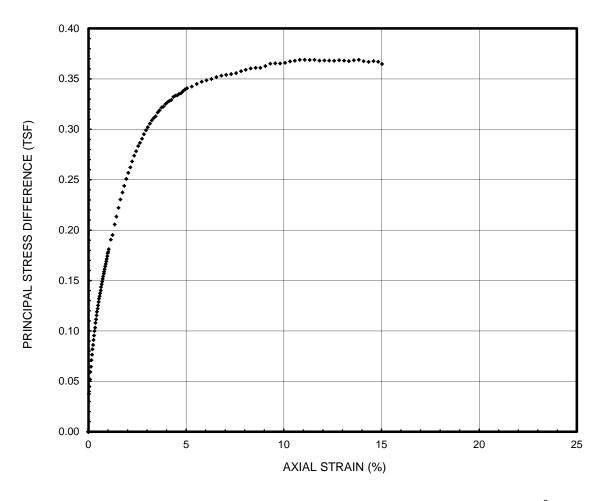


Initial Height	2.796	in	Cell Pressure	8.00	lb/in ²
Initial Diameter	1.353	in	Strain Rate	1.0	%/min
Dry Density	62.5	lb/ft ³	Peak Stress	0.074	ton/ft ²
Water Content	64.5	%	Strain at Peak Stress	0.32	%
Saturation	104	%	Failure Type	Bulging	

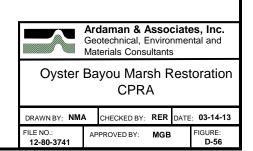


Project NameOyster BayouProject Number12-80-3741Sample NameB-07 (BL-2)Depth0-2ft

Description Gray CLAY (CH) w/ silt

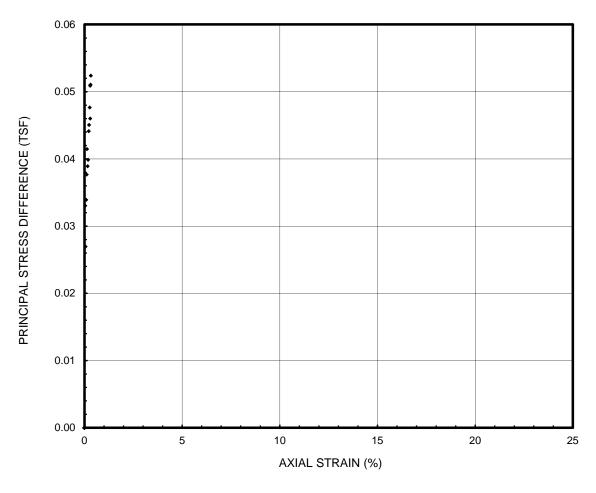


Initial Height	2.794	in	Cell Pressure	2.00	lb/in ²
Initial Diameter	1.411	in	Strain Rate	1.0	%/min
Dry Density	52.2	lb/ft ³	Peak Stress	0.369	ton/ft ²
Water Content	79.6	%	Strain at Peak Stress	11.07	%
Saturation	97	%	Failure Type	Bulging	

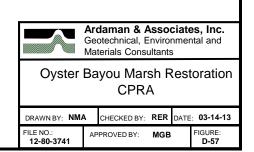


Project NameOyster BayouProject Number12-80-3741Sample NameB-07 (BL-2)Depth2-4ft

Description Gray CLAY (CH) w/ silt and shells

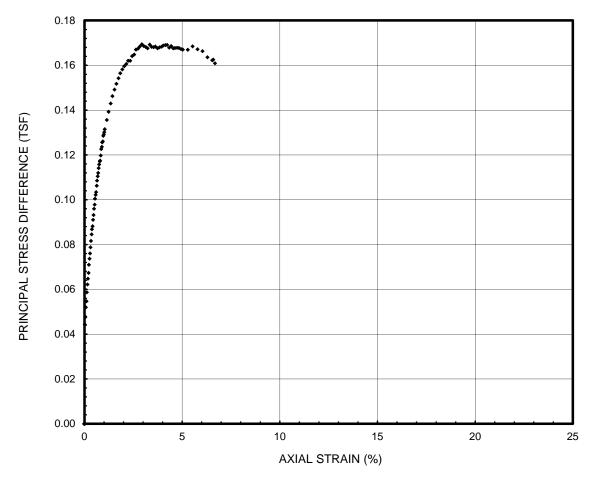


Initial Height Initial Diameter	2.777 1.389	in in	Cell Pressure Strain Rate	2.00 1.0	lb/in² %/min
Dry Density	50.0	lb/ft ³	Peak Stress	0.052	ton/ft ²
Water Content	87.7	%	Strain at Peak Stress	0.33	%
Saturation	101	%	Failure Type	Bulging	

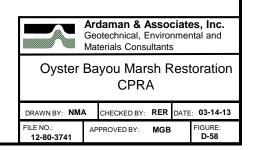


Project NameOyster BayouProject Number12-80-3741Sample NameB-07 (BL-2)Depth4-6ft

Description Gray CLAY (CH) w/ silt and shells

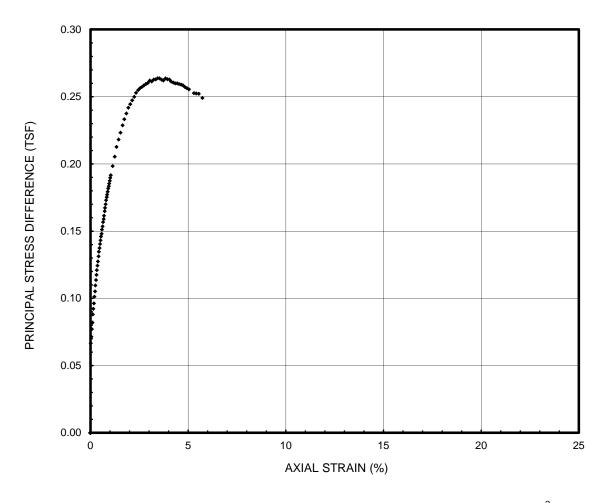


Initial Height	2.786	in	Cell Pressure	3.00	lb/in ²
Initial Diameter	1.326	in	Strain Rate	1.0	%/min
Dry Density	55.5	lb/ft ³	Peak Stress	0.169	ton/ft ²
Water Content	77.7	%	Strain at Peak Stress	2.94	
Saturation	101	%	Failure Type	Combination	

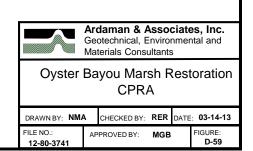


Project NameOyster BayouProject Number12-80-3741Sample NameB-07 (BL-2)Depth12-14

Description Gray CLAY (CH) w/ silt

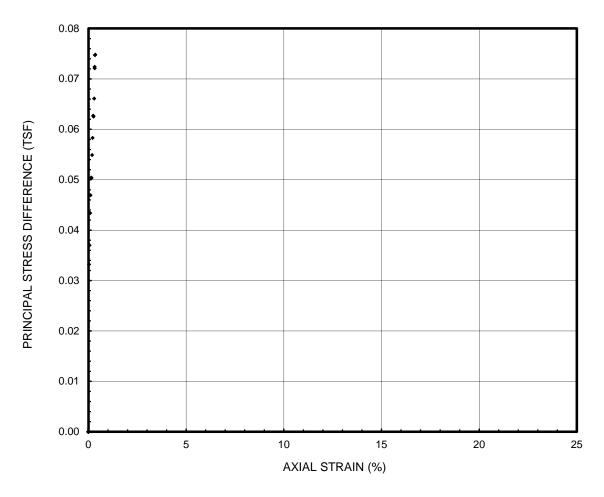


lb/in² **Cell Pressure** 14.00 **Initial Height** 2.806 in **Initial Diameter** 1.342 Strain Rate 1.0 %/min in lb/ft³ ton/ft² **Dry Density** 54.3 **Peak Stress** 0.264 **Water Content** 76.6 % **Strain at Peak Stress** 3.44 Saturation 99 % **Failure Type** Diagonal Plane

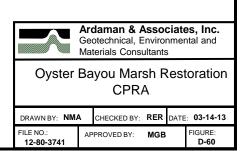


Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-07 (BL-3)
Depth 0-2 ft

Description Gray CLAY (CH) w/ silt

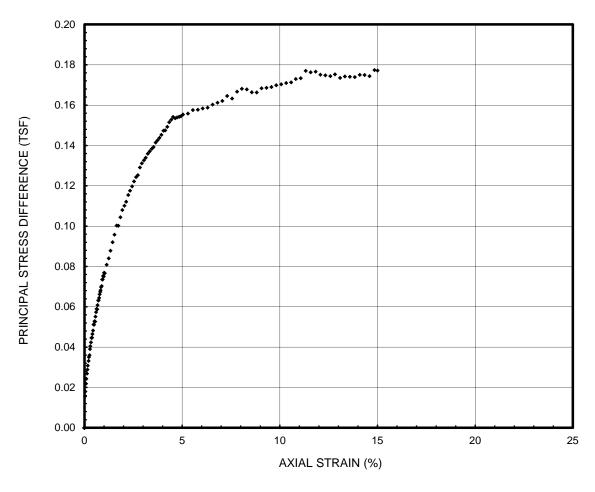


Initial Height	2.792	in	Cell Pressure	1.00	lb/in ²
Initial Diameter	1.365	ın	Strain Rate	1.0	%/min
Dry Density	52.8	lb/ft ³	Peak Stress	0.075	ton/ft ²
Water Content	82.9	%	Strain at Peak Stress	0.35	%
Saturation	103	%	Failure Type	Combination	

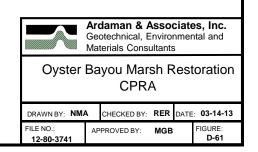


Project NameOyster BayouProject Number12-80-3741Sample NameB-07 (BL-3)Depth10-12

Description Gray CLAY (CH) w/ silt and sand layers

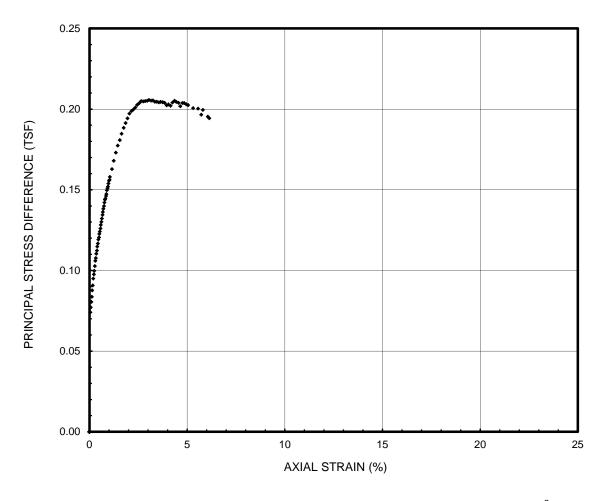


Initial Height Initial Diameter	5.728 2.768	in in	Cell Pressure Strain Rate	5.00 1.0	lb/in ² %/min
Dry Density	65.1	lb/ft ³	Peak Stress	0.177	ton/ft ²
Water Content	64.0	%	Strain at Peak Stress	14.85	%
Saturation	110	%	Failure Type	Bulging	

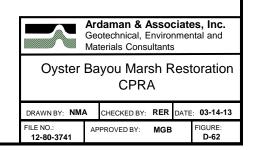


Project NameOyster BayouProject Number12-80-3741Sample NameB-07 (BL-3)Depth12-14

Description Gray CLAY (CH) w/ silt

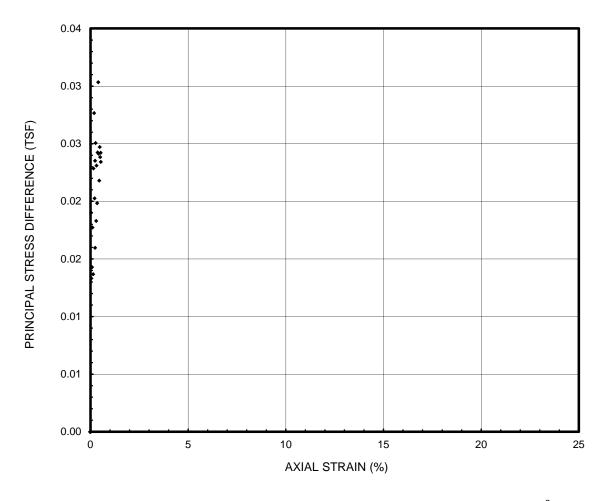


Initial Height	2.800	in	Cell Pressure	28.00	lb/in ²
Initial Diameter	1.327	in	Strain Rate	1.0	%/min
Dry Density	51.2	lb/ft ³	Peak Stress	0.206	ton/ft ²
Water Content	87.1	%	Strain at Peak Stress	3.05	%
Saturation	103	%	Failure Type	Diagonal Plane	

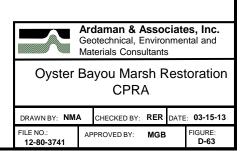


Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-08
Depth 4-6 ft

Description Gray CLAY (CH) w/ shells and sand

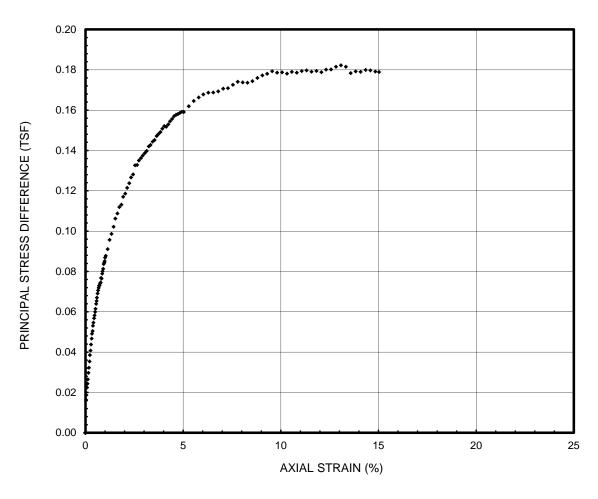


Initial Height	2.812	in	Cell Pressure	2.00	lb/in ²
Initial Diameter	1.411	in	Strain Rate	1.0	%/min
Dry Density	45.9	lb/ft ³	Peak Stress	0.030	ton/ft ²
Water Content	97.0	%	Strain at Peak Stress	0.40	%
Saturation	99	%	Failure Type	Diagonal Plane	

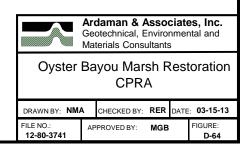


Project NameOyster BayouProject Number12-80-3741Sample NameB-08

Depth 8-10 ft **Description** Gray CLAY (CH)



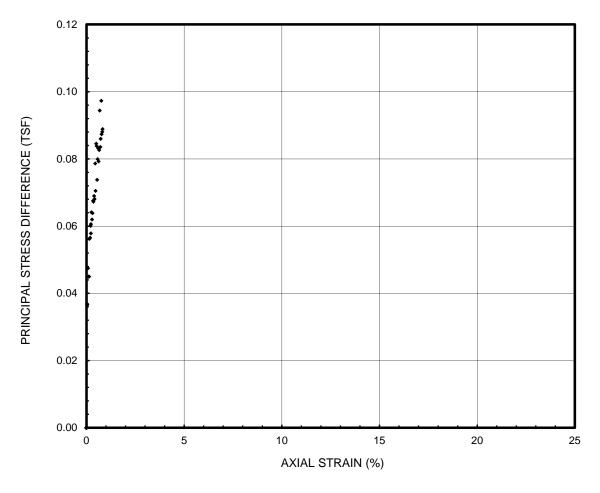
lb/in² **Cell Pressure Initial Height** 5.756 4.00 in **Initial Diameter** 2.785 Strain Rate 1.0 %/min in lb/ft³ ton/ft² **Dry Density** 57.3 **Peak Stress** 0.182 **Water Content** 76.6 % **Strain at Peak Stress** 13.08 Saturation 107 % **Failure Type** Combination



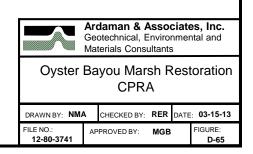
Project NameOyster BayouProject Number12-80-3741Sample NameB-08

Depth 12-14 ft

Description Gray CLAY (CH) with silt pockets



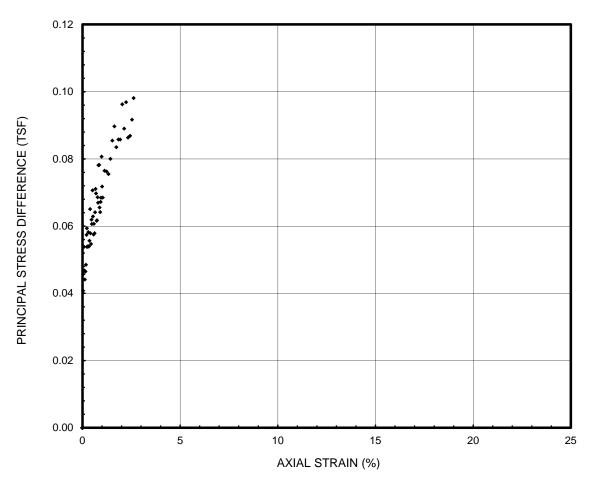
Initial Height Initial Diameter	2.788 1.350	in in	Cell Pressure Strain Rate	6.00 1.0	lb/in ² %/min
Dry Density	71.5	lb/ft ³	Peak Stress	0.097	ton/ft ²
Water Content	52.4	%	Strain at Peak Stress	0.76	%
Saturation	106	%	Failure Type	Other	



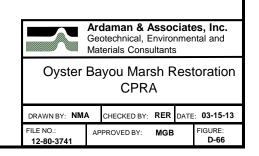
Project NameOyster BayouProject Number12-80-3741Sample NameB-08

Depth 16-18 ft

Description Gray CLAY (CH) with shells



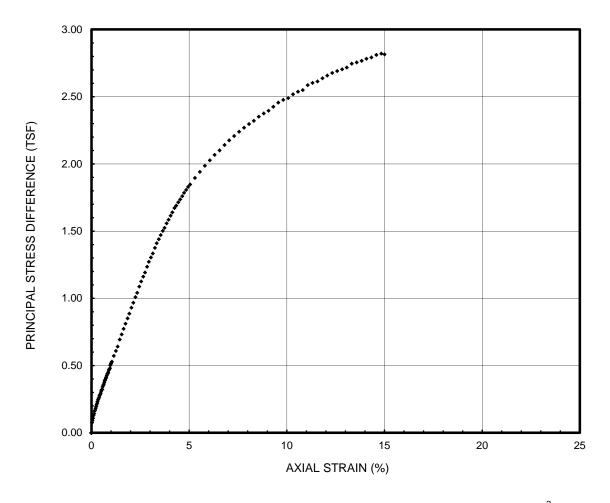
Initial Height Initial Diameter	2.802 1.401	in in	Cell Pressure Strain Rate	7.00 1.0	lb/in² %/min
Dry Density	55.7	lb/ft ³	Peak Stress	0.098	ton/ft ²
Water Content	75.8	%	Strain at Peak Stress	2.62	%
Saturation	102	%	Failure Type	Diagonal Plane	



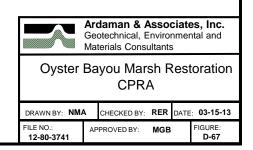
Project NameOyster BayouProject Number12-80-3741Sample NameB-08

Depth 38-40 ft

Description Gray CLAYEY SAND (SC)

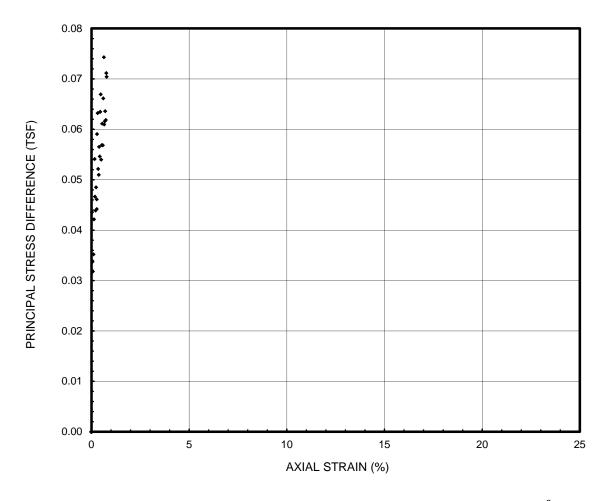


Initial Height	2.791	in	Cell Pressure	16.00	lb/in ²
Initial Diameter	1.405	in	Strain Rate	1.0	%/min
Dry Density	112.1	lb/ft ³	Peak Stress	2.821	ton/ft ²
Water Content	18.9	%	Strain at Peak Stress	14.83	%
Saturation	106	%	Failure Type	Combination	

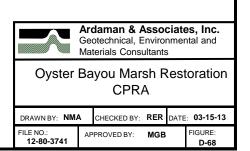


Project NameOyster BayouProject Number12-80-3741Sample NameB-08 (BL-1)Depth18-20

Description Gray CLAY (CH) with shells

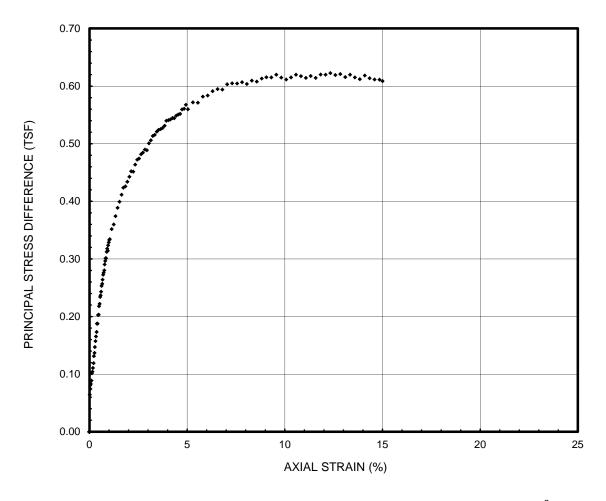


Initial Height	2.808	in	Cell Pressure	8.00	lb/in ²
Initial Diameter	1.379	in	Strain Rate	1.0	%/min
Dry Density	53.5	lb/ft ³	Peak Stress	0.074	ton/ft ²
Water Content	81.6	%	Strain at Peak Stress	0.63	%
Saturation	103	%	Failure Type	Combination	

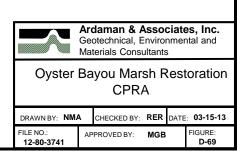


Project NameOyster BayouProject Number12-80-3741Sample NameB-08 (BL-1)Depth28-30

Description Gray and tan SILTY CLAY (CL)

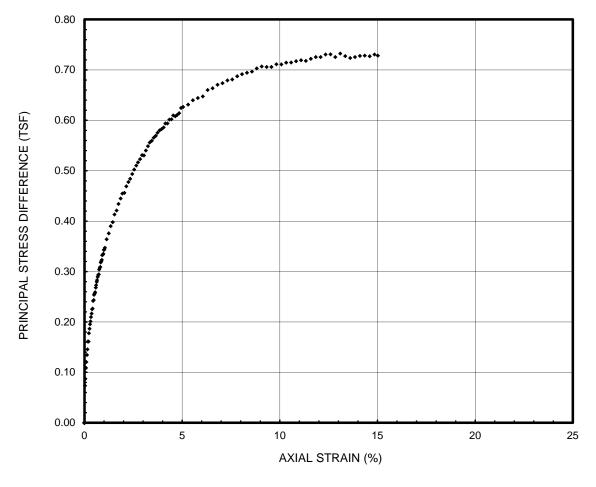


lb/in² **Cell Pressure Initial Height** 2.789 12.00 in **Initial Diameter** 1.380 Strain Rate 1.0 %/min in lb/ft³ ton/ft² **Dry Density** 102.1 **Peak Stress** 0.623 **Water Content** 24.9 % **Strain at Peak Stress** 12.34 Saturation 106 % **Failure Type** Combination

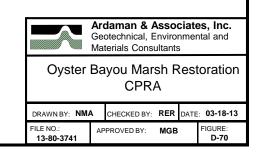


Project NameOyster BayouProject Number12-80-3741Sample NameB-08 (BL-2)Depth23-25ft

Description Gray and tan SILTY CLAY (CL)



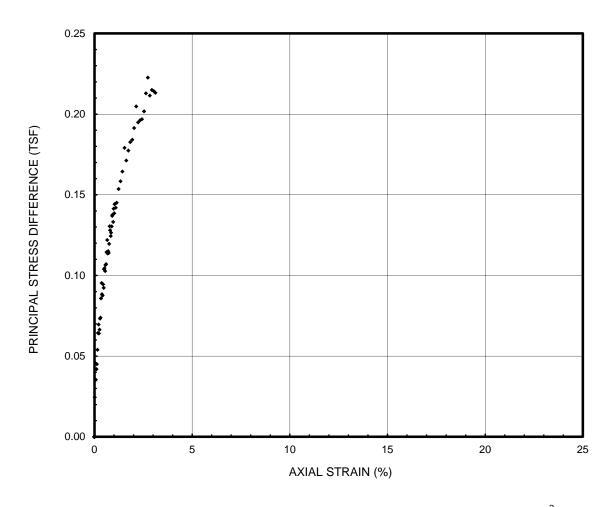
Initial Height Initial Diameter	2.795 1.377	in in	Cell Pressure Strain Rate	10.00 1.0	lb/in ² %/min
Dry Density	98.6	lb/ft ³	Peak Stress	0.732	ton/ft ²
Water Content	27.2	%	Strain at Peak Stress	13.09	%
Saturation	107	%	Failure Type	Bulging	



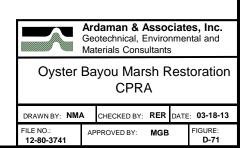
Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-09

Depth 0-2 ft

Description Gray CLAY (CH) w/ silt



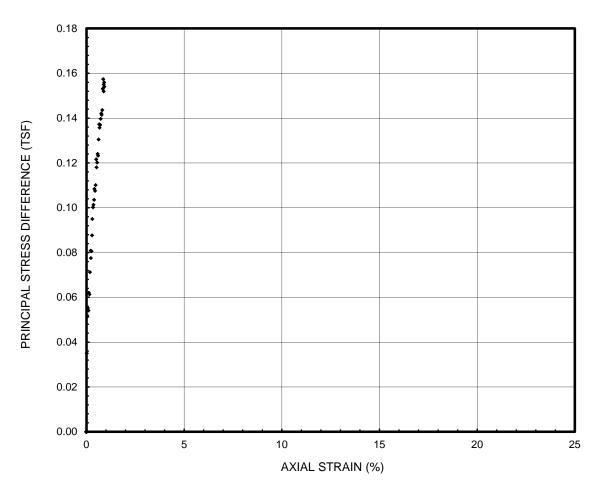
lb/in² **Cell Pressure Initial Height** 2.798 1.00 in **Initial Diameter** 1.401 Strain Rate 1.0 %/min in lb/ft³ ton/ft² **Dry Density** 60.6 **Peak Stress** 0.223 **Water Content** 65.4 % **Strain at Peak Stress** 2.74 Saturation 100 % **Failure Type** Combination



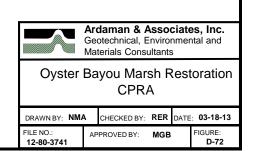
Project NameOyster BayouProject Number12-80-3741Sample NameB-09

Depth 2-4 ft

Description Gray CLAY (CH) w/ silt

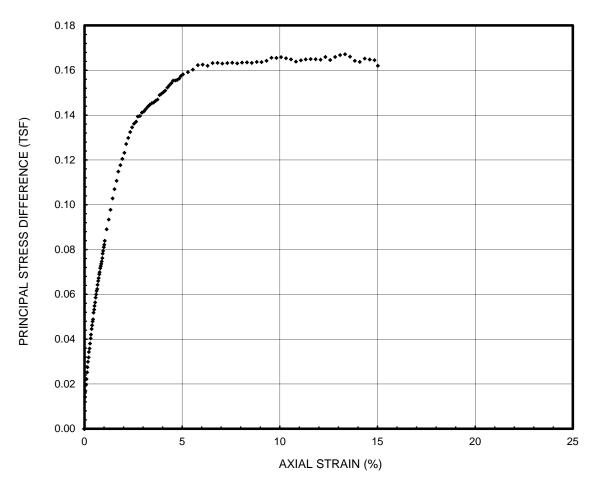


Initial Height Initial Diameter	2.793 1.350	in in	Cell Pressure Strain Rate	2.00 1.0	lb/in² %/min
Dry Density	51.1	lb/ft ³	Peak Stress	0.157	ton/ft ²
Water Content	87.3	%	Strain at Peak Stress	0.86	%
Saturation	103	%	Failure Type	Bulging	

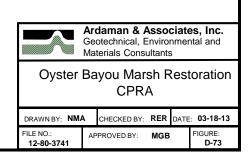


Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-09
Depth 6-8 ft

Description Gray CLAY (CH) w/ silt and shells

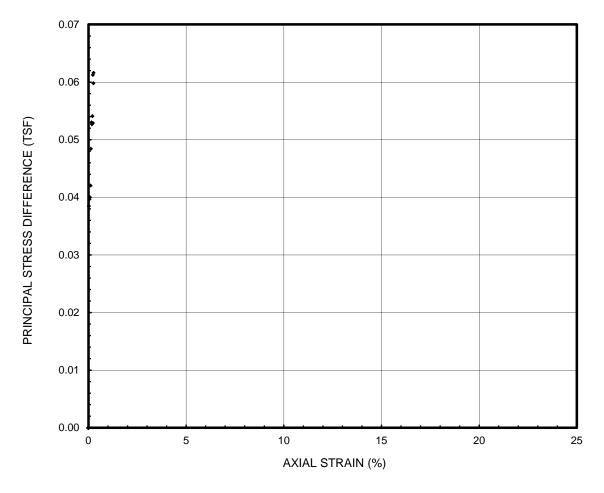


Initial Height	5.808	in	Cell Pressure	3.00	lb/in ²
Initial Diameter	2.809	in	Strain Rate	1.0	%/min
Dry Density	55.5	lb/ft ³	Peak Stress	0.167	ton/ft ²
Water Content	76.9	%	Strain at Peak Stress	13.34	%
Saturation	103	%	Failure Type	Other	

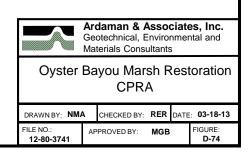


Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-09
Depth 10-12 ft

Description Gray CLAY (CH) w/ silt and shells



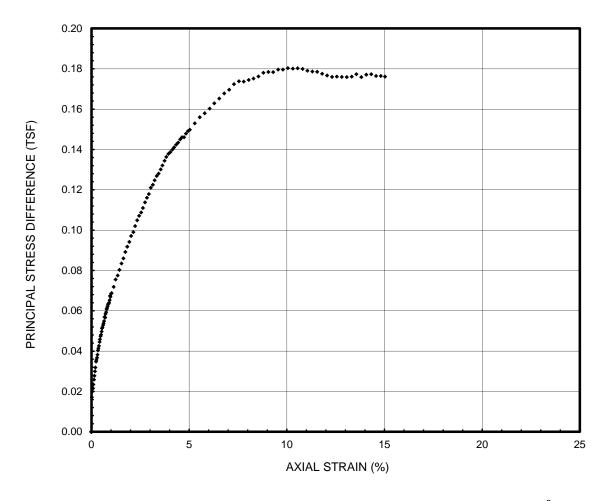
Initial Height Initial Diameter	2.805 1.351	in in	Cell Pressure Strain Rate	5.00 1.0	lb/in ² %/min
Dry Density Water Content	53.5 80.1	lb/ft ³	Peak Stress Strain at Peak Stress	0.062 0.26	ton/ft ²
Saturation	101	%	Failure Type	Bulging	,,



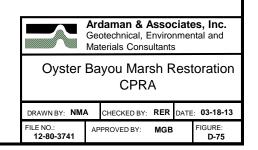
Project NameOyster BayouProject Number12-80-3741Sample NameB-09

Depth 14-16 ft

Description Gray CLAY (CH) w/ silt

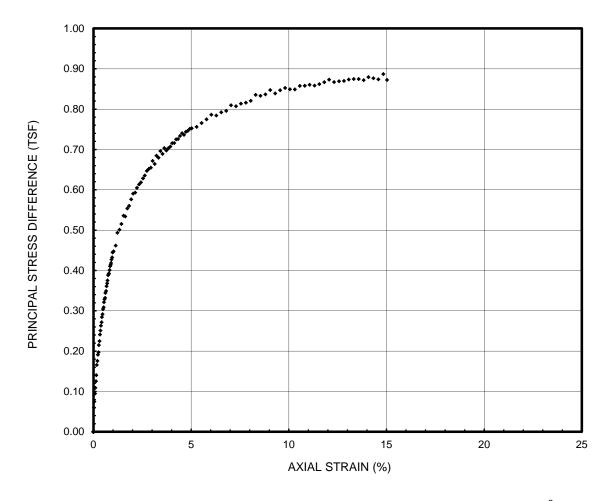


Initial Height	5.804	in	Cell Pressure	6.00	lb/in ²
Initial Diameter	2.802	in	Strain Rate	1.0	%/min
Dry Density	53.7	lb/ft ³	Peak Stress	0.180	ton/ft ²
Water Content	82.1	%	Strain at Peak Stress	10.05	%
Saturation	105	%	Failure Type	Combination	

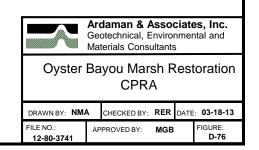


Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-09
Depth 18-20 ft

Description Gray SILTY CLAY (CL) w/ sand

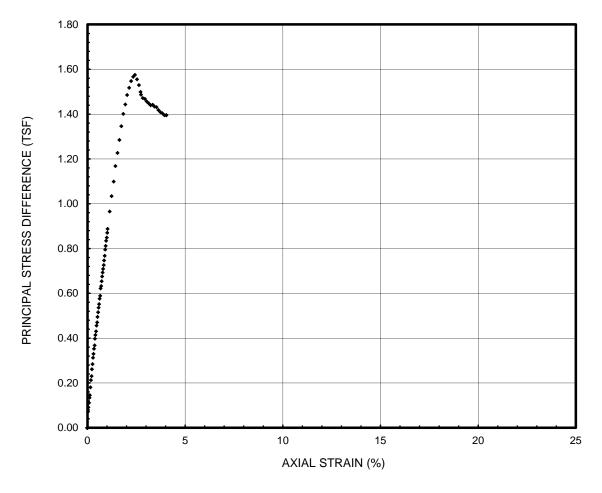


Initial Height	2.791	in	Cell Pressure	8.00	lb/in ²
Initial Diameter	1.403	in	Strain Rate	1.0	%/min
Dry Density	103.8	lb/ft ³	Peak Stress	0.887	ton/ft ²
Water Content	22.9	%	Strain at Peak Stress	14.84	%
Saturation	102	%	Failure Type	Combination	

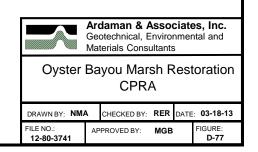


Project NameOyster BayouProject Number12-80-3741Sample NameB-09 (BL-1)Depth33-35ft

Description Tan and gray SILTY CLAY (CL)

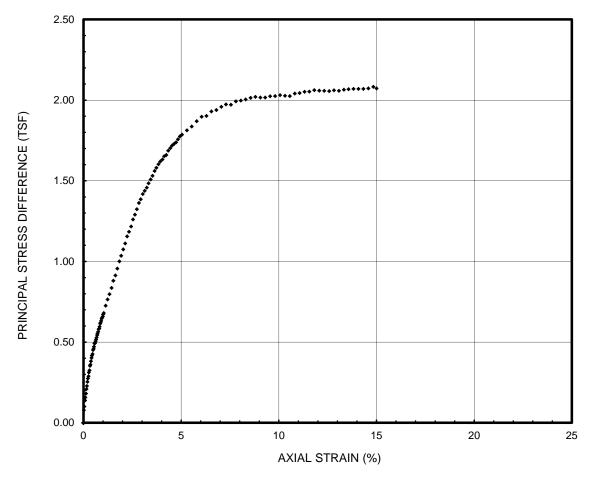


Initial Height Initial Diameter	2.807 1.408	in in	Cell Pressure Strain Rate	14.00 1.0	lb/in ² %/min
Dry Density	85.3	lb/ft ³	Peak Stress	1.575	ton/ft ²
Water Content	35.6	%	Strain at Peak Stress	2.43	%
Saturation	101	%	Failure Type	Combination	

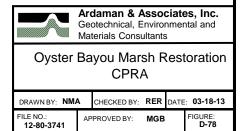


Project NameOyster BayouProject Number12-80-3741Sample NameB-09 (BL-2)Depth23-25

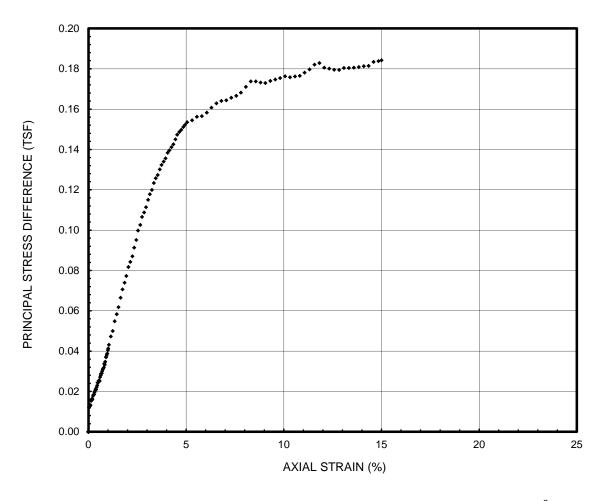
Description Tan and gray SILTY CLAY (CL)



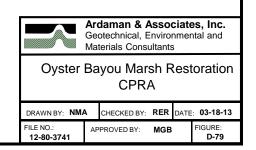
Cell Pressure Strain Rate Peak Stress Strain at Peak Stress Failure Type 10.00 lb/in²
1.0 %/min
2.083 ton/ft²
14.83 %
Combination



Project Name
Oyster Bayou
12-80-3741
Sample Name
Depth
Description
Oyster Bayou
12-80-3741
B-10
Gray CLAY (CH)

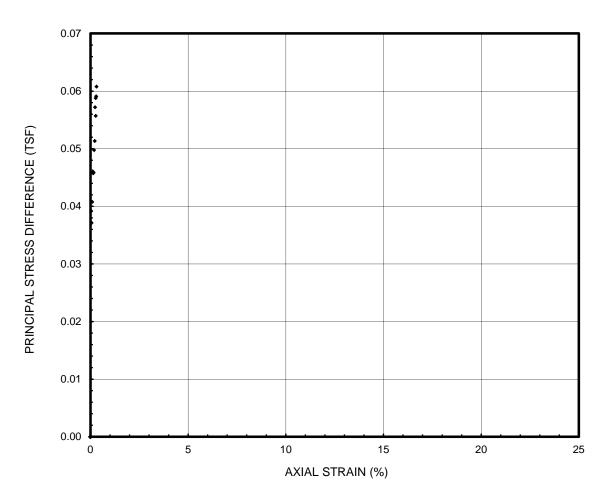


lb/in² **Cell Pressure Initial Height** 5.710 2.00 in **Initial Diameter** 2.806 Strain Rate 1.0 %/min in lb/ft³ ton/ft² **Dry Density** 53.9 **Peak Stress** 0.184 **Water Content** 84.7 % **Strain at Peak Stress** 15.00 % Saturation 109 % **Failure Type** Bulging

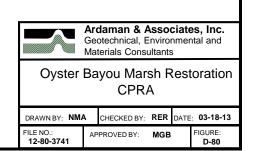


Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-10
Depth 4-6 ft

Description Gray CLAY (CH) w/ shells

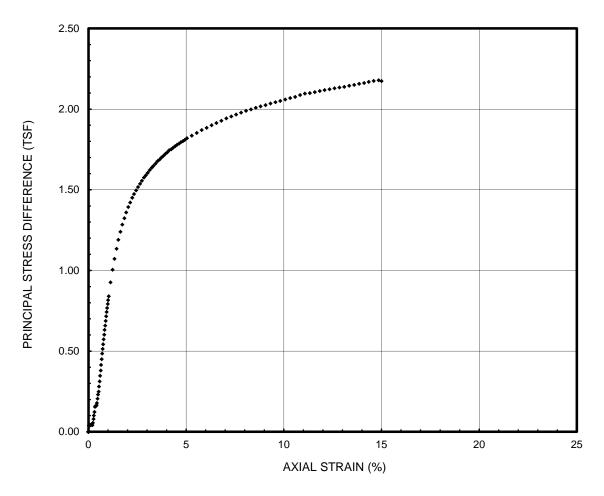


Initial Height	2.803	in	Cell Pressure	2.00	lb/in ²
Initial Diameter	1.356	in	Strain Rate	1.0	%/min
Dry Density	56.4	lb/ft ³	Peak Stress	0.061	ton/ft ²
Water Content	74.6	%	Strain at Peak Stress	0.31	%
Saturation	102	%	Failure Type	Bulging	

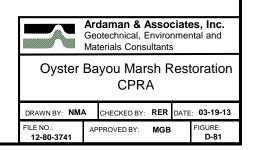


Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-10
Depth 33-35 ft

Description Tan and gray CLAY (CH) w/ sand

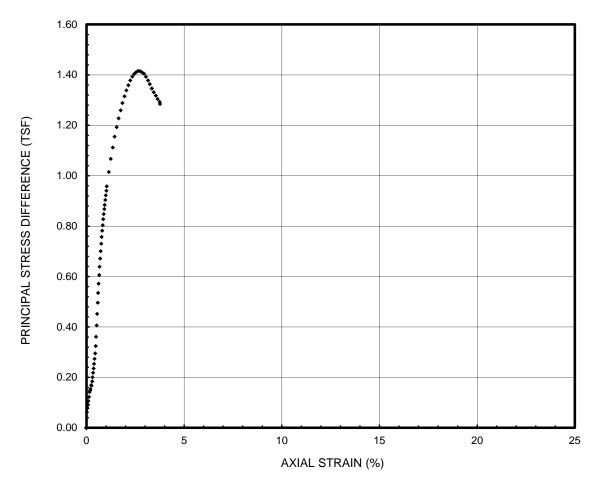


Initial Height Initial Diameter	5.746 2.857	in in	Cell Pressure Strain Rate	14.00 1.0	lb/in² %/min
Dry Density	106.0	lb/ft ³	Peak Stress	2.178	ton/ft ²
Water Content	21.4	%	Strain at Peak Stress	14.86	%
Saturation	101	%	Failure Type	Bulging	

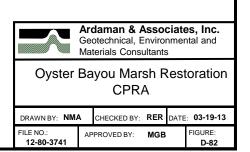


Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-10
Depth 53-55 ft

Description Brown and gray CLAY (CH) w/ silt layers

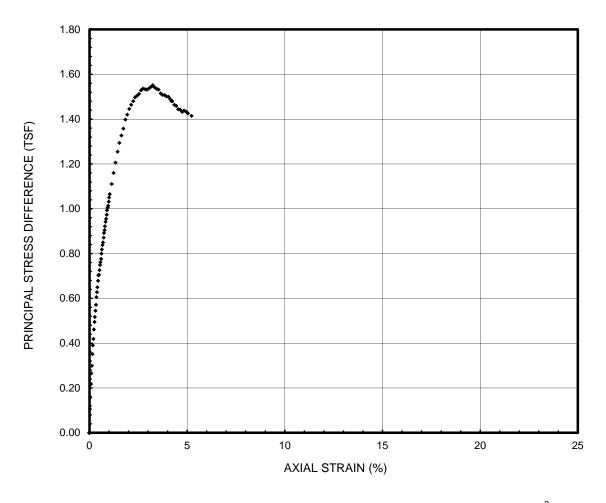


Initial Height Initial Diameter	5.772 2.847	in in	Cell Pressure Strain Rate	22.00 1.0	lb/in² %/min
Dry Density	71.1	lb/ft ³	Peak Stress	1.415	ton/ft ²
Water Content	49.7	%	Strain at Peak Stress	2.64	%
Saturation	99	%	Failure Type	Diagonal Plane	

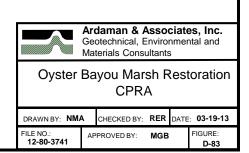


Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-10
Depth 58-60 ff

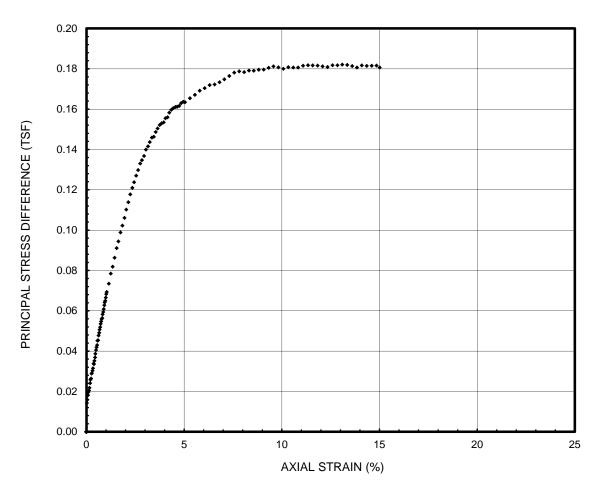
Description Brown and gray CLAY (CH) w/ silt layers



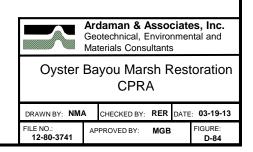
Initial Height	2.816	in	Cell Pressure	24.00	lb/in ²
Initial Diameter	1.379	in	Strain Rate	1.0	%/min
Dry Density	83.6	lb/ft ³	Peak Stress	1.551	ton/ft ²
Water Content	36.4	%	Strain at Peak Stress	3.24	%
Saturation	98	%	Failure Type	Bulging	



Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-10 (BL-1)
Depth 8-10 ft
Description Gray CLAY (CH)

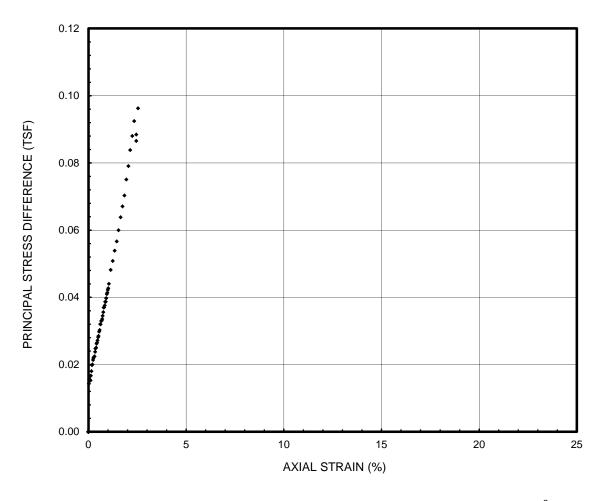


Initial Height Initial Diameter	5.740 2.807	in in	Cell Pressure Strain Rate	4.00 1.0	lb/in² %/min
Dry Density	51.9	lb/ft ³	Peak Stress	0.182	ton/ft ²
Water Content	86.4	%	Strain at Peak Stress	13.10	%
Saturation	105	%	Failure Type	Bulging	

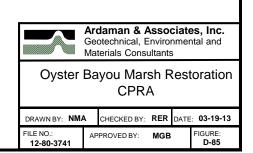


Project NameOyster BayouProject Number12-80-3741Sample NameB-10 (BL-1)Depth16-18

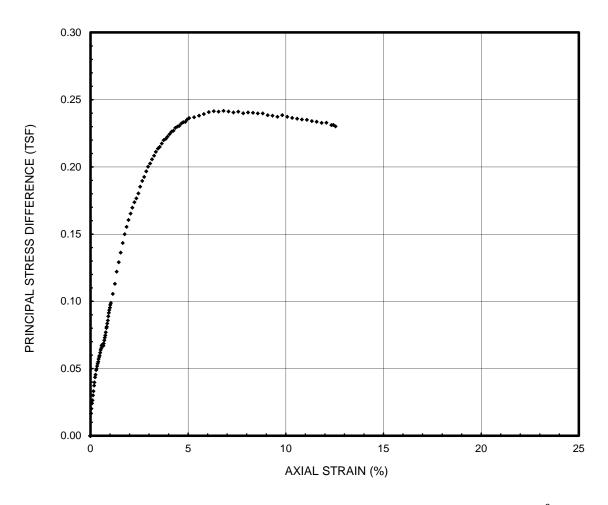
Description Gray CLAY (CH) w/ silt



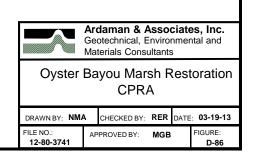
Initial Height	5.693	in	Cell Pressure	7.00	lb/in ²
Initial Diameter	2.778	in	Strain Rate	1.0	%/min
Dry Density	100.3	lb/ft ³	Peak Stress	0.096	ton/ft ²
Water Content	27.1	%	Strain at Peak Stress	2.54	%
Saturation	110	%	Failure Type	Bulging	



Project NameOyster BayouProject Number12-80-3741Sample NameB-10 (BL-2)Depth14-16 ftDescriptionGray CLAY (CH)

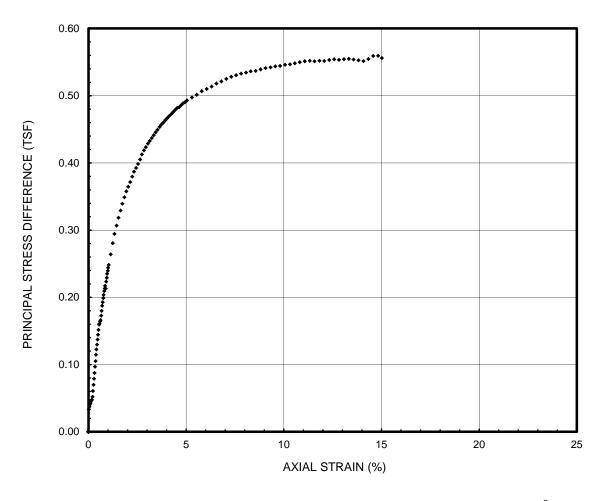


Initial Height	5.734	in	Cell Pressure	6.00	lb/in ²
Initial Diameter	2.794	in	Strain Rate	1.0	%/min
Dry Density	51.1	lb/ft ³	Peak Stress	0.242	ton/ft ²
Water Content	89.0	%	Strain at Peak Stress	6.81	%
Saturation	105	%	Failure Type	Bulging	

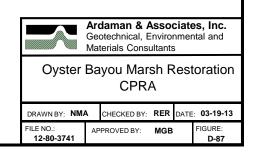


Project NameOyster BayouProject Number12-80-3741Sample NameB-10 (BL-2)Depth23-25

Description Gray SILTY CLAY (CL)



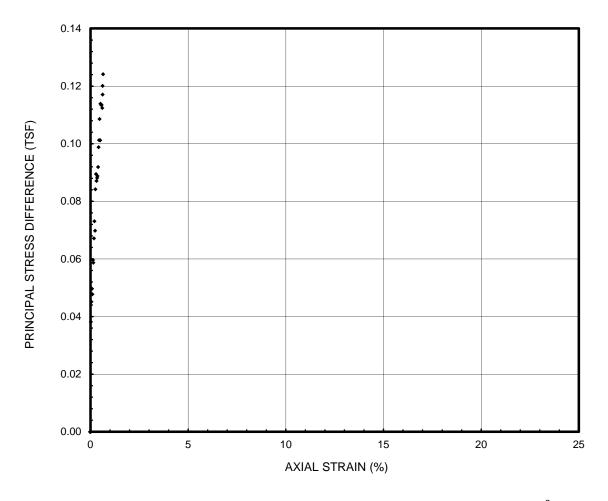
Initial Height	5.732	in	Cell Pressure	10.00	lb/in ²
Initial Diameter	2.829	in	Strain Rate	1.0	%/min
Dry Density	96.3	lb/ft ³	Peak Stress	0.559	ton/ft ²
Water Content	29.2	%	Strain at Peak Stress	14.83	%
Saturation	108	%	Failure Type	Bulging	



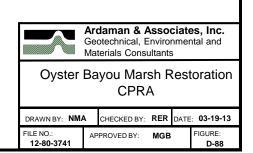
Project NameOyster BayouProject Number12-80-3741Sample NameB-11

Depth 6-8 ft

Description Gray CLAY (CH) w/ silt and sand layers



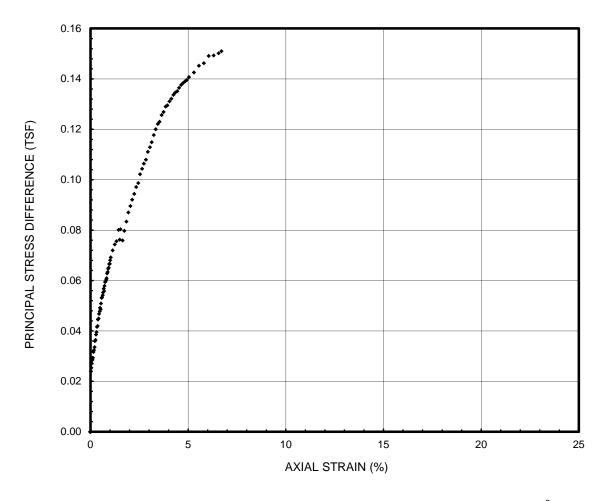
Initial Height	2.805	in	Cell Pressure	3.00	lb/in ²
Initial Diameter	1.342	in	Strain Rate	1.0	%/min
Dry Density	50.3	lb/ft ³	Peak Stress	0.124	ton/ft ²
Water Content	87.3	%	Strain at Peak Stress	0.64	%
Saturation	101	%	Failure Type	Bulging	



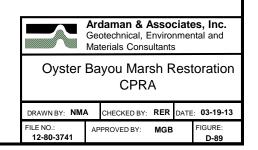
Project NameOyster BayouProject Number13-80-3741Sample NameB-11

Depth 10-12 ft

Description Gray CLAY (CH) w/ silt and sand layers



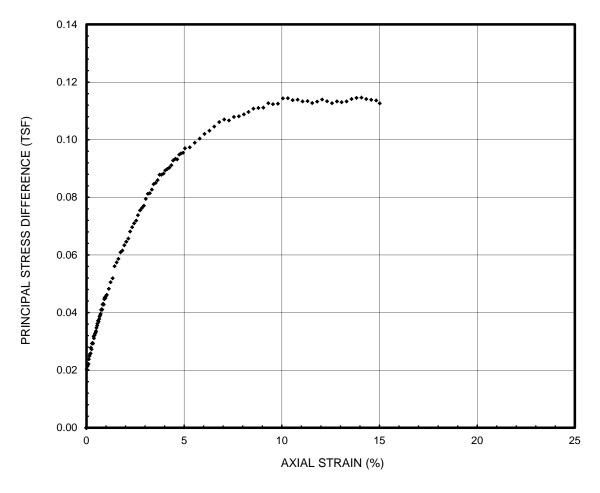
Initial Height	5.790	in	Cell Pressure	5.00	lb/in ²
Initial Diameter	2.811	in	Strain Rate	1.0	%/min
Dry Density	53.6	lb/ft ³	Peak Stress	0.151	ton/ft ²
Water Content	82.1	%	Strain at Peak Strain	6.70	%
Saturation	104	%	Failure Type	Diagonal Plane	



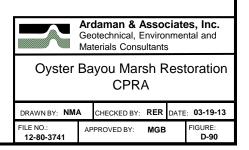
Project Name
Oyster Bayou
12-80-3741
Sample Name
B-11

Depth 14-16 ft

Description Gray CLAY (CH) w/ silt and sand layers



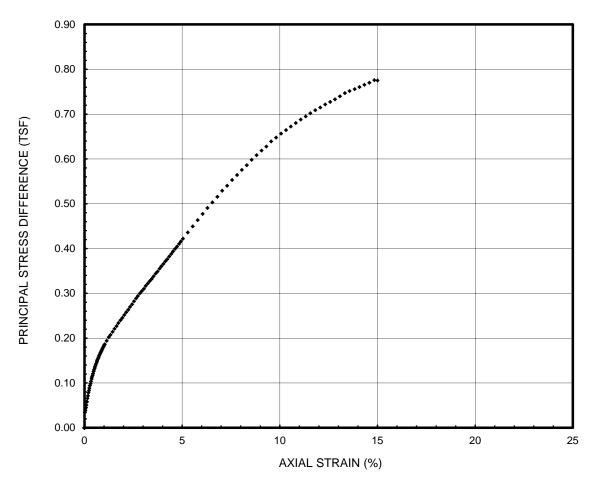
lb/in² **Cell Pressure Initial Height** 6.00 5.778 in **Initial Diameter** 2.775 Strain Rate 1.0 %/min in lb/ft³ ton/ft² **Dry Density** 60.0 **Peak Stress** 0.115 **Water Content** 71.4 % **Strain at Peak Stress** 14.07 Saturation 108 % **Failure Type** Combination



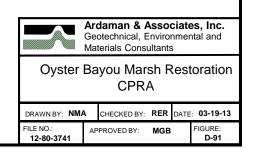
Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-11

Depth 18-20 ft

Description Gray SILTY CLAY (CL) w/ sand



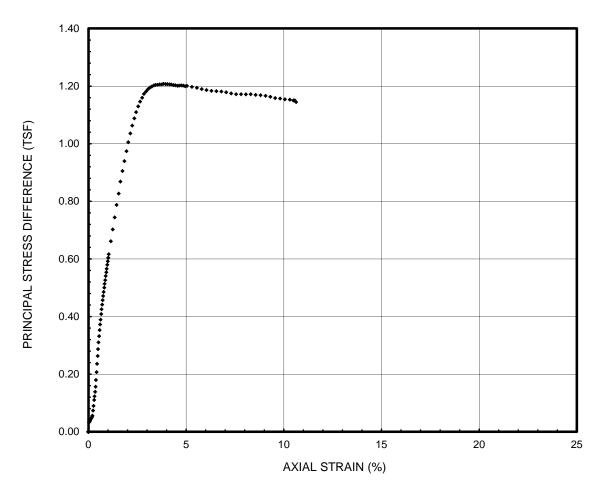
Initial Height Initial Diameter	5.809 2.798	in in	Cell Pressure Strain Rate	8.00 1.0	lb/in ² %/min
Dry Density	107.0	lb/ft ³	Peak Stress	0.776	ton/ft ²
Water Content	22.5	%	Strain at Peak Stress	14.84	%
Saturation	109	%	Failure Type	Bulging	



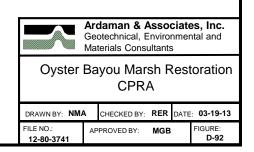
Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-11

Depth 38-40 ft

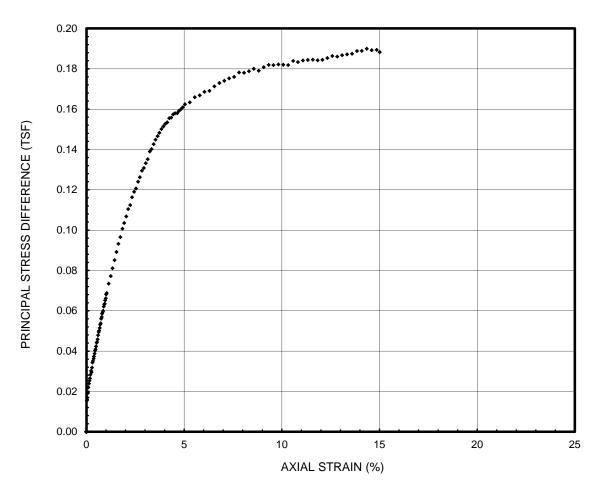
Description Gray SILTY CLAY (CL)



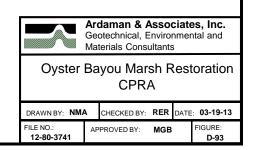
Initial Height Initial Diameter	5.809 2.852	in in	Cell Pressure Strain Rate	16.00 1.0	lb/in² %/min
Dry Density	84.7	lb/ft ³	Peak Stress	1.208	ton/ft ²
Water Content	38.3	%	Strain at Peak Stress	3.84	%
Saturation	106	%	Failure Type	Combination	



Project Name
Oyster Bayou
12-80-3741
Sample Name
Depth
Description
Oyster Bayou
12-80-3741
B-12
C-4
ft
Gray CLAY (CH)

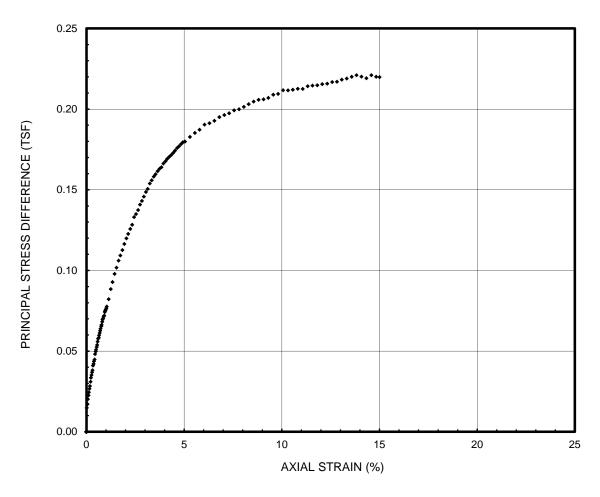


lb/in² **Cell Pressure Initial Height** 5.789 2.00 in **Initial Diameter** 2.786 Strain Rate 1.0 %/min in lb/ft³ ton/ft² **Dry Density** 54.0 **Peak Stress** 0.190 **Water Content** 85.0 % **Strain at Peak Stress** 14.35 Saturation 109 % **Failure Type** Combination

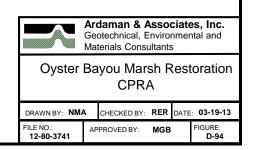


Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-12
Depth 6-8 ft

Depth 6-8 ft **Description** Gray CLAY (CH)

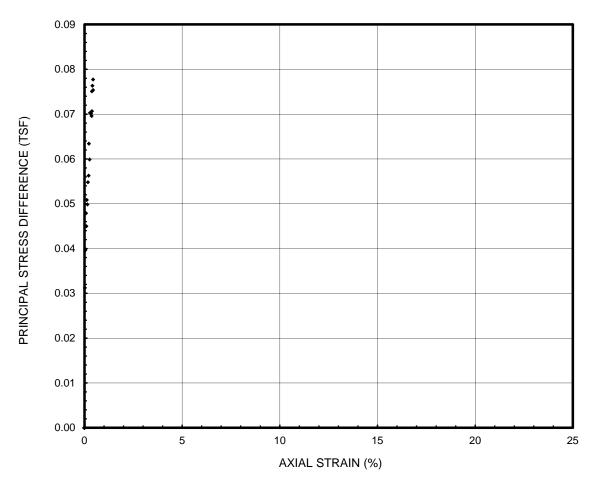


lb/in² **Cell Pressure Initial Height** 5.802 3.00 in **Initial Diameter** 2.792 Strain Rate 1.0 %/min in lb/ft³ ton/ft² **Dry Density** 57.7 **Peak Stress** 0.221 **Water Content** 74.9 % **Strain at Peak Stress** 13.83 Saturation 106 % **Failure Type** Combination

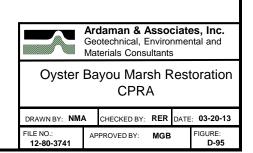


Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-12

 $\begin{array}{lll} \textbf{Depth} & & 8 \text{-} 10 & \text{ft} \\ \textbf{Description} & & \text{Gray CLAY (CH)} \\ \end{array}$

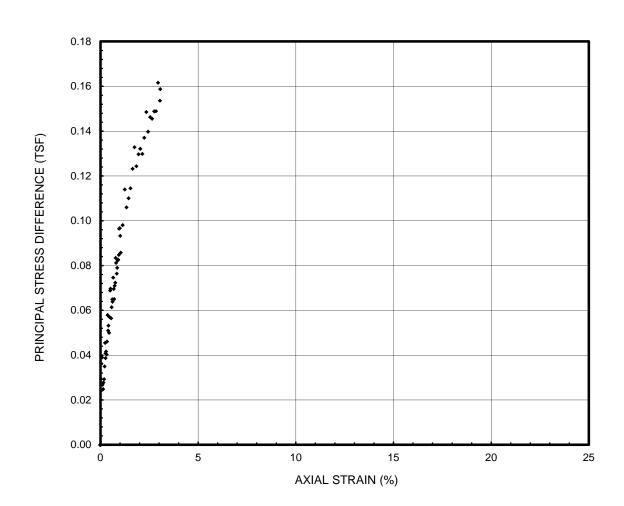


Initial Height Initial Diameter	2.795 1.344	in in	Cell Pressure Strain Rate	4.00 1.0	lb/in² %/min
Dry Density	50.8	lb/ft ³	Peak Stress	0.078	ton/ft ²
Water Content	85.3	%	Strain at Peak Stress	0.44	%
Saturation	100	%	Failure Type	Bulging	

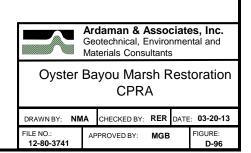


Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-12
Depth 12-14 ft

Description Gray CLAY (CH) w/ sand layers

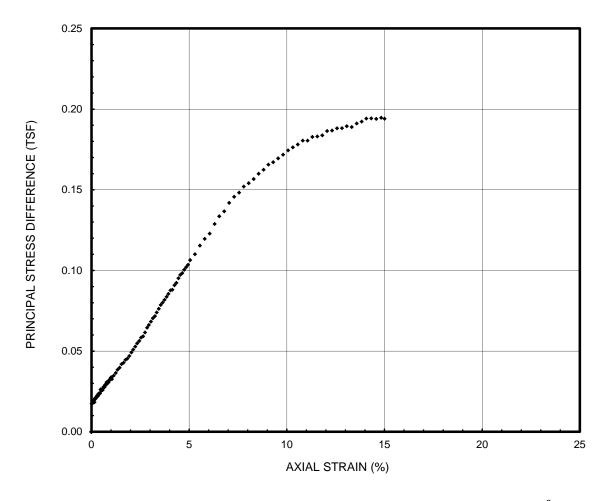


Initial Height	2.806	in	Cell Pressure	6.00	lb/in ²
Initial Diameter	1.348	in	Strain Rate	1.0	%/min
Dry Density	57.4	lb/ft ³	Peak Stress	0.162	ton/ft ²
Water Content	74.9	%	Strain at Peak Stress	2.95	%
Saturation	105	%	Failure Type	Other	

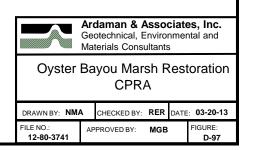


Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-12
Depth 14-16 ft

Description Tan and gray SILTY CLAY (CL)

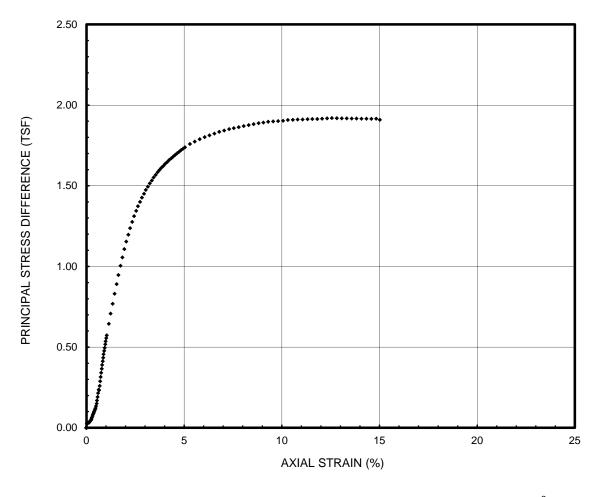


Initial Height	5.704	in	Cell Pressure	6.00	lb/in ²
Initial Diameter	2.804	in	Strain Rate	1.0	%/min
Dry Density	88.7	lb/ft ³	Peak Stress	0.195	ton/ft ²
Water Content	35.9	%	Strain at Peak Stress	14.83	%
Saturation	110	%	Failure Type	Combination	

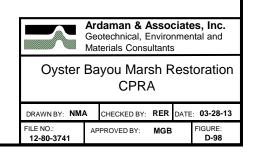


Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-12
Depth 18-20 ft

Description Tan and gray CLAY (CH) w/ silty sand layers

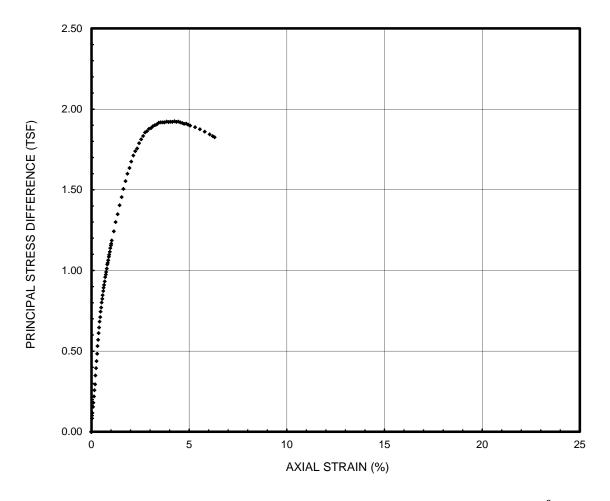


Initial Height	5.624	in	Cell Pressure	8.00	lb/in ²
Initial Diameter	2.855	in	Strain Rate	1.0	%/min
Dry Density	106.5	lb/ft ³	Peak Stress	1.920	ton/ft ²
Water Content	21.7	%	Strain at Peak Stress	12.57	%
Saturation	104	%	Failure Type	Bulging	

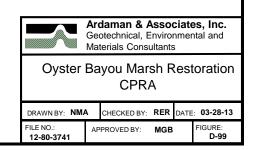


Project NameOyster BayouProject Number12-80-3741Sample NameB-12 (BL-1)Depth43-45ft

Description Tan and gray CLAY (CH) w/ silt layers

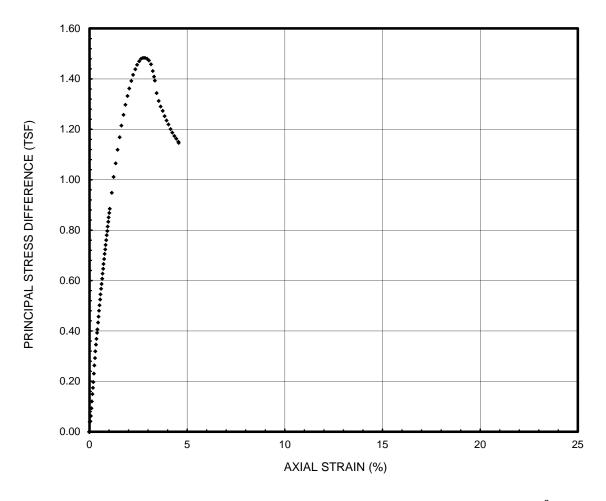


Initial Height	2.804	in	Cell Pressure	18.00	lb/in ²
Initial Diameter	1.401	in	Strain Rate	1.0	%/min
Dry Density	89.8	lb/ft ³	Peak Stress	1.924	ton/ft ²
Water Content	32.5	%	Strain at Peak Stress	4.25	%
Saturation	102	%	Failure Type	Combination	

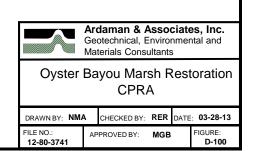


Project NameOyster BayouProject Number12-80-3741Sample NameB-12 (BL-1)Depth48-50

Description Tan and gray CLAY (CH) w/ silt layers

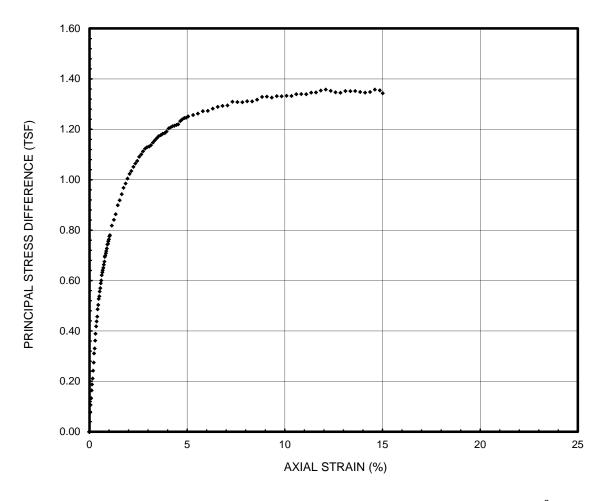


Initial Height	5.603	in	Cell Pressure	20.00	lb/in ²
Initial Diameter	2.854	in	Strain Rate	1.0	%/min
Dry Density	77.0	lb/ft ³	Peak Stress	1.483	ton/ft ²
Water Content	45.1	%	Strain at Peak Stress	2.75	%
Saturation	104	%	Failure Type	Diagonal Plane	

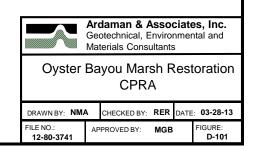


Project NameOyster BayouProject Number12-80-3741Sample NameB-12 (BL-2)Depth28-30

Description Tan and gray SILTY CLAY (CL)

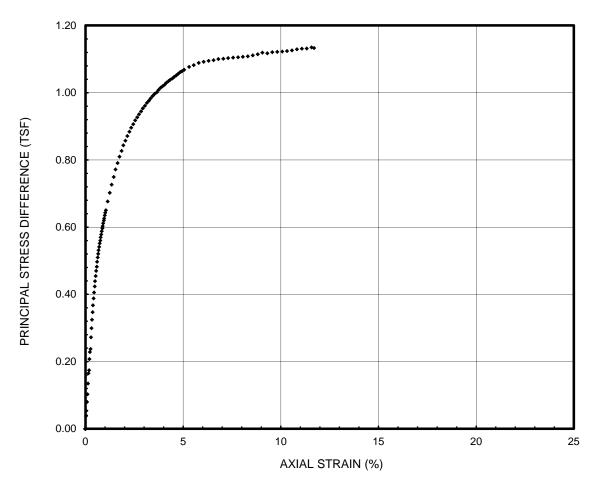


Initial Height	2.791	in	Cell Pressure	12.00	lb/in ²
Initial Diameter	1.369	in	Strain Rate	1.0	%/min
Dry Density	100.3	lb/ft ³	Peak Stress	1.358	ton/ft ²
Water Content	25.7	%	Strain at Peak Stress	12.09	%
Saturation	105	%	Failure Type	Bulging	

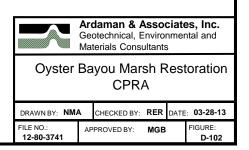


Project NameOyster BayouProject Number12-80-3741Sample NameB-12 (BL-2)Depth38-40ft

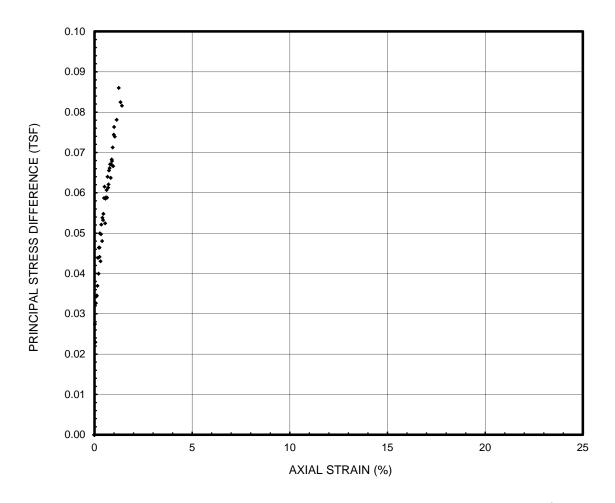
Description Tan and gray CLAY (CH) w/ silt layers



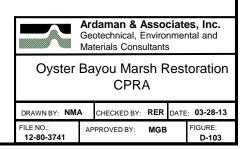
lb/in² **Cell Pressure Initial Height** 5.619 16.00 in **Initial Diameter** 2.864 Strain Rate 1.0 %/min in lb/ft³ ton/ft² **Dry Density** 80.5 **Peak Stress** 1.135 **Water Content** 39.9 % **Strain at Peak Stress** 11.57 Saturation 100 % **Failure Type** Combination



Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-13
Depth 2-4 ft
Description Gray CLAY (CH)

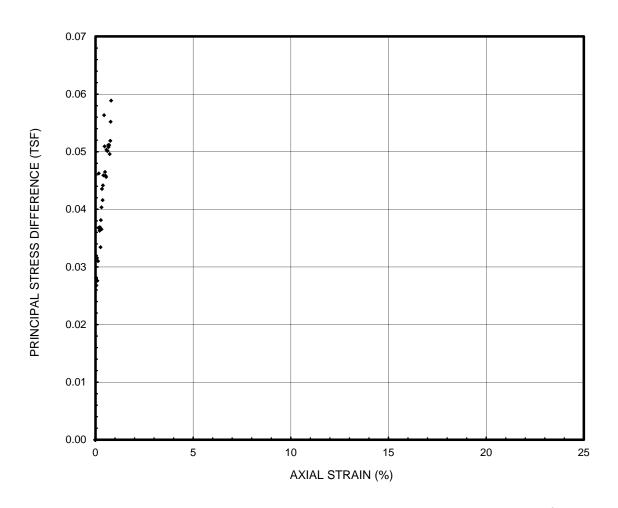


Initial Height	2.794	in	Cell Pressure	2.00	lb/in ²
Initial Diameter	1.367	in	Strain Rate	1.0	%/min
Dry Density	53.8	lb/ft ³	Peak Stress	0.086	ton/ft ²
Water Content	82.7	%	Strain at Peak Stress	1.24	%
Saturation	106	%	Failure Type	Combination	

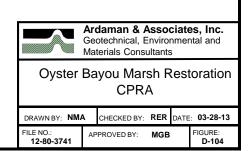


Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-13
Depth 6-8 ft

Description Gray CLAY (CH) w/ shells

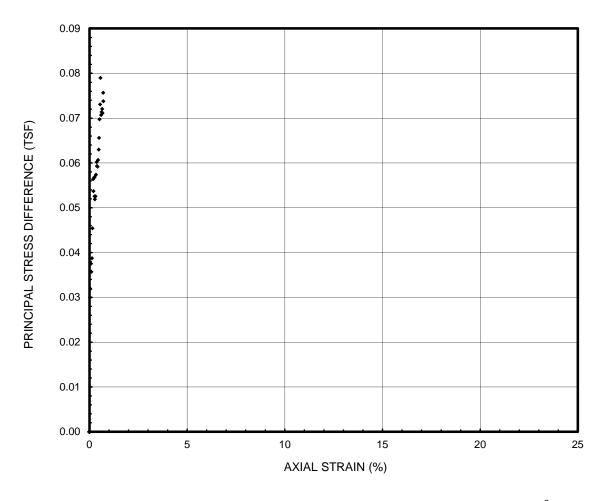


Initial Height	2.793	in	Cell Pressure	3.00	lb/in ²
Initial Diameter	1.374	in	Strain Rate	1.0	%/min
Dry Density	47.5	lb/ft ³	Peak Stress	0.059	ton/ft ²
Water Content	95.6	%	Strain at Peak Stress	0.80	%
Saturation	102	%	Failure Type	Bulging	

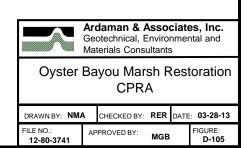


Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-13
Depth 10-12 ft

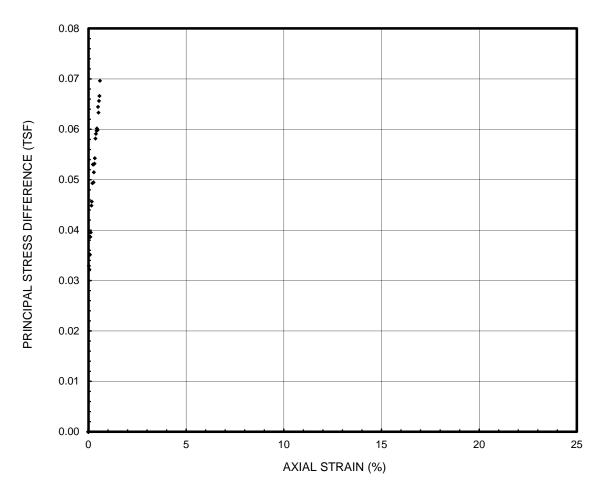
Depth 10-12 ft Gray CLAY (CH)



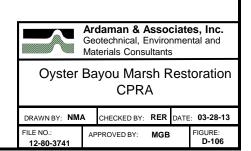
lb/in² **Cell Pressure Initial Height** 2.786 5.00 in **Initial Diameter** 1.388 Strain Rate 1.0 %/min in lb/ft³ ton/ft² **Dry Density** 54.1 **Peak Stress** 0.079 **Water Content** 78.0 % **Strain at Peak Stress** 0.57 Saturation 101 % **Failure Type** Combination



Project Name
Project Number
Sample Name
Depth
Description
Oyster Bayou
12-80-3741
B-13
B-13
Gray CLAY (CH)



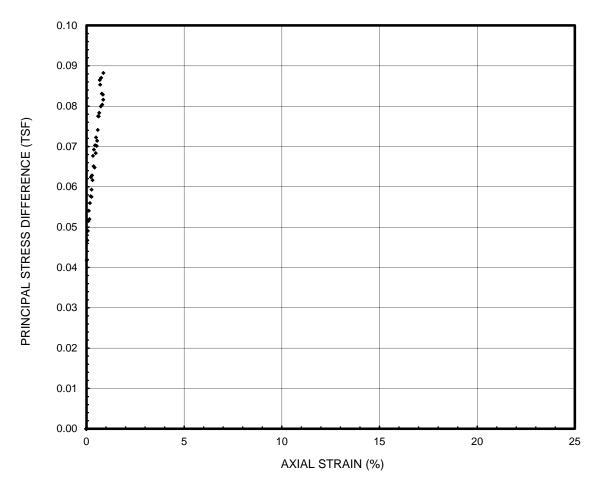
lb/in² **Cell Pressure Initial Height** 2.791 6.00 in **Initial Diameter** 1.392 Strain Rate 1.0 %/min in lb/ft³ ton/ft² **Dry Density** 49.7 **Peak Stress** 0.070 **Water Content** 89.1 % **Strain at Peak Stress** 0.59 Saturation 102 % **Failure Type** Combination



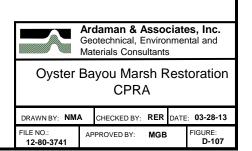
Project NameOyster BayouProject Number12-80-3741Sample NameB-13

Depth 18-20 ft

Description Gray CLAY (CH) w/ shells

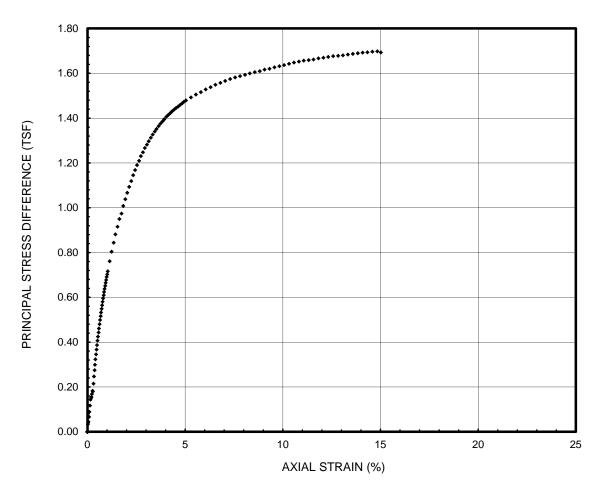


Initial Height	2.813	in	Cell Pressure	8.00	lb/in ²
Initial Diameter	1.392	in	Strain Rate	1.0	%/min
Dry Density	77.4	lb/ft ³	Peak Stress	0.088	ton/ft ²
Water Content	43.7	%	Strain at Peak Stress	0.87	%
Saturation	102	%	Failure Type	Combination	

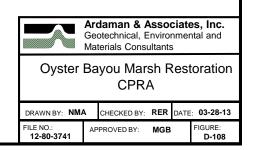


Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-13
Depth 23-25 ft

Description Tan and gray CLAY (CH) w/ silt layers and sand

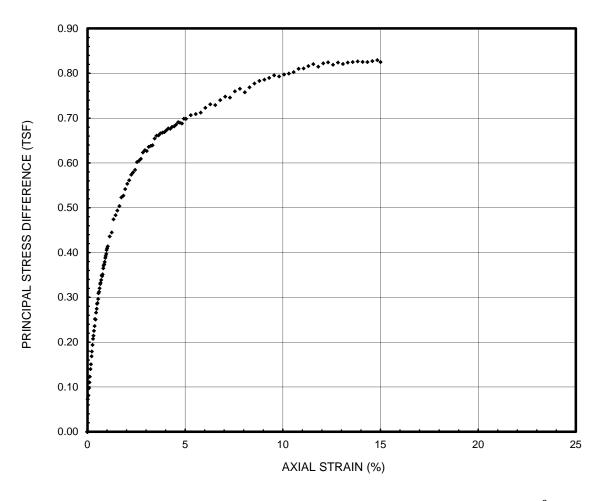


Initial Height	5.767	in	Cell Pressure	10.00	lb/in ²
Initial Diameter	2.868	in	Strain Rate	1.0	%/min
Dry Density	103.9	lb/ft ³	Peak Stress	1.698	ton/ft ²
Water Content	21.3	%	Strain at Peak Stress	14.84	%
Saturation	96	%	Failure Type	Bulging	

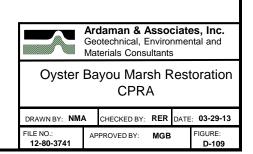


Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-13
Depth 28-30 ft

Description Tan and gray CLAY (CH) w/ silt layers and sand

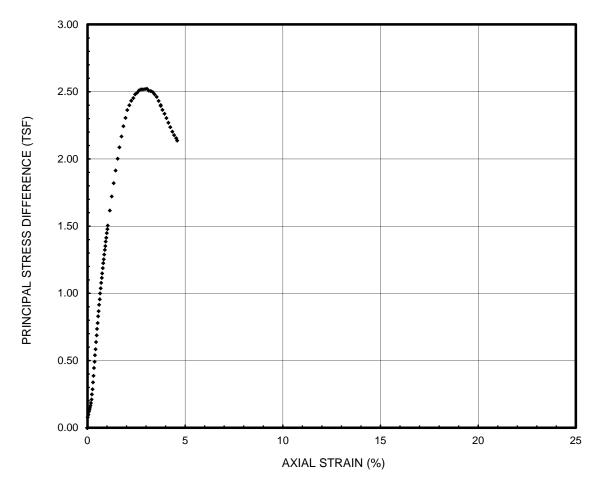


Initial Height	2.805	in	Cell Pressure	12.00	lb/in ²
Initial Diameter	1.400	in	Strain Rate	1.0	%/min
Dry Density	90.9	lb/ft ³	Peak Stress	0.829	ton/ft ²
Water Content	30.6	%	Strain at Peak Stress	14.84	%
Saturation	99	%	Failure Type	Bulging	

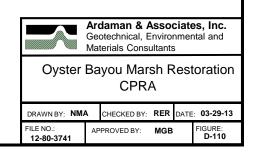


Project NameOyster BayouProject Number12-80-3741Sample NameB-13 (BL-2)Depth38-40

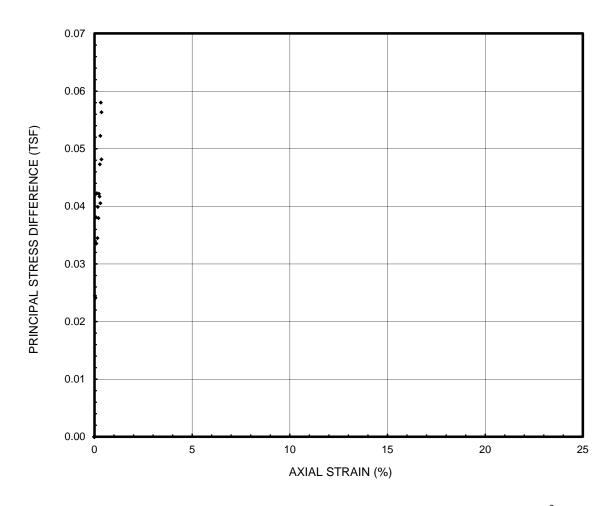
Description Tan and gray CLAY (CH)



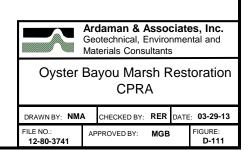
Initial Height Initial Diameter	2.672 1.423	in in	Cell Pressure Strain Rate	16.00 1.0	lb/in² %/min
Dry Density	87.9	lb/ft ³	Peak Stress	2.521	ton/ft ²
Water Content	33.3	%	Strain at Peak Stress	3.04	%
Saturation	100	%	Failure Type	Diagonal Plane	



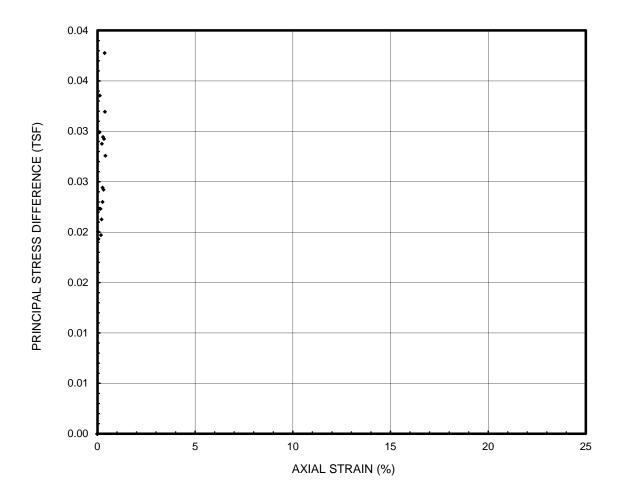
Project Name
Project Number
Sample Name
Depth
Description
Oyster Bayou
12-80-3741
B-14
2-4
ft
Gray CLAY (CH)



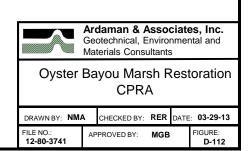
lb/in² **Cell Pressure Initial Height** 2.837 2.00 in **Initial Diameter** 1.387 Strain Rate 1.0 %/min in lb/ft³ ton/ft² **Dry Density** 57.3 **Peak Stress** 0.058 **Water Content** 70.6 % **Strain at Peak Stress** 0.32 Saturation 99 % **Failure Type** Combination



Project Name
Project Number
Sample Name
Depth
Description
Oyster Bayou
12-80-3741
B-14
4-6
ft
Gray CLAY (CH)

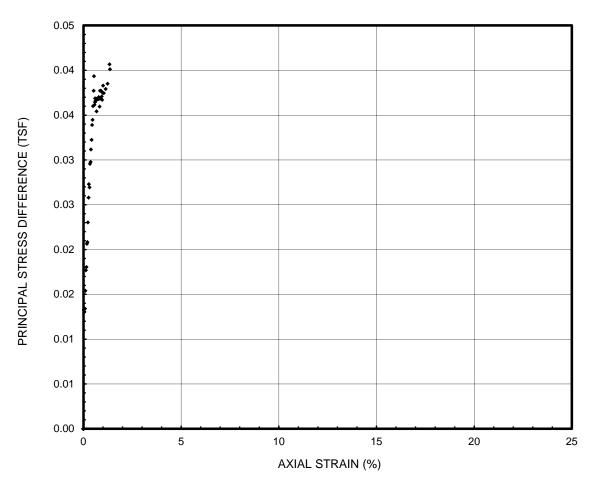


lb/in² **Cell Pressure Initial Height** 2.787 2.00 in **Initial Diameter** 1.392 Strain Rate 1.0 %/min in lb/ft³ ton/ft² **Dry Density** 49.2 **Peak Stress** 0.038 **Water Content** 86.3 % **Strain at Peak Stress** 0.37 Saturation % 97 **Failure Type** Combination

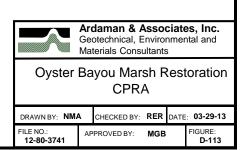


Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-14
Depth 8-10 ft

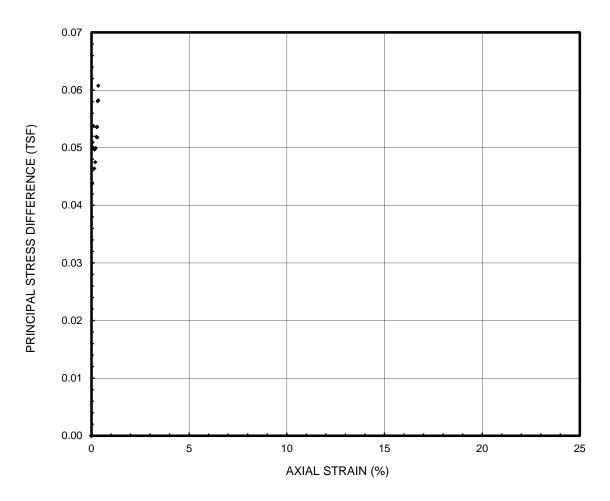
Description 8-10 ft Gray CLAY (CH)



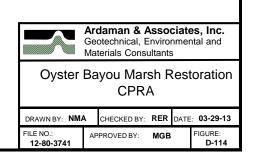
lb/in² **Cell Pressure Initial Height** 5.799 4.00 in **Initial Diameter** 2.799 Strain Rate 1.0 %/min in lb/ft³ ton/ft² **Dry Density** 57.3 **Peak Stress** 0.041 **Water Content** 76.1 % **Strain at Peak Stress** 1.33 Saturation 107 % **Failure Type** Combination



Project Name
Oyster Bayou
12-80-3741
Sample Name
Depth
Description
Oyster Bayou
12-80-3741
B-14
ft
Gray CLAY (CH)

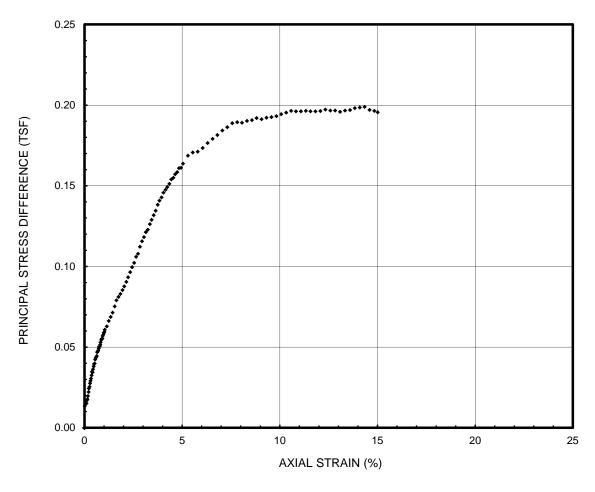


Initial Height Initial Diameter	2.797 1.375	in in	Cell Pressure Strain Rate	6.00 1.0	lb/in² %/min
Dry Density	52.3	lb/ft ³	Peak Stress	0.061	ton/ft ²
Water Content Saturation	82.8 101	% %	Strain at Peak Stress Failure Type	0.35 Other	%



Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-14
Depth 16-18 ft

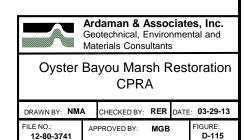
Description 16-18 ft Gray CLAY (CH)



Initial Height5.838inInitial Diameter2.767inDry Density59.1lb/ft³Water Content74.6%Saturation110%

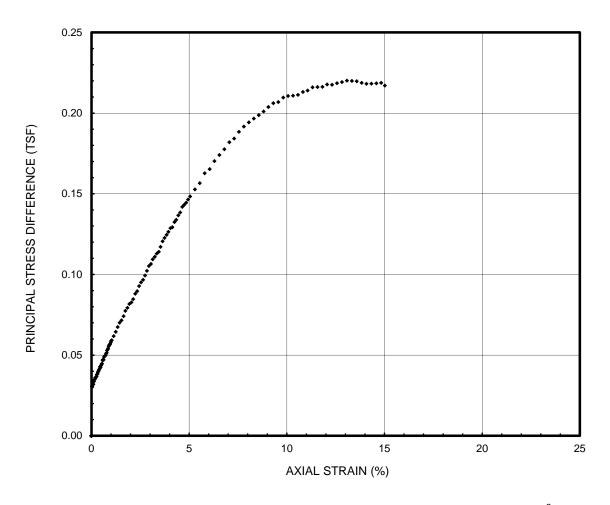
Cell Pressure
Strain Rate
Peak Stress
Strain at Peak Stress
Failure Type

7.00 lb/in²
1.0 %/min
0.199 ton/ft²
14.34 %
Combination

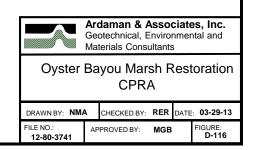


Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-14
Depth 18-20 ft

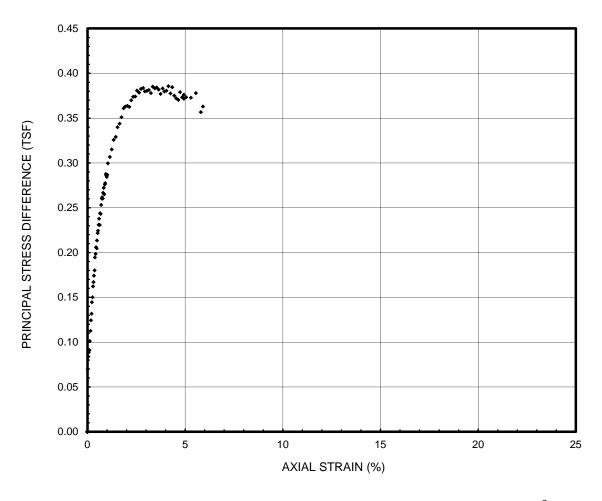
Description Gray SILTY CLAY (CL) w/ trace sand



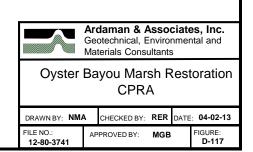
Initial Height	5.801	in	Cell Pressure	8.00	lb/in ²
Initial Diameter	2.769	in	Strain Rate	1.0	%/min
Dry Density	84.8	lb/ft ³	Peak Stress	0.220	ton/ft ²
Water Content	39.8	%	Strain at Peak Stress	13.08	%
Saturation	111	%	Failure Type	Bulging	



Project Name
Project Number
Sample Name
Depth
Description
Oyster Bayou
12-80-3741
B-14
23-25
ft
Gray CLAY (CH)

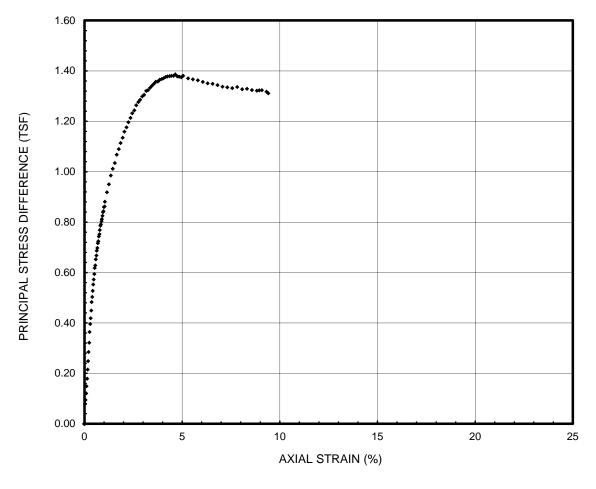


lb/in² **Cell Pressure** 10.00 **Initial Height** 2.805 in **Initial Diameter** 1.393 Strain Rate 1.0 %/min in lb/ft³ **Peak Stress** ton/ft² **Dry Density** 58.1 0.386 **Water Content** 67.3 % **Strain at Peak Stress** 4.14 Saturation 96 % **Failure Type** Diagonal Plane

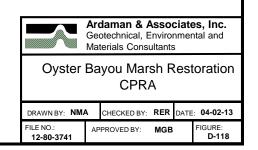


Project NameOyster BayouProject Number12-80-3741Sample NameB-14 (BL-1)Depth38-40ft

Description Brown and gray CLAY (CH) w/ silt layers

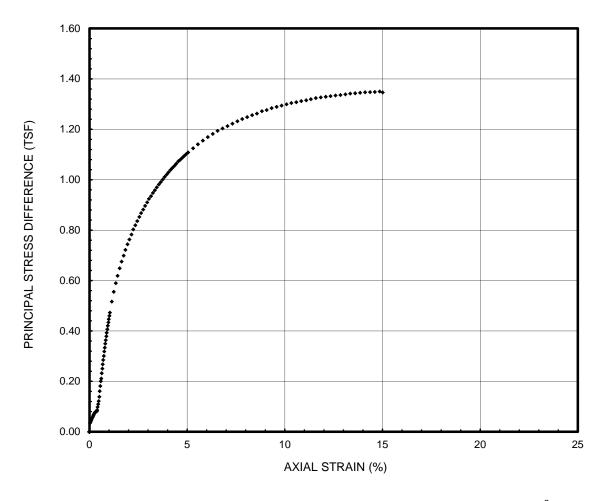


Initial Height Initial Diameter	2.803 1.393	in in	Cell Pressure Strain Rate	16.00 1.0	lb/in² %/min
Dry Density	86.0	lb/ft ³	Peak Stress	1.386	ton/ft ²
Water Content	36.0	%	Strain at Peak Stress	4.65	%
Saturation	103	%	Failure Type	Combination	

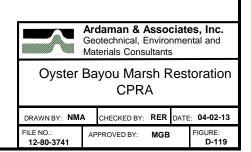


Project NameOyster BayouProject Number12-80-3741Sample NameB-14 (BL-2)Depth33-35ft

Description Gray SILTY CLAY (CL) w/ trace sand

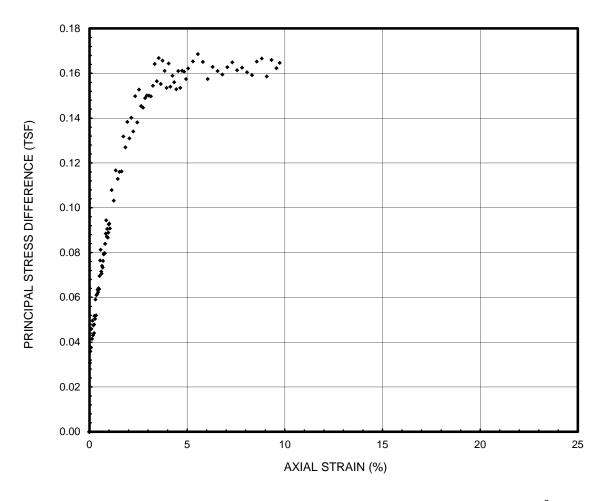


lb/in² **Cell Pressure** 14.00 **Initial Height** 5.600 in **Initial Diameter** 2.839 Strain Rate 1.0 %/min in lb/ft³ ton/ft² **Dry Density** 97.2 **Peak Stress** 1.350 **Water Content** 28.7 % **Strain at Peak Stress** 14.85 % Saturation 108 % **Failure Type** Bulging

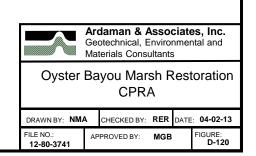


Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-15
Depth 0-2 ft

Description Gray CLAY (CH) w/ organics



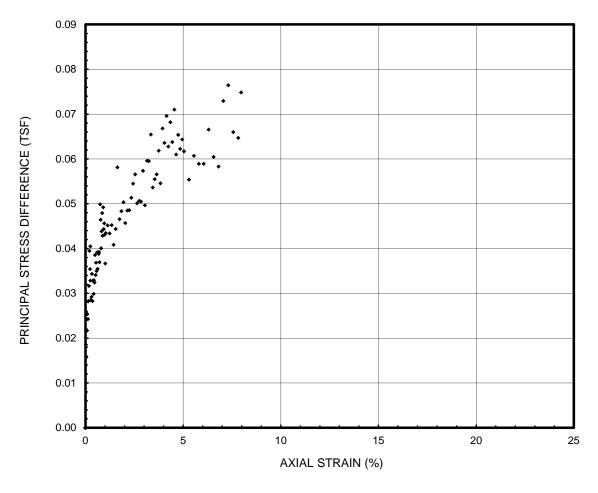
Initial Height	2.785	in	Cell Pressure	1.00	lb/in ²
Initial Diameter	1.400	in	Strain Rate	1.0	%/min
Dry Density	54.0	lb/ft ³	Peak Stress	0.169	ton/ft ²
Water Content	78.1	%	Strain at Peak Stress	5.55	%
Saturation	100	%	Failure Type	Bulging	



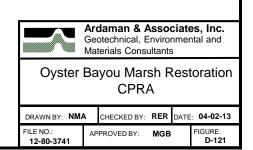
Project Name
Oyster Bayou
12-80-3741
Sample Name
B-15

Depth 4-6 ft

Description Gray CLAY (CH) w/ organics

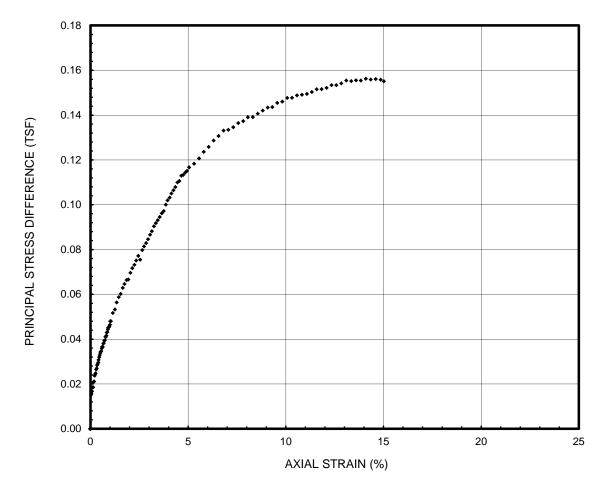


lb/in² **Cell Pressure Initial Height** 2.786 2.00 in **Initial Diameter** 1.388 Strain Rate 1.0 %/min in lb/ft³ **Peak Stress** ton/ft² **Dry Density** 47.2 0.076 **Water Content** 92.6 % **Strain at Peak Stress** 7.31 Saturation 98 % **Failure Type** Combination

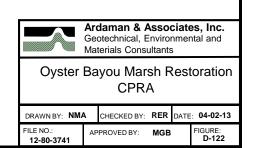


Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-15
Depth 6-8 ft

Description Gray CLAY (CH) w/ organics

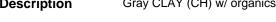


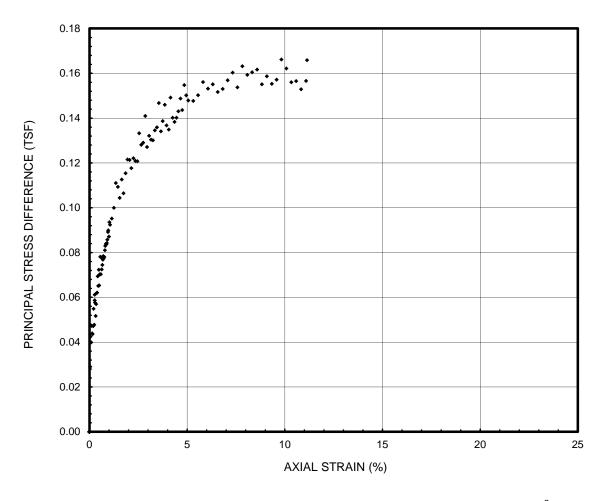
Initial Height	5.763	in	Cell Pressure	3.00	lb/in ²
Initial Diameter	2.820	in	Strain Rate	1.0	%/min
Dry Density	63.1	lb/ft ³	Peak Stress	0.156	ton/ft ²
Water Content	65.6	%	Strain at Peak Stress	14.10	%
Saturation	107	%	Failure Type	Combination	



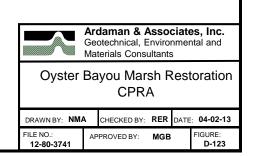
Project Name Oyster Bayou **Project Number** 12-80-3741 Sample Name B-15 Depth 8-10

Description Gray CLAY (CH) w/ organics



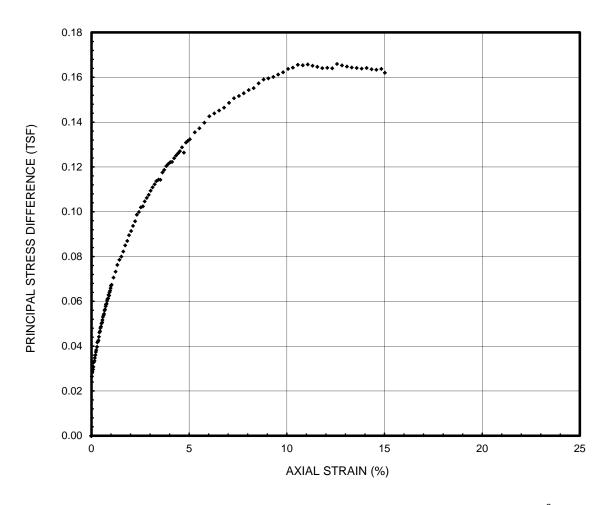


Initial Height	2.815	in	Cell Pressure	4.00	lb/in ²
Initial Diameter	1.371	in	Strain Rate	1.0	%/min
Dry Density	53.9	lb/ft ³	Peak Stress	0.166	ton/ft ²
Water Content	78.5	%	Strain at Peak Stress	9.83	%
Saturation	100	%	Failure Type	Bulging	

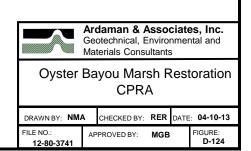


Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-15
Depth 12-14 ft

Description Gray CLAY (CH) w/ organics

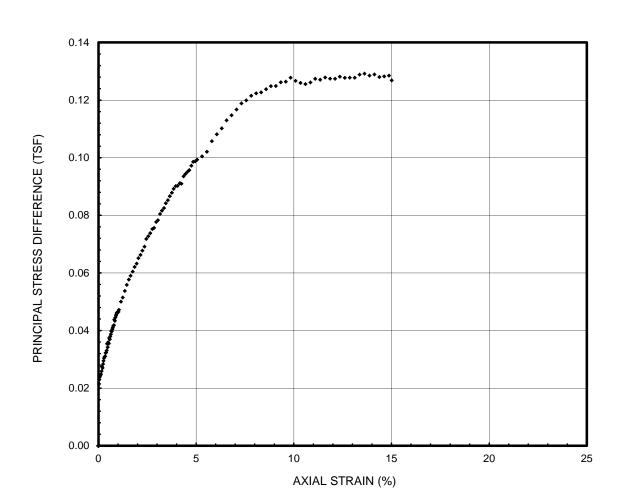


Initial Height	5.785	in	Cell Pressure	6.00	lb/in ²
Initial Diameter	2.809	in	Strain Rate	1.0	%/min
Dry Density	50.3	lb/ft ³	Peak Stress	0.166	ton/ft ²
Water Content	91.8	%	Strain at Peak Stress	12.57	%
Saturation	106	%	Failure Type	Bulging	

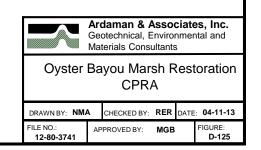


Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-15
Depth 14-16 ft

Description Gray CLAY (CH) w/ organics

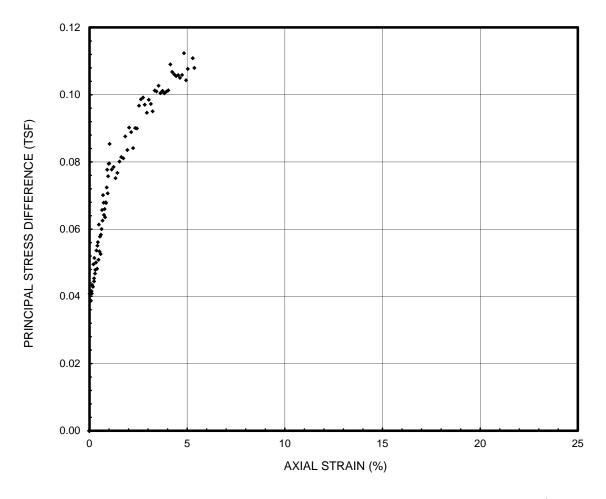


Initial Height Initial Diameter	5.802 2.872	in in	Cell Pressure Strain Rate	6.00 1.0	lb/in ² %/min
Dry Density	53.3	lb/ft ³	Peak Stress	0.129	ton/ft ²
Water Content	81.9	%	Strain at Peak Stress	13.62	%
Saturation	103	%	Failure Type	Bulging	

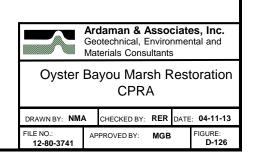


Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-15
Depth 18-20 ff

Description Gray CLAY (CH) w/ organics and sand

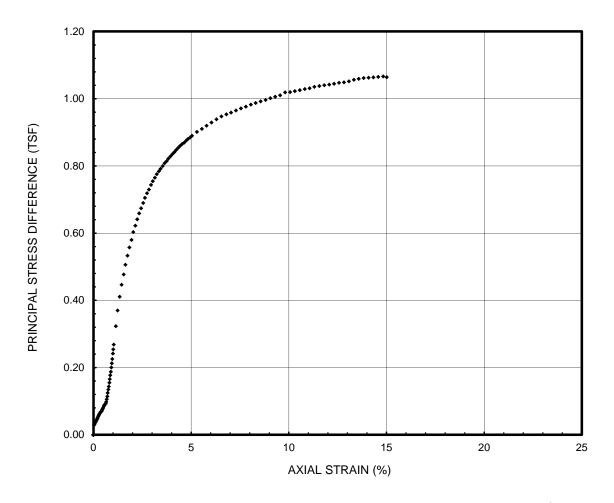


Initial Height	2.789	in	Cell Pressure	8.00	lb/in ²
Initial Diameter	1.388	in	Strain Rate	1.0	%/min
Dry Density	79.3	lb/ft ³	Peak Stress	0.112	ton/ft ²
Water Content	38.9	%	Strain at Peak Stress	4.84	%
Saturation	95	%	Failure Type	Bulging	

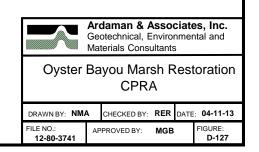


Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-15
Depth 23-25 ft

Description Gray CLAY (CH) w/ sand

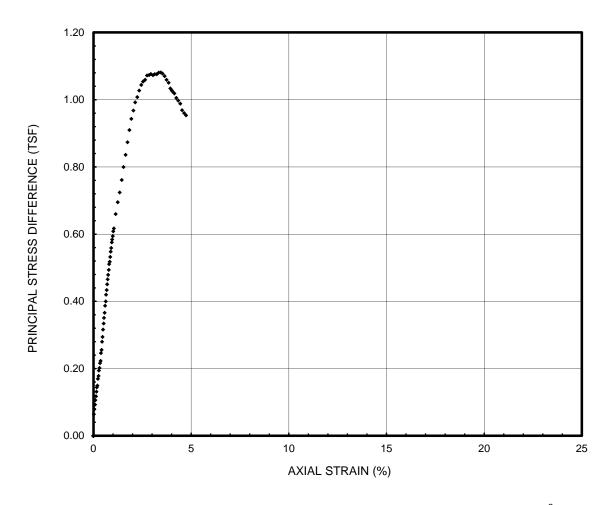


Initial Height	5.595	in	Cell Pressure	10.00	lb/in ²
Initial Diameter	2.845	in	Strain Rate	1.0	%/min
Dry Density	102.3	lb/ft ³	Peak Stress	1.066	ton/ft ²
Water Content	24.0	%	Strain at Peak Stress	14.83	%
Saturation	103	%	Failure Type	Bulging	

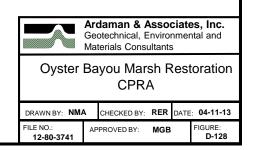


Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-15
Depth 33-35 ft

Description Tan and gray CLAY (CH) w/ silt layers

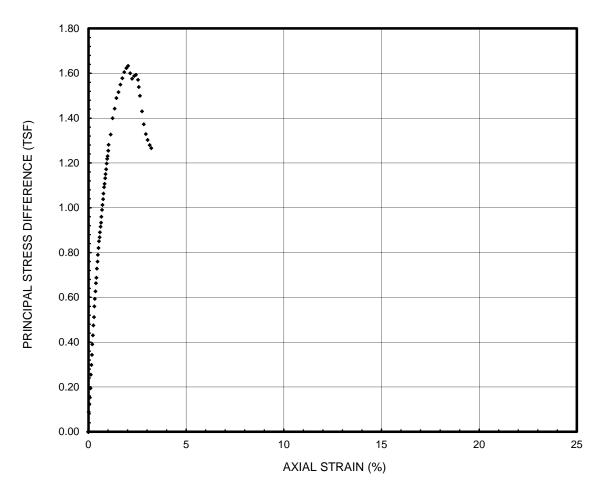


lb/in² **Cell Pressure** 14.00 **Initial Height** 2.656 in **Initial Diameter** 1.406 Strain Rate 1.0 %/min in lb/ft³ ton/ft² **Dry Density** 88.6 **Peak Stress** 1.081 **Water Content** 31.4 % **Strain at Peak Stress** 3.45 Saturation % **Failure Type** Diagonal Plane 96

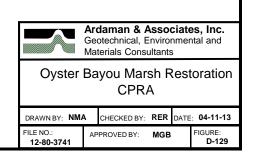


Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-15
Depth 43-45 ft

Description Tan and gray CLAY (CH) w/ silt layers

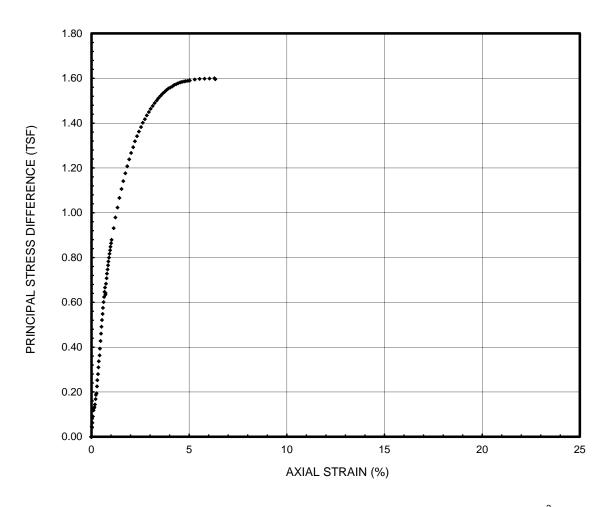


Initial Height Initial Diameter	2.803 1.415	in in	Cell Pressure Strain Rate	18.00 1.0	lb/in² %/min
Dry Density	84.1	lb/ft ³	Peak Stress	1.633	ton/ft ²
Water Content	37.0	%	Strain at Peak Stress	2.03	%
Saturation	101	%	Failure Type	Diagonal Plane	

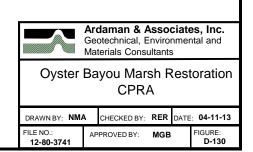


Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-15
Depth 53-55 ft

Description Tan and gray CLAY (CH) w/ silt layers

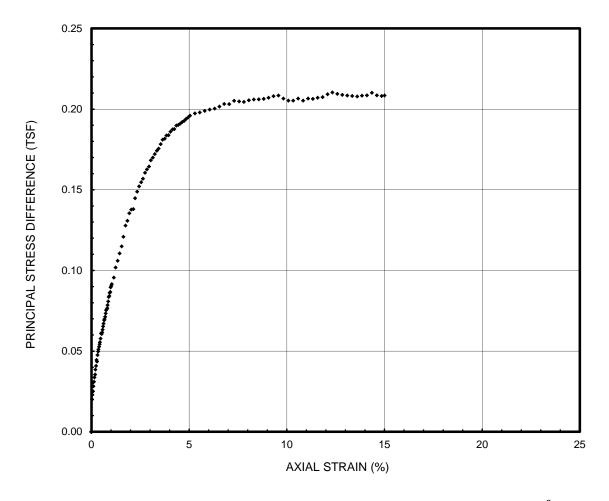


Initial Diameter 2.860 in Strain Rate 1.0 %/mir
Dry Density 85.9 lb/ft ³ Peak Stress 1.600 ton/ft ²
Water Content 36.3 % Strain at Peak Stress 6.29 %
Saturation 104 % Failure Type Bulging

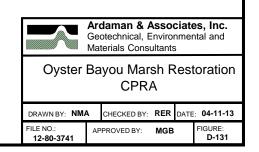


Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-16
Depth 2-4 ft

Description Gray CLAY (CH) w/ trace organics

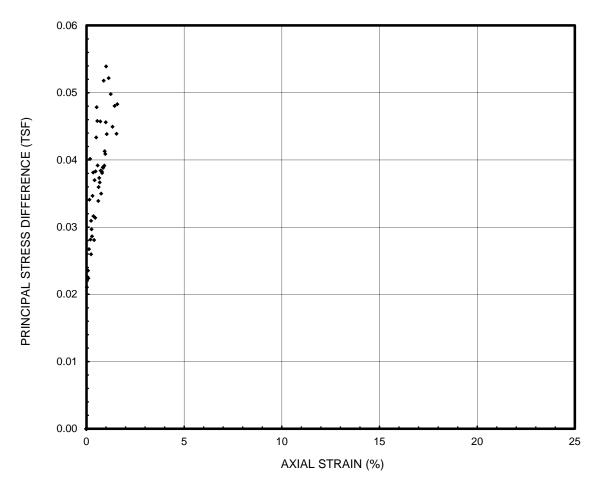


Initial Height	5.809	in	Cell Pressure	2.00	lb/in ²
Initial Diameter	2.808	in	Strain Rate	1.0	%/min
Dry Density	49.1	lb/ft ³	Peak Stress	0.210	ton/ft ²
Water Content	90.3	%	Strain at Peak Stress	12.34	%
Saturation	101	%	Failure Type	Bulging	

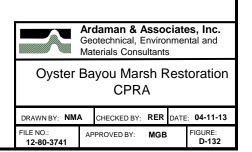


Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-16
Depth 4-6 ft

Description Gray CLAY (CH) w/ trace organics and shells



Initial Height	2.794	in	Cell Pressure	2.00	lb/in ²
Initial Diameter	1.374	in	Strain Rate	1.0	%/min
Dry Density	41.0	lb/ft ³	Peak Stress	0.054	ton/ft ²
Water Content	117.5	%	Strain at Peak Stress	1.01	%
Saturation	103	%	Failure Type	Combination	

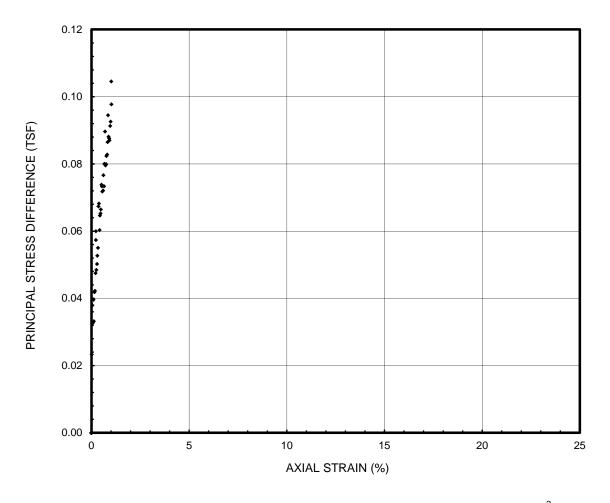


Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-16

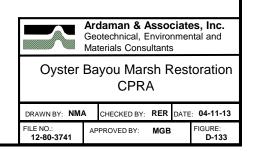
Depth 8-10 ft

Description Gray CLAY (CH) w/ trace organics and sand

pockets

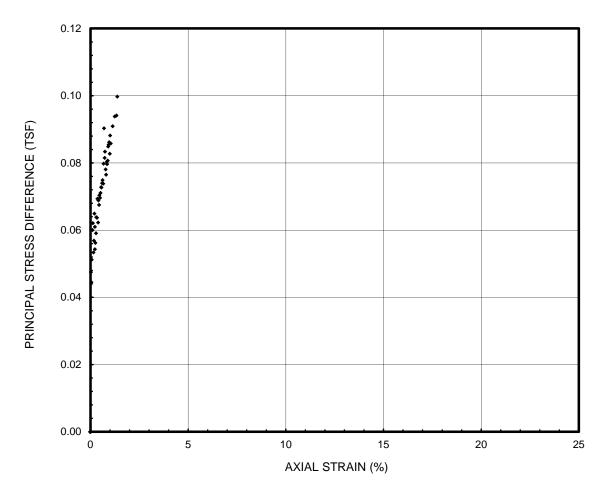


Initial Height	2.793	in	Cell Pressure	4.00	lb/in ²
Initial Diameter	1.377	in	Strain Rate	1.0	%/min
Dry Density	51.3	lb/ft ³	Peak Stress	0.105	ton/ft ²
Water Content	85.2	%	Strain at Peak Stress	1.01	%
Saturation	101	%	Failure Type	Combination	

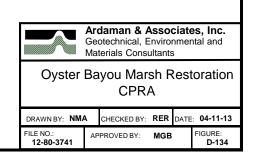


Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-16
Depth 12-14 ft

Description Gray CLAY (CH) w/ trace organics



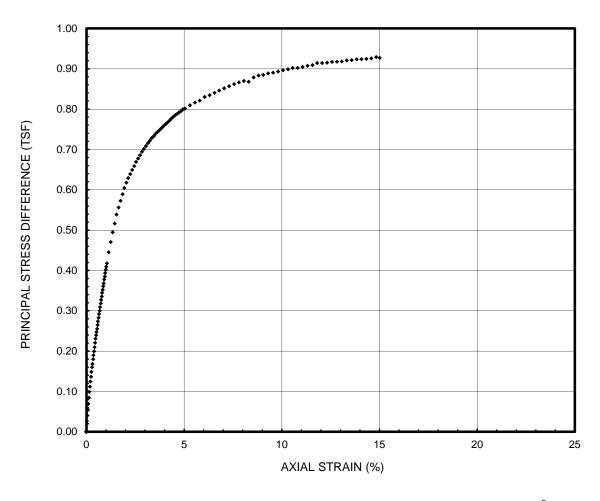
Initial Height Initial Diameter	2.794 1.373	in in	Cell Pressure Strain Rate	6.00 1.0	lb/in² %/min
Dry Density	55.9	lb/ft ³	Peak Stress	0.100	ton/ft ²
Water Content	76.9	%	Strain at Peak Stress	1.38	%
Saturation	104	%	Failure Type	Combination	



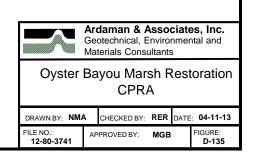
Project NameOyster BayouProject Number12-80-3741Sample NameB-16

Depth 16-18 ft

Description Gray SILTY CLAY (CL)



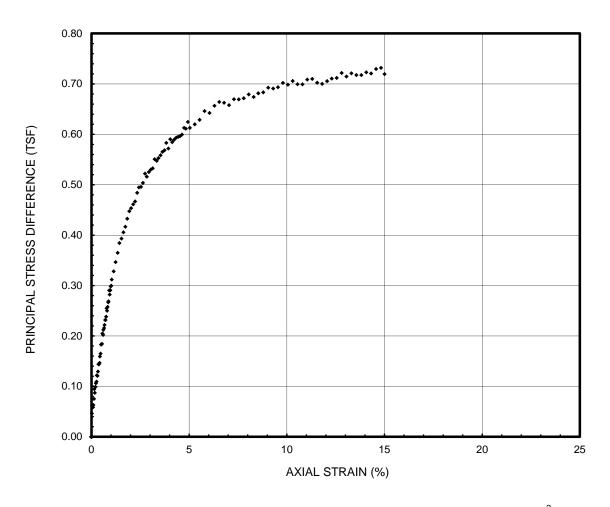
Initial Height	5.825	in	Cell Pressure	7.00	lb/in ²
Initial Diameter	2.850	in	Strain Rate	1.0	%/min
Dry Density	94.0	lb/ft ³	Peak Stress	0.929	ton/ft ²
Water Content	31.1	%	Strain at Peak Stress	14.83	%
Saturation	108	%	Failure Type	Bulging	



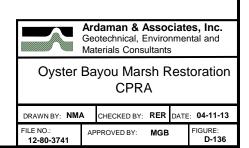
Project NameOyster BayouProject Number12-80-3741Sample NameB-16

Depth 18-20 ft

Description Gray CLAY (CH) w/ silt

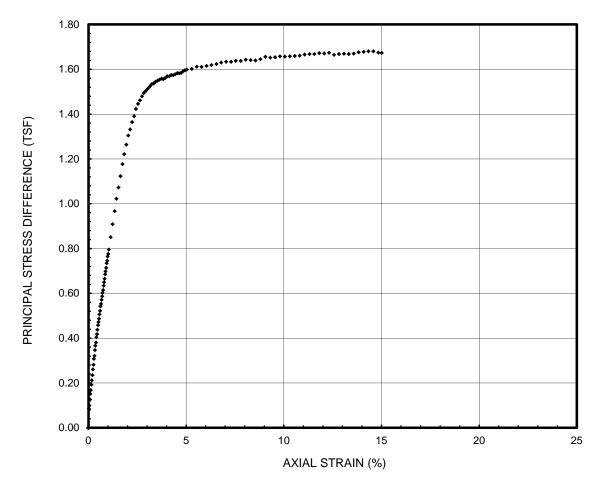


lb/in² **Cell Pressure Initial Height** 2.791 8.00 in **Initial Diameter** 1.392 Strain Rate 1.0 %/min in lb/ft³ ton/ft² **Dry Density** 91.3 **Peak Stress** 0.732 **Water Content** 31.0 % **Strain at Peak Stress** 14.82 Saturation 101 % **Failure Type** Combination

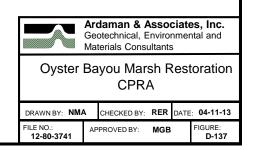


Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-16
Depth 23-25 ft

Description Gray SILTY CLAY (CL) w/ sand layers

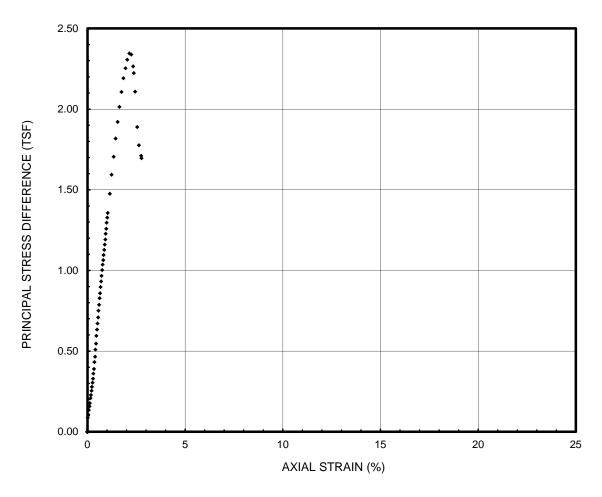


Initial Height Initial Diameter	2.726 1.410	in in	Cell Pressure Strain Rate	10.00 1.0	lb/in² %/min
Dry Density	99.4	lb/ft ³	Peak Stress	1.680	ton/ft ²
Water Content	23.7	%	Strain at Peak Stress	14.58	%
Saturation	95	%	Failure Type	Combination	

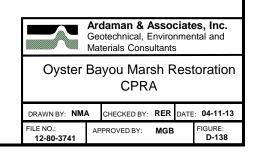


Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-16
Depth 33-35 ft

Description Tan and gray CLAY (CH) w/ silt layers

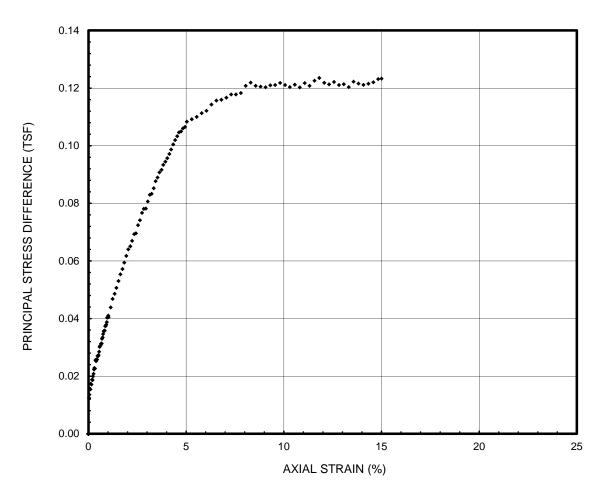


Initial Height Initial Diameter	2.801 1.401	in in	Cell Pressure Strain Rate	14.00 1.0	lb/in² %/min
Dry Density	90.6	lb/ft ³	Peak Stress	2.346	ton/ft ²
Water Content	32.3	%	Strain at Peak Stress	2.15	%
Saturation	104	%	Failure Type	Diagonal Plane	

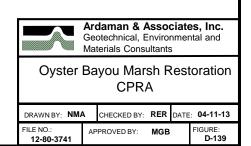


Project Name
Oyster Bayou
12-80-3741
Sample Name
B-17

 $\begin{array}{lll} \textbf{Depth} & & \text{0-2} & \text{ft} \\ \textbf{Description} & & \text{Gray CLAY (CH)} \\ \end{array}$

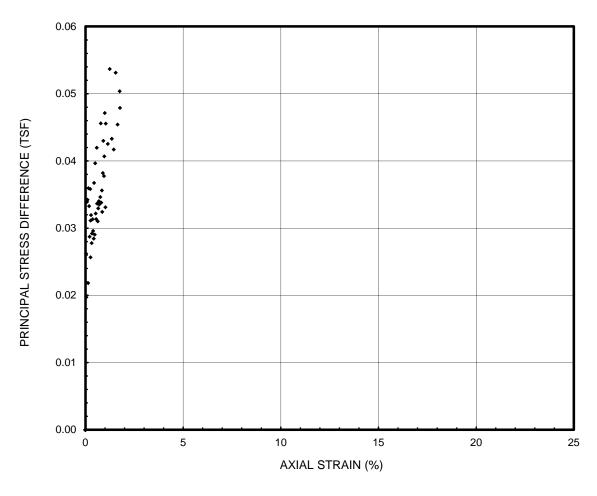


lb/in² **Cell Pressure Initial Height** 5.764 1.00 in **Initial Diameter** 2.731 Strain Rate 1.0 %/min in lb/ft³ ton/ft² **Dry Density** 44.4 **Peak Stress** 0.124 **Water Content** 114.0 % **Strain at Peak Stress** 11.81 Saturation 111 % **Failure Type** Combination

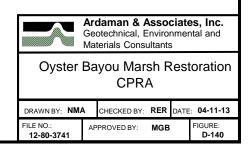


Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-17
Depth 2-4 ft

Depth 2-4 ft **Description** Gray CLAY (CH)

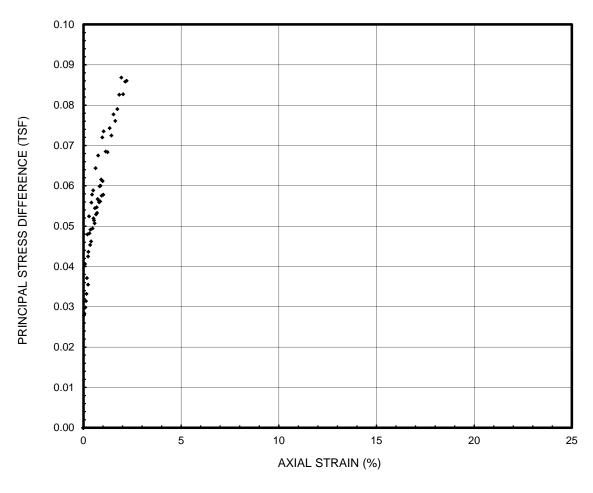


lb/in² **Cell Pressure Initial Height** 2.781 2.00 in **Initial Diameter** 1.388 Strain Rate 1.0 %/min in lb/ft³ ton/ft² **Dry Density** 36.5 **Peak Stress** 0.054 **Water Content** 135.6 % **Strain at Peak Stress** 1.24 Saturation 102 % **Failure Type** Combination

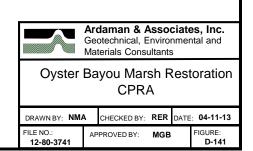


Project Name
Oyster Bayou
Project Number
12-80-3741
Sample Name
B-17
Depth
6-8
ft

Description Gray CLAY (CH)

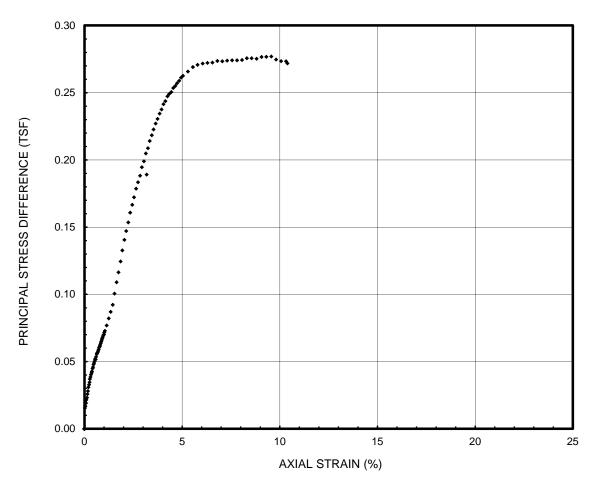


lb/in² **Cell Pressure Initial Height** 2.800 3.00 in **Initial Diameter** 1.361 Strain Rate 1.0 %/min in lb/ft³ ton/ft² **Dry Density** 54.6 **Peak Stress** 0.087 **Water Content** 80.5 % **Strain at Peak Stress** 1.94 % Saturation 105 % **Failure Type** Other

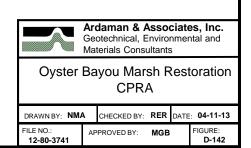


Project Name
Oyster Bayou
12-80-3741
Sample Name
B-17

Depth 10-12 ft **Description** Gray CLAY (CH)

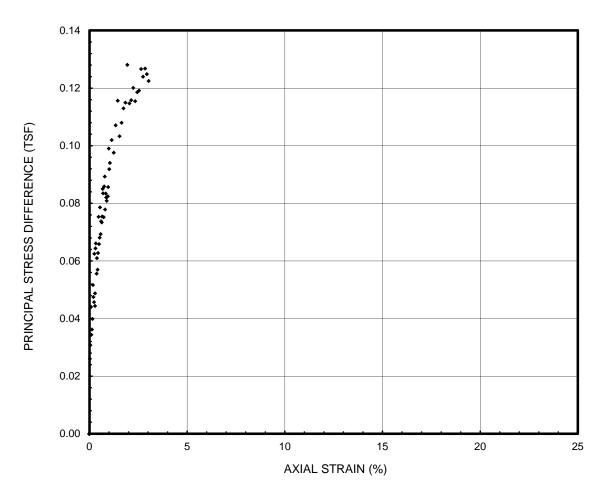


lb/in² **Cell Pressure Initial Height** 5.00 5.777 in **Initial Diameter** 2.798 Strain Rate 1.0 %/min in lb/ft³ ton/ft² **Dry Density** 52.2 **Peak Stress** 0.277 **Water Content** 87.1 % **Strain at Peak Stress** 9.57 Saturation 106 % **Failure Type** Combination

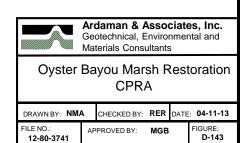


Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-17
Depth 14-16 ft

Depth 14-16 ft **Description** Gray CLAY (CH)



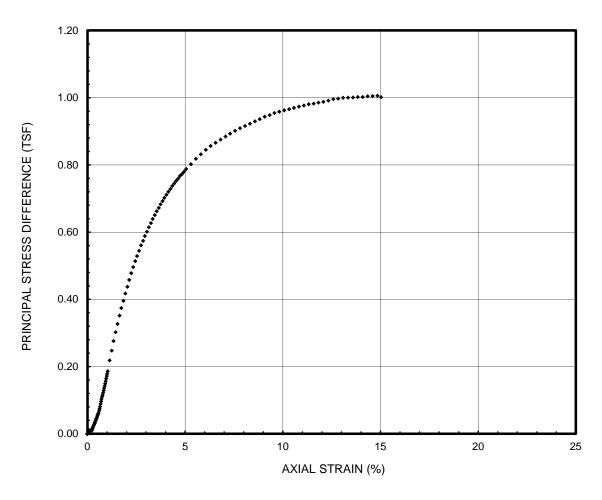
lb/in² **Cell Pressure Initial Height** 2.797 6.00 in **Initial Diameter** 1.383 Strain Rate 1.0 %/min in lb/ft³ ton/ft² **Dry Density** 50.7 **Peak Stress** 0.128 **Water Content** 87.0 % **Strain at Peak Stress** 1.94 Saturation 102 % **Failure Type** Combination



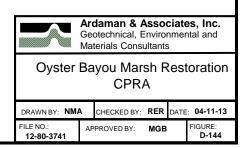
Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-17

Depth 16-18 ft

Description Gray SILTY CLAY (CL)



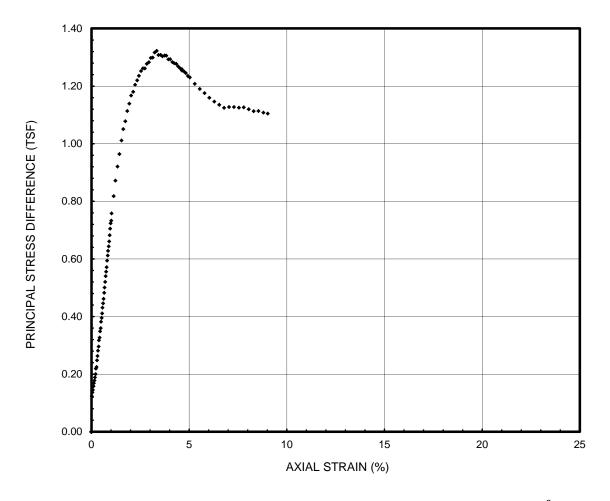
Initial Height	5.820	in	Cell Pressure	7.00	lb/in ²
Initial Diameter	2.814	in	Strain Rate	1.0	%/min
Dry Density	101.2	lb/ft ³	Peak Stress	1.006	ton/ft ²
Water Content	26.7	%	Strain at Peak Stress	14.84	%
Saturation	111	%	Failure Type	Combina	tion



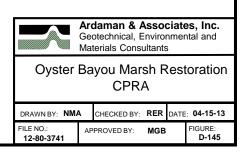
Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-17

Depth 38-40 ft

Description Tan and gray CLAY (CH) w/ silt layers

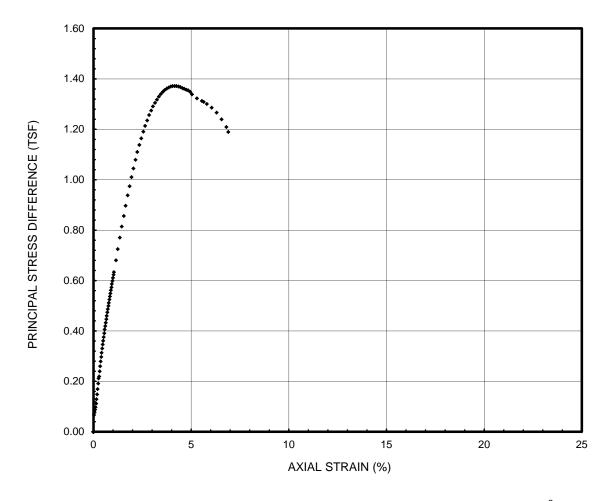


Initial Height	2.805	in	Cell Pressure	16.00	lb/in ²
Initial Diameter	1.393	in	Strain Rate	1.0	%/min
Dry Density	85.4	lb/ft ³	Peak Stress	1.322	ton/ft ²
Water Content	37.2	%	Strain at Peak Stress	3.34	%
Saturation	105	%	Failure Type	Diagonal	l Plane

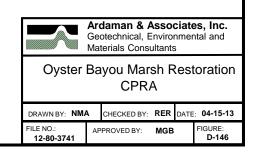


Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-17
Depth 48-50 ft

Description Tan and gray CLAY (CH) w/ silt layers

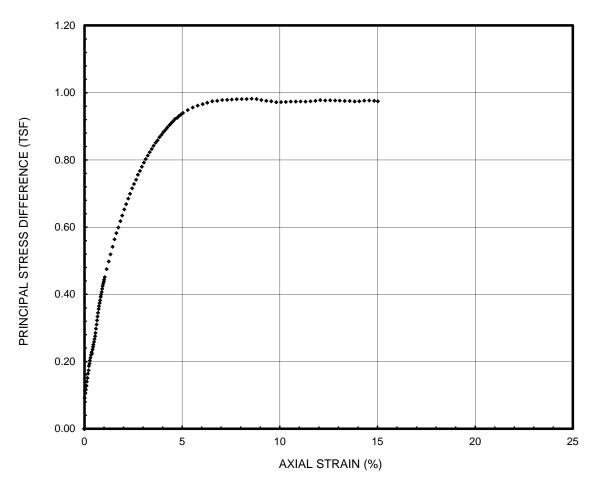


Initial Height	4.569	in	Cell Pressure	20.00	lb/in ²
Initial Diameter	2.826	in	Strain Rate	1.0	%/min
Dry Density	82.5	lb/ft ³	Peak Stress	1.372	ton/ft ²
Water Content	40.6	%	Strain at Peak Stress	4.05	%
Saturation	107	%	Failure Type	Diagonal	Plane

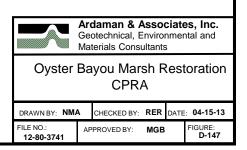


Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-17
Depth 58-60 ft

Description Tan and gray CLAY (CH) w/ silt layers

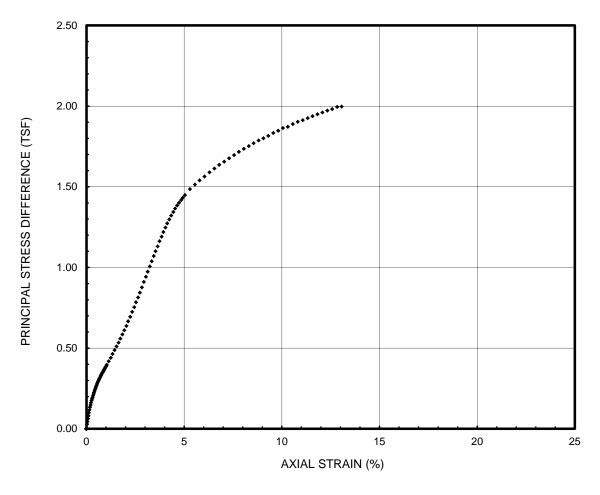


Initial Height	5.603	in	Cell Pressure	24.00	lb/in ²
Initial Diameter	2.822	in	Strain Rate	1.0	%/min
Dry Density	80.5	lb/ft ³	Peak Stress	0.982	ton/ft ²
Water Content	43.3	%	Strain at Peak Stress	8.55	%
Saturation	109	%	Failure Type	Combina	tion

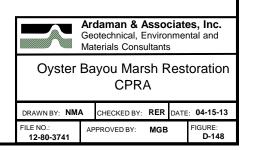


Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-18
Depth 23-25 ft

Description Brown and gray CLAYEY SAND (SC) w/ silt



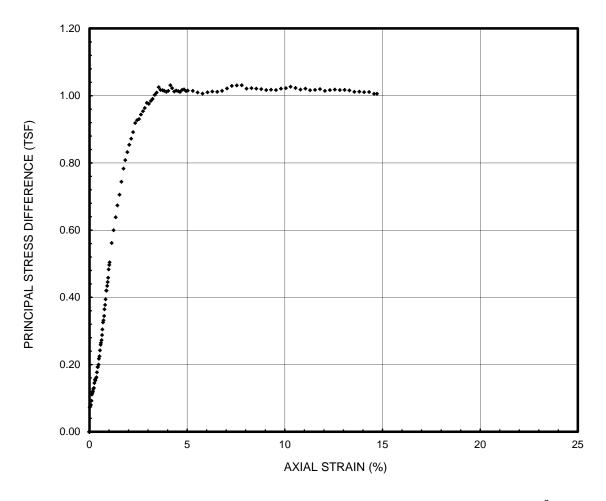
Initial Height	5.601	in	Cell Pressure	10.00	lb/in ²
Initial Diameter	2.831	in	Strain Rate	1.0	%/min
Dry Density	109.0	lb/ft ³	Peak Stress	1.997	ton/ft ²
Water Content	21.0	%	Strain at Peak Stress	13.06	%
Saturation	108	%	Failure Type	Combina	tion



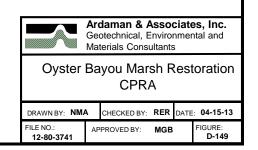
Project NameOyster BayouProject Number12-80-3741Sample NameB-18

Depth 33-35 ft

Description Gray SILTY CLAY (CL) w/ sand layers

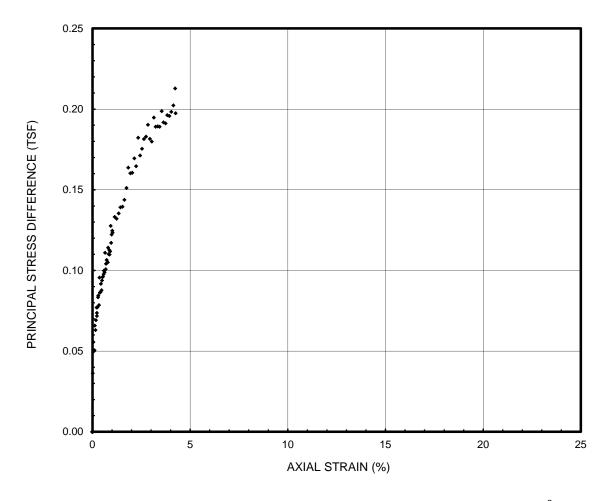


Initial Height	2.789	in	Cell Pressure	14.00	lb/in ²
Initial Diameter	1.427	in	Strain Rate	1.0	%/min
Dry Density	89.5	lb/ft ³	Peak Stress	1.031	ton/ft ²
Water Content	30.0	%	Strain at Peak Stress	7.79	%
Saturation	94	%	Failure Type	Diagonal	Plane

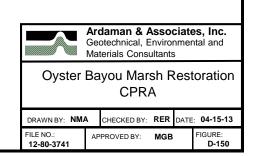


Project Name
Oyster Bayou
Project Number
12-80-3741
Sample Name
B-19
Depth
4-6
ft

Description Gray SANDY CLAY (CL) w/ silt



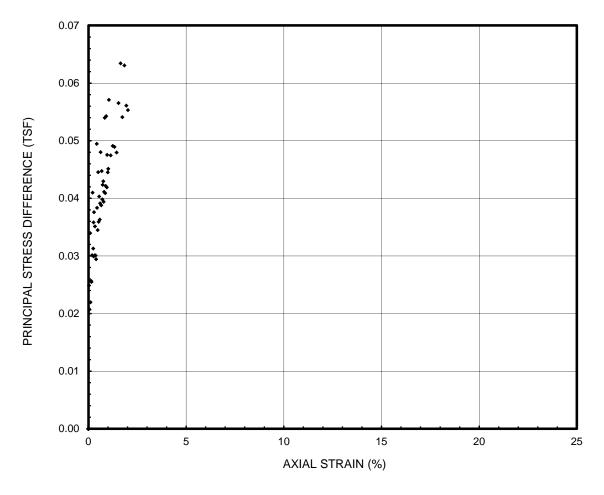
Initial Height	2.791	in	Cell Pressure	2.00	lb/in ²
Initial Diameter	1.369	in	Strain Rate	1.0	%/min
Dry Density	89.5	lb/ft ³	Peak Stress	0.213	ton/ft ²
Water Content	30.8	%	Strain at Peak Stress	4.24	%
Saturation	96	%	Failure Type	Combina	ıtion



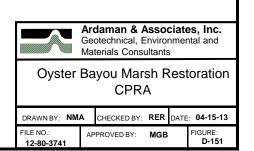
Project NameOyster BayouProject Number12-80-3741Sample NameB-19

Depth 8-10 ft

Description Gray SANDY CLAY (CL) w/ silt

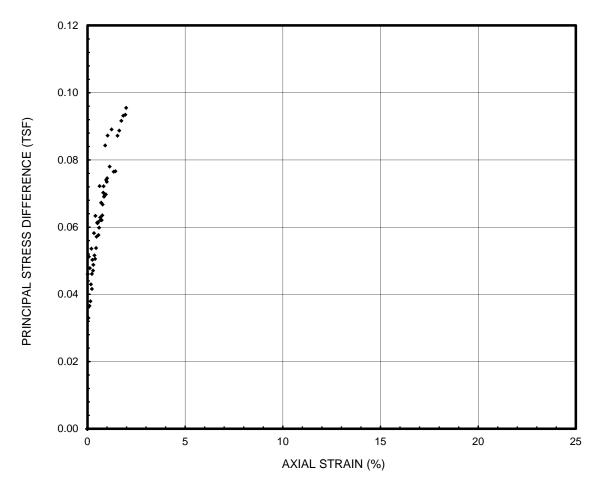


Initial Height	2.786	in	Cell Pressure	4.00	lb/in ²
Initial Diameter	1.363	in	Strain Rate	1.0	%/min
Dry Density	63.4	lb/ft ³	Peak Stress	0.063	ton/ft ²
Water Content	62.6	%	Strain at Peak Stress	1.64	%
Saturation	103	%	Failure Type	Combina	ition

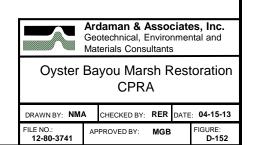


Project NameOyster BayouProject Number12-80-3741Sample NameB-19Depth10-12ft

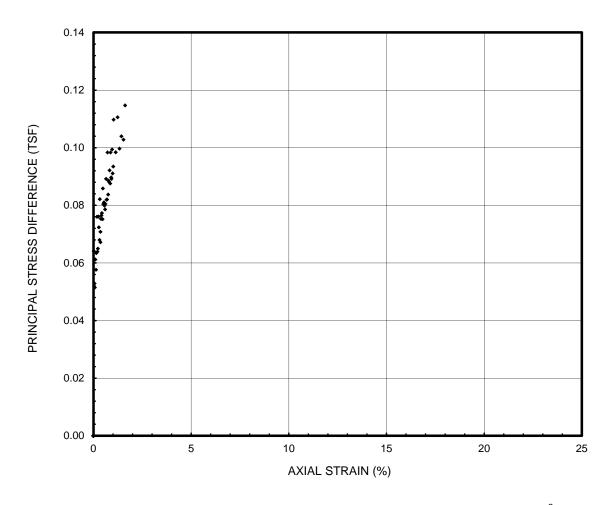
Depth 10-12 ft Gray CLAY (CH)



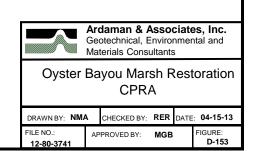
lb/in² **Cell Pressure Initial Height** 2.804 5.00 in **Initial Diameter** 1.357 Strain Rate 1.0 %/min in lb/ft³ ton/ft² **Dry Density** 61.6 **Peak Stress** 0.095 **Water Content** 66.5 % **Strain at Peak Stress** 1.98 Saturation 105 % **Failure Type** Combination



Project Name
Project Number
Sample Name
Depth
Description
Oyster Bayou
12-80-3741
B-19
B-20
ft
Gray CLAY (CH)



lb/in² **Cell Pressure Initial Height** 2.792 8.00 in **Initial Diameter** 1.373 Strain Rate 1.0 %/min in lb/ft³ ton/ft² **Dry Density** 53.0 **Peak Stress** 0.115 **Water Content** 77.9 % **Strain at Peak Stress** 1.62 % Saturation 97 % **Failure Type** Other

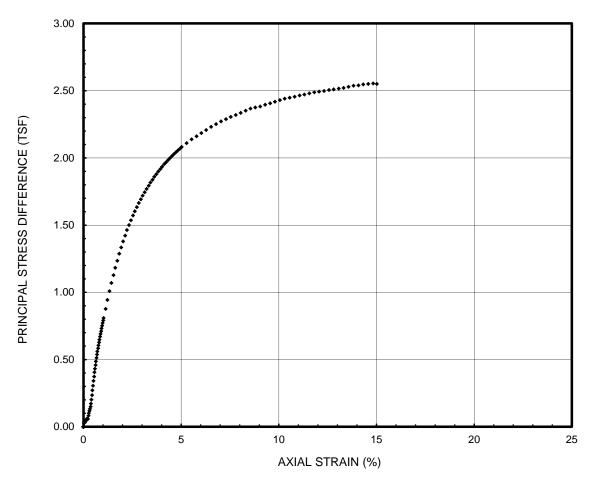


Project NameOyster BayouProject Number12-80-3741Sample NameB-19

Depth 28-30 ft

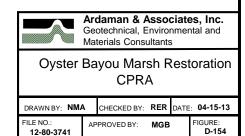
Description Tan and gray SILTY CLAY (CL) w/ trace sand

layers



Initial Height	5.598	in
Initial Diameter	2.842	in
Dry Density	107.8	lb/ft ³
Water Content	21.3	%
Saturation	105	%

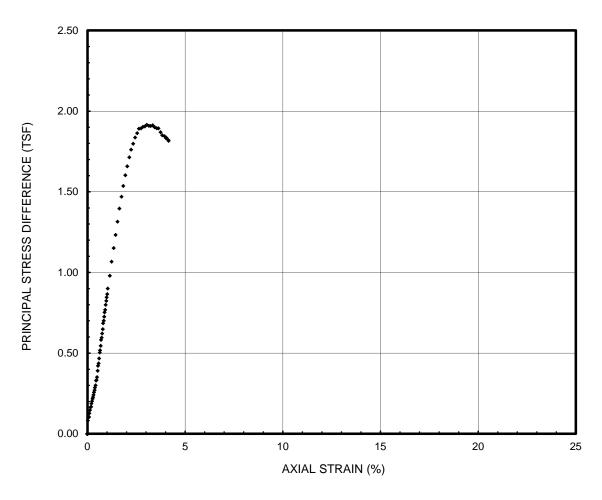
Cell Pressure Strain Rate Peak Stress Strain at Peak Stress Failure Type 12.00 lb/in²
1.0 %/min
2.554 ton/ft²
14.83 %
Combination



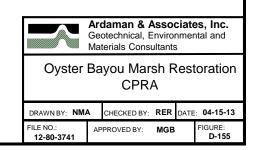
Project Name Oyster Bayou
Project Number 12-80-3741
Sample Name B-19
Depth 38-40 ft

Description Tan and gray SILTY CLAY (CL) w/ trace sand

layers



Initial Height	2.806	in	Cell Pressure	16.00	lb/in ²
Initial Diameter	1.389	in	Strain Rate	1.0	%/min
Dry Density	90.6	lb/ft ³	Peak Stress	1.915	ton/ft ²
Water Content	29.1	%	Strain at Peak Stress	3.04	%
Saturation	94	%	Failure Type	Other	

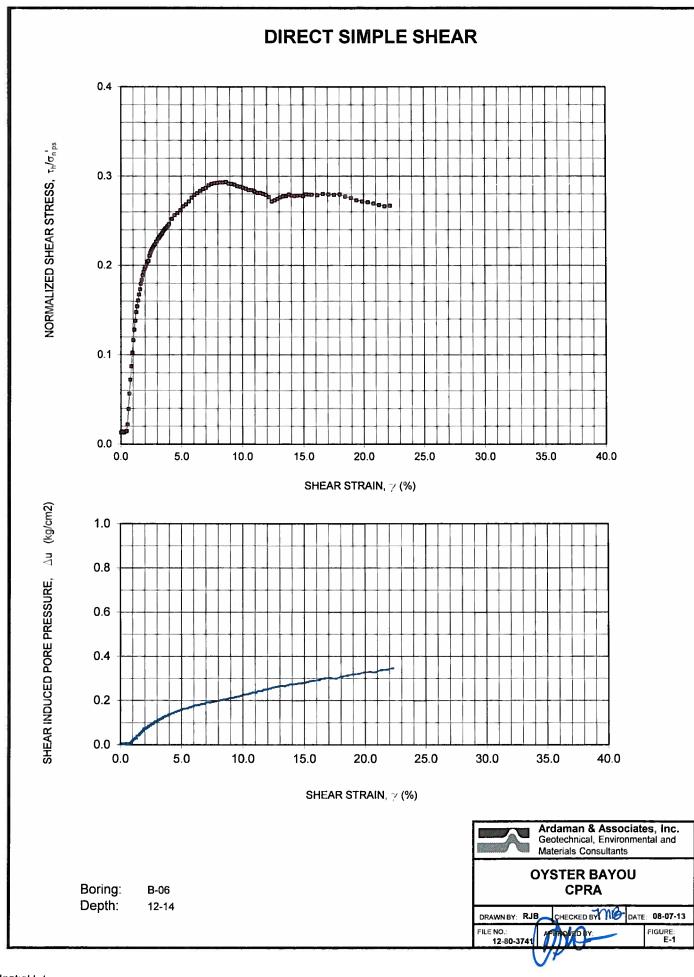


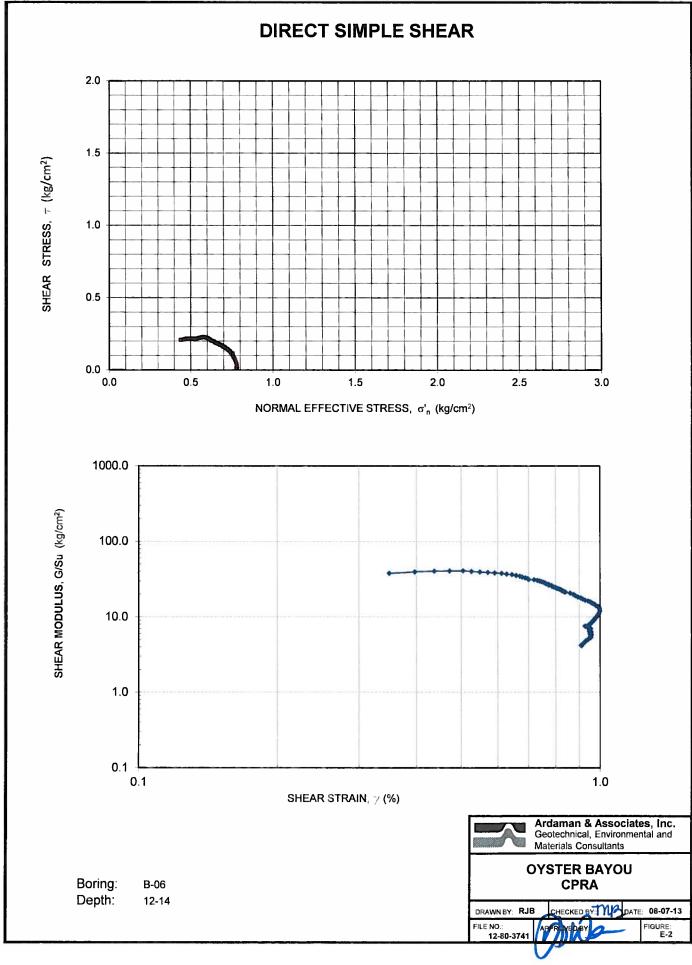
APPENDIX E. CONSOLIDATED-UNDRAINED SHEAR STRENGTH TEST RESULTS

This Appendix contains the following:

• Consolidated Undrained Shear Strength Test – Plots and Results







File Number

12-80-3741

Project Name Sample Name

B-06 12-14

Sample Area Height (preshear) Normal Load Normal Stress

Displacement Rate 0.00019

34.78 1.63 27.2 0.78 cm² cm Kg Kg/cm² in/min

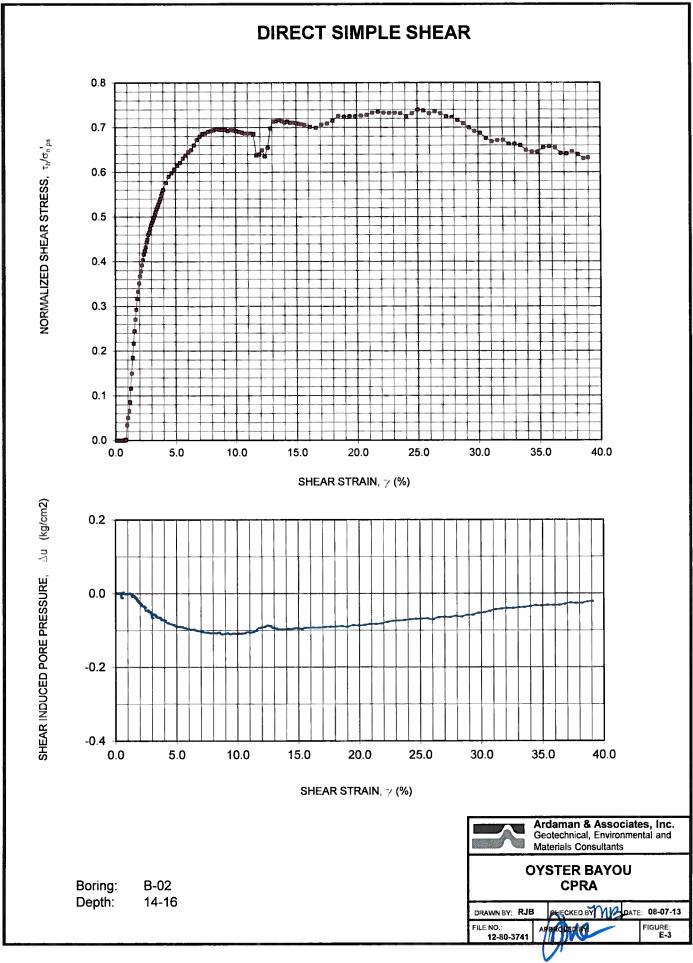
Calibration Factors

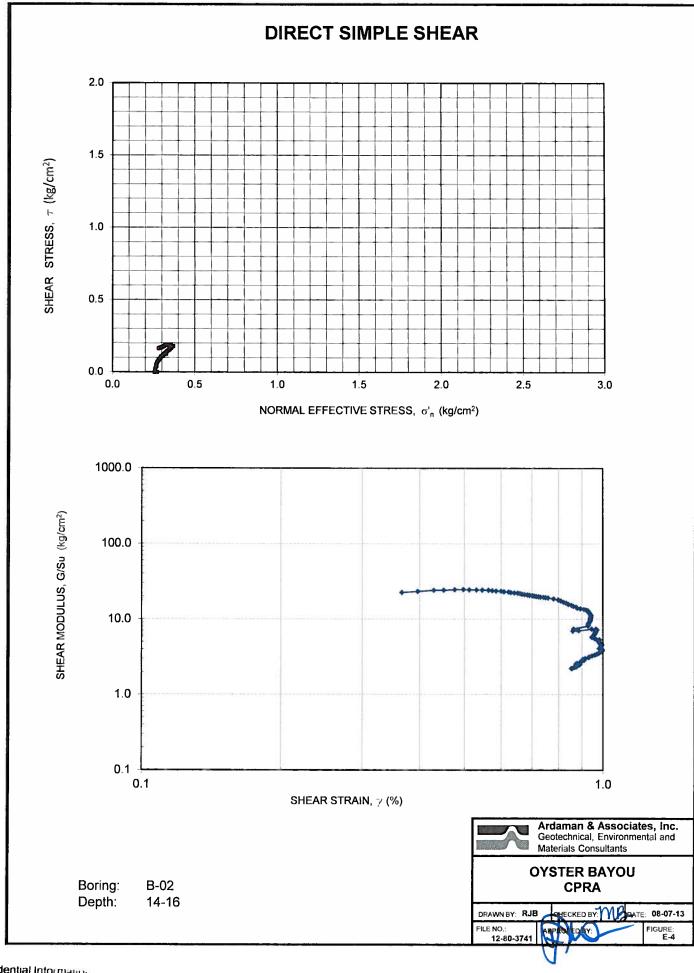
Horizontal Load, kgs.: -115721.6 Vertical Load, kgs: -67588.6 Vertical dcdt, cm: -219.453 Excitation volts: 10.000

Care Care				Normal	Shear induced				
(minutes) Stross Strain Stross Pressure (kg/cm²) Strain Modulus (kg/cm²) Stress 0.00 0.010 0.000 0.781 0.000 0.000 0.000 0.001 0.011 0.013 1.00 0.011 0.078 0.778 0.004 0.001 14.435 0.014 0.014 2.00 0.010 0.155 0.778 0.004 0.001 14.435 0.014 0.013 4.00 0.011 0.331 0.780 0.001 0.003 3.514 0.014 0.014 5.00 0.011 0.339 0.776 0.005 0.004 2.872 0.014 0.014 6.00 0.012 0.487 0.776 0.005 0.004 2.872 0.014 0.015 7.00 0.017 0.545 0.777 0.005 0.004 2.872 0.014 0.015 9.00 0.021 0.623 0.779 0.774 0.007 0.006 6.306 0.057	Elapsed Time	Shear	Shear	Effective	Pore	Axial	Shear	Normalized	Obliquity
0.00	(minutes)		Strain	Stress	Pressure	Strain	Modulus	Shear	
0.00		(kg/cm ²)	(%)	(kg/cm²)	(kg/cm ²)	(%)	(kg/cm2)	Stress	
1.00	0.00		0.000					0.0131	
2 00					0.004	0.001	14.435	0.014	0.014
3.00 0.010 0.233 0.780 0.001 0.003 4.379 0.013 0.013 4.00 0.011 0.311 0.777 0.005 0.003 3.514 0.014 0.014 6.00 0.011 0.389 0.776 0.005 0.005 2.463 0.015 0.015 0.005 0.000 0.012 0.467 0.776 0.005 0.005 2.463 0.015 0.015 0.015 0.005 0.000 0.005 2.463 0.015 0.015 0.005 0.000 0.005 0.004 0.005 0.005 0.004 0.005 0.0							6.686	0.013	0.013
4.00 0.011 0.311 0.777 0.005 0.003 3.514 0.014 0.014 5.00 0.011 0.389 0.776 0.005 0.004 2.872 0.015 0.015 7.00 0.017 0.545 0.777 0.005 0.004 3.174 0.022 0.022 8.00 0.031 0.623 0.778 0.003 0.006 4.943 0.039 0.044 9.00 0.044 0.701 0.778 0.003 0.006 6.306 0.057 0.057 10.00 0.056 0.779 0.774 0.007 0.006 6.306 0.057 0.057 11.00 0.068 0.857 0.770 0.012 0.007 7.960 0.087 0.089 12.00 0.080 0.935 0.785 0.017 0.007 8.561 0.102 0.05 13.00 0.091 0.756 0.022 0.09 8.976 0.116 0.128 14.00						0.003	4.379	0.013	0.013
5.00 0.011 0.388 0.776 0.005 0.004 2.872 0.014 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.015 0.022 0.022 0.022 0.022 0.022 0.022 0.022 0.022 0.023 0.077 0.004 0.006 6.306 0.057 0.057 0.057 0.057 0.056 0.0779 0.077 0.004 0.006 6.306 0.057 0.057 1.00 0.056 0.779 0.774 0.007 0.006 7.243 0.072 0.073 11.00 0.068 0.857 0.770 0.012 0.007 7.960 0.087 0.083 12.00 0.080 0.935 0.765 0.017 0.007 7.960 0.087 0.083 1.083 1.444 1.00 0.100 1.091 0.756 0.025 0.012 9.181 0						0.003	3.514	0.014	
6.00 0.012 0.467 0.776 0.005 0.004 3.174 0.015 7.00 7.00 0.017 0.545 0.777 0.005 0.004 3.174 0.022 0.022 8.00 0.031 0.623 0.778 0.003 0.006 4.943 0.039 0.040 9.00 0.044 0.701 0.778 0.007 0.006 6.306 0.057 0.057 10.00 0.056 0.857 0.770 0.012 0.007 0.006 7.243 0.072 0.073 11.00 0.068 0.857 0.770 0.012 0.007 7.960 0.087 0.089 12.00 0.080 0.935 0.755 0.017 0.007 8.976 0.116 0.126 13.00 0.091 1.013 0.759 0.022 0.009 8.976 0.116 0.126 14.00 0.100 1.181 0.752 0.030 0.014 9.246 0.138 0.144						0.004	2.872	0.014	0.014
7,00 0,017 0,545 0,777 0,005 0,004 3,174 0,022 0,029 8,00 0,031 0,623 0,778 0,003 0,006 4,943 0,039 0,040 9,00 0,044 0,701 0,778 0,004 0,006 6,306 0,057 0,057 10,00 0,056 0,779 0,774 0,007 0,006 7,243 0,072 0,073 11,00 0,068 0,857 0,770 0,012 0,007 7,960 0,087 0,088 12,00 0,080 0,935 0,765 0,017 0,007 8,561 0,102 0,108 13,00 0,091 1,013 0,756 0,025 0,012 9,181 0,128 0,132 1,132 1,132 1,132 1,132 1,132 1,132 1,132 1,132 1,132 1,132 1,132 1,132 1,144 1,153 1,144 1,153 1,144 1,153 1,144 1,153 1,1							2.463		0.015
8,00 0,031 0,623 0,778 0,003 0,006 4,943 0,039 0,044 9,00 0,044 0,701 0,778 0,004 0,006 6,306 0,057 0,057 10,00 0,056 0,779 0,774 0,007 0,006 7,243 0,072 0,073 11,00 0,068 0,857 0,770 0,012 0,007 7,960 0,087 0,089 12,00 0,080 0,935 0,755 0,017 0,007 8,561 0,102 0,108 13,00 0,091 1,013 0,759 0,022 0,009 8,976 0,116 0,120 14,00 0,100 1,091 0,752 0,300 0,014 9,246 0,138 0,144 16,00 0,116 1,248 0,754 0,027 0,016 9,268 0,148 0,153 17,00 0,121 1,325 0,742 0,040 0,017 9,055 0,154 0,163			0.545		0.005	0.004	3.174	0.022	0.022
9.00 0.044 0.701 0.778 0.004 0.006 6.306 0.057 0.057 10.00 0.056 0.779 0.774 0.007 0.006 7.243 0.072 0.073 11.00 0.068 0.857 0.770 0.012 0.007 7.960 0.087 0.088 12.00 0.080 0.935 0.765 0.017 0.007 8.561 0.102 0.105 13.00 0.091 1.013 0.759 0.022 0.009 8.976 0.116 0.122 14.00 0.100 1.091 0.756 0.025 0.012 9.181 0.128 0.132 15.00 0.108 1.169 0.752 0.030 0.014 9.246 0.138 0.144 16.00 0.116 1.248 0.754 0.027 0.016 9.268 0.148 0.153 17.00 0.121 1.325 0.742 0.040 0.017 9.105 0.154 0.163 18.00 0.126 1.403 0.740 0.041 0.017 8.964 0.161 0.170 19.00 0.131 1.481 0.736 0.045 0.017 8.839 0.168 0.178 20.00 0.136 1.559 0.731 0.050 0.019 8.692 0.173 0.185 21.02 0.144 1.715 0.722 0.059 0.018 8.569 0.180 0.193 22.02 0.144 1.715 0.722 0.059 0.018 8.569 0.180 0.193 22.02 0.144 1.715 0.722 0.059 0.018 8.589 0.189 0.205 24.02 0.154 1.950 0.711 1.872 0.709 0.073 0.022 8.055 0.193 0.213 25.02 0.158 2.105 0.709 0.073 0.022 8.055 0.193 0.213 25.02 0.158 2.105 0.706 0.073 0.022 8.055 0.193 0.213 25.02 0.158 2.105 0.706 0.073 0.024 7.669 0.199 0.220 27.02 0.166 2.183 0.703 0.078 0.024 7.669 0.199 0.220 27.02 0.166 2.283 0.069 0.091 0.023 7.876 0.196 0.216 26.02 0.155 2.027 0.708 0.073 0.024 7.669 0.199 0.220 27.02 0.166 2.283 0.703 0.078 0.024 7.689 0.199 0.220 27.02 0.166 2.283 0.703 0.078 0.024 7.689 0.199 0.220 27.02 0.166 2.283 0.703 0.078 0.024 7.689 0.199 0.220 27.02 0.166 2.248 0.697 0.085 0.086 0.091 0.024 7.689 0.199 0.220 27.02 0.166 2.418 0.697 0.085 0.086 0.024 7.494 0.202 0.224 28.02 0.161 2.261 0.697 0.085 0.086 0.024 7.311 0.204 0.227 29.02 0.166 2.418 0.691 0.091 0.025 6.794 0.217 0.245 33.02 0.177 2.495 0.698 0.094 0.024 7.689 0.199 0.220 0.224 2.0166 2.418 0.691 0.091 0.025 6.794 0.217 0.245 33.02 0.177 2.495 0.698 0.094 0.024 6.650 0.211 0.236 33.03 0.177 2.886 0.676 0.105 0.024 6.331 0.223 0.247 0.245 33.03 0.177 2.886 0.676 0.105 0.024 6.335 0.224 0.223 0.257 33.03 0.177 2.886 0.676 0.105 0.024 6.335 0.224 0.223 0.257 33.03 0.177 2.886 0.676 0.105 0.024 6.335 0.224 0.259 33.03 0.180 3.042 0.671 0.110 0.023 5.907 0.230						0.006	4.943	0.039	0.040
10.00							6.306	0.057	0.057
11.00 0.068 0.857 0.770 0.012 0.007 7.960 0.087 0.089 12.00 0.080 0.935 0.765 0.017 0.007 8.561 0.102 0.105 13.00 0.091 1.013 0.759 0.022 0.009 8.976 0.116 0.120 14.00 0.100 1.091 0.756 0.025 0.012 9.181 0.128 0.132 15.00 0.108 1.169 0.752 0.030 0.014 9.246 0.138 0.144 16.00 0.116 1.248 0.754 0.027 0.016 9.268 0.148 0.153 17.00 0.121 1.325 0.742 0.040 0.017 9.105 0.154 0.163 18.00 0.126 1.403 0.740 0.041 0.017 9.105 0.154 0.163 18.00 0.131 1.481 0.736 0.045 0.017 8.839 0.173 0.188							7.243	0.072	0.073
12.00 0.080 0.935 0.765 0.017 0.007 8.561 0.102 0.105 13.00 0.091 1.013 0.759 0.022 0.009 8.976 0.116 0.120 14.00 0.100 1.091 0.756 0.022 0.009 8.976 0.118 0.128 0.132 15.00 0.108 1.169 0.752 0.030 0.014 9.246 0.138 0.144 16.00 0.116 1.248 0.754 0.027 0.016 9.268 0.148 0.153 17.00 0.121 1.325 0.742 0.040 0.017 9.105 0.154 0.163 18.00 0.126 1.403 0.740 0.041 0.017 8.964 0.161 0.170 19.00 0.131 1.481 0.736 0.045 0.017 8.839 0.168 0.178 20.00 0.136 1.559 0.731 0.050 0.019 8.692 0.173 0.185 <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>0.087</td> <td>0.089</td>								0.087	0.089
13.00						0.007	8.561		0.105
14.00 0.100 1.091 0.756 0.025 0.012 9.181 0.128 0.132 15.00 0.108 1.169 0.752 0.030 0.014 9.246 0.138 0.144 16.00 0.116 1.248 0.754 0.027 0.016 9.268 0.148 0.153 17.00 0.121 1.325 0.742 0.040 0.017 9.105 0.154 0.163 18.00 0.126 1.403 0.740 0.041 0.017 8.964 0.161 0.170 19.00 0.131 1.481 0.736 0.045 0.017 8.839 0.168 0.178 20.00 0.136 1.559 0.731 0.050 0.019 8.692 0.173 0.185 21.02 0.140 1.637 0.727 0.055 0.018 8.589 0.180 0.193 22.02 0.144 1.715 0.722 0.055 0.018 8.384 0.184 0.199									0.120
15.00 0.108 1.169 0.752 0.030 0.014 9.246 0.138 0.144 16.00 0.116 1.248 0.754 0.027 0.016 9.268 0.148 0.153 17.00 0.121 1.325 0.742 0.040 0.017 9.105 0.154 0.163 18.00 0.126 1.403 0.740 0.041 0.017 8.964 0.161 0.170 19.00 0.131 1.481 0.736 0.045 0.017 8.839 0.168 0.178 20.00 0.136 1.559 0.731 0.050 0.019 8.692 0.173 0.185 21.02 0.140 1.637 0.727 0.055 0.018 8.569 0.180 0.193 22.02 0.144 1.715 0.722 0.059 0.018 8.384 0.184 0.199 23.02 0.148 1.793 0.720 0.061 0.020 8.236 0.189 0.205 24.02 0.151 1.872 0.709 0.073 0.022 8.055 0.193 0.213 25.02 0.154 1.950 0.711 0.070 0.023 7.876 0.196 0.216 26.02 0.155 2.027 0.708 0.073 0.024 7.669 0.199 0.220 27.02 0.158 2.105 0.706 0.076 0.024 7.311 0.204 0.227 29.02 0.161 2.261 0.697 0.085 0.024 7.311 0.204 0.227 29.02 0.161 2.261 0.697 0.085 0.024 7.311 0.204 0.227 29.02 0.161 2.261 0.697 0.085 0.024 7.311 0.204 0.227 29.02 0.161 2.261 0.697 0.085 0.024 7.311 0.204 0.227 29.02 0.161 2.261 0.697 0.085 0.024 7.311 0.204 0.227 29.02 0.161 2.261 0.697 0.085 0.024 7.311 0.204 0.227 29.02 0.161 2.261 0.697 0.085 0.026 7.098 0.205 0.230 30.02 0.168 2.418 0.691 0.091 0.023 6.932 0.214 0.243 32.02 0.170 2.495 0.691 0.091 0.023 6.932 0.214 0.243 32.02 0.171 2.574 0.687 0.094 0.094 0.024 6.650 0.219 0.249 34.02 0.173 2.652 0.684 0.097 0.004 6.235 0.224 0.259 37.03 0.174 2.730 0.679 0.103 0.024 6.850 0.221 0.225 35.03 0.177 2.886 0.676 0.105 0.024 6.35 0.221 0.225 38.03 0.177 2.886 0.676 0.105 0.024 6.35 0.227 0.262 38.03 0.177 2.886 0.676 0.105 0.022 6.137 0.227 0.265 38.03 0.177 2.886 0.676 0.105 0.022 6.137 0.227 0.265 38.03 0.177 2.886 0.676 0.105 0.022 6.137 0.227 0.265 38.03 0.177 2.886 0.676 0.105 0.024 5.983 0.227 0.268 38.03 0.177 2.886 0.676 0.105 0.022 6.137 0.227 0.265 38.03 0.177 2.886 0.676 0.105 0.022 6.137 0.227 0.265 38.03 0.177 2.886 0.676 0.105 0.022 6.137 0.227 0.265 38.03 0.177 2.886 0.676 0.105 0.022 6.137 0.227 0.262 38.03 0.177 2.886 0.676 0.105 0.022 6.137 0.227 0.262 38.03 0.177 2.886 0.676 0.105 0.022 6.137 0.227 0.262 38.03 0.177 2.886 0.676 0.105 0.023 5.977 0.							9.181		0.132
16.00 0.116 1.248 0.754 0.027 0.016 9.268 0.148 0.153 17.00 0.121 1.325 0.742 0.040 0.017 9.105 0.154 0.163 18.00 0.126 1.403 0.740 0.041 0.017 8.964 0.161 0.170 19.00 0.131 1.481 0.736 0.045 0.017 8.839 0.168 0.178 20.00 0.136 1.559 0.731 0.050 0.019 8.692 0.173 0.185 21.02 0.140 1.637 0.727 0.055 0.018 8.569 0.180 0.193 22.02 0.144 1.715 0.722 0.059 0.018 8.384 0.184 0.199 23.02 0.148 1.793 0.720 0.061 0.020 8.236 0.189 0.205 24.02 0.151 1.872 0.709 0.073 0.022 8.055 0.193 0.213									0.144
17.00 0.121 1.325 0.742 0.040 0.017 9.105 0.154 0.163 18.00 0.126 1.403 0.740 0.041 0.017 8.964 0.161 0.170 19.00 0.131 1.481 0.736 0.045 0.017 8.839 0.168 0.178 20.00 0.136 1.559 0.731 0.050 0.019 8.692 0.173 0.185 21.02 0.140 1.637 0.727 0.055 0.018 8.569 0.180 0.193 22.02 0.144 1.715 0.722 0.059 0.018 8.384 0.184 0.199 23.02 0.148 1.793 0.720 0.061 0.020 8.236 0.189 0.205 24.02 0.151 1.872 0.709 0.073 0.022 8.055 0.193 0.213 25.02 0.154 1.950 0.711 0.070 0.023 7.876 0.196 0.216 26.02 0.155 2.027 0.708 0.073 0.024 7.669 0.199 0.224 28.02 0.160 2.183 0.703 0.076 0.024 7.494 0.202 0.224 28.02 0.160 2.183 0.703 0.078 0.024 7.311 0.204 0.227 29.02 0.161 2.261 0.697 0.085 0.026 7.098 0.205 0.230 30.02 0.165 2.339 0.698 0.084 0.026 7.051 0.211 0.236 32.02 0.170 2.495 0.691 0.091 0.026 7.051 0.211 0.236 32.02 0.166 2.2339 0.698 0.084 0.026 7.051 0.211 0.236 32.02 0.165 2.339 0.698 0.084 0.026 7.051 0.211 0.236 32.02 0.170 2.495 0.691 0.091 0.023 6.932 0.214 0.243 32.02 0.170 2.495 0.691 0.091 0.023 6.932 0.214 0.243 32.02 0.170 2.495 0.691 0.091 0.023 6.518 0.221 0.236 33.02 0.171 2.574 0.687 0.094 0.094 0.024 6.650 0.219 0.249 34.02 0.173 2.652 0.684 0.097 0.023 6.518 0.221 0.255 35.03 0.174 2.730 0.679 0.103 0.024 6.850 0.219 0.249 34.02 0.175 2.808 0.676 0.105 0.024 6.351 0.221 0.255 35.03 0.177 2.866 0.676 0.105 0.024 6.335 0.227 0.262 38.03 0.177 2.866 0.676 0.105 0.024 6.331 0.227 0.262 38.03 0.177 2.868 0.676 0.105 0.024 5.983 0.227 0.262 38.03 0.177 2.868 0.676 0.105 0.024 5.983 0.227 0.262 38.03 0.177 2.868 0.676 0.105 0.024 5.983 0.227 0.262 38.03 0.177 2.868 0.676 0.105 0.024 5.983 0.227 0.262 38.03 0.177 2.868 0.676 0.105 0.024 5.983 0.227 0.262 38.03 0.177 2.864 0.671 0.110 0.023 5.907 0.230 0.268 40.03 0.180 3.120 0.668 0.113 0.023 5.774 0.231 0.270							9.268	0.148	0.153
18.00 0.126 1.403 0.740 0.041 0.017 8.964 0.161 0.170 19.00 0.131 1.481 0.736 0.045 0.017 8.839 0.168 0.178 20.00 0.136 1.559 0.731 0.050 0.019 8.692 0.173 0.185 21.02 0.140 1.637 0.727 0.055 0.018 8.569 0.180 0.193 22.02 0.144 1.715 0.722 0.059 0.018 8.384 0.184 0.199 23.02 0.148 1.793 0.720 0.061 0.020 8.236 0.189 0.205 24.02 0.151 1.872 0.709 0.073 0.022 8.055 0.193 0.213 25.02 0.154 1.950 0.711 0.070 0.023 7.876 0.196 0.216 26.02 0.155 2.027 0.708 0.073 0.024 7.669 0.199 0.220									0.163
19.00 0.131 1.481 0.736 0.045 0.017 8.839 0.168 0.178 20.00 0.136 1.559 0.731 0.050 0.019 8.692 0.173 0.185 21.02 0.140 1.637 0.727 0.055 0.018 8.569 0.180 0.193 22.02 0.144 1.715 0.722 0.059 0.018 8.384 0.184 0.199 23.02 0.148 1.793 0.720 0.061 0.020 8.236 0.189 0.205 24.02 0.151 1.872 0.709 0.073 0.022 8.055 0.193 0.213 25.02 0.154 1.950 0.711 0.070 0.023 7.876 0.196 0.216 26.02 0.155 2.027 0.708 0.073 0.024 7.669 0.199 0.220 27.02 0.158 2.105 0.706 0.076 0.024 7.494 0.202 0.224 28.02 0.160 2.183 0.703 0.078 0.024 7.311 0.204 0.227 29.02 0.161 2.261 0.697 0.085 0.026 7.098 0.205 0.230 30.02 0.165 2.339 0.698 0.084 0.026 7.051 0.211 0.236 31.02 0.168 2.418 0.691 0.091 0.021 6.932 0.214 0.243 32.02 0.170 2.495 0.691 0.091 0.025 6.794 0.217 0.245 33.02 0.171 2.574 0.687 0.094 0.091 0.022 6.335 0.224 0.249 34.02 0.173 2.652 0.684 0.097 0.023 6.932 0.214 0.245 35.03 0.174 2.730 0.679 0.105 0.024 6.351 0.221 0.255 35.03 0.175 2.808 0.676 0.105 0.024 6.335 0.224 0.259 37.03 0.177 2.886 0.676 0.105 0.024 6.335 0.224 0.225 38.03 0.177 2.886 0.676 0.105 0.024 5.983 0.227 0.266 39.03 0.177 2.886 0.676 0.105 0.024 5.983 0.227 0.266 39.03 0.180 3.042 0.671 0.110 0.023 5.997 0.230 0.268 40.03 0.180 3.042 0.6671 0.110 0.023 5.907 0.230 0.268 40.03 0.180 3.042 0.6671 0.110 0.023 5.907 0.230 0.227 0.266 39.03 0.177 2.886 0.676 0.105 0.024 5.983 0.227 0.266 39.03 0.177 2.886 0.676 0.105 0.024 5.983 0.227 0.266 39.03 0.180 3.042 0.671 0.110 0.023 5.907 0.230 0.268 40.03 0.180 3.042 0.671 0.110 0.023 5.907 0.230 0.268 40.03 0.180 3.042 0.671 0.110 0.023 5.907 0.230 0.268 40.03 0.180 3.042 0.671 0.110 0.023 5.907 0.230 0.268 40.03 0.180 3.042 0.6671 0.110 0.023 5.907 0.230 0.268 40.03 0.180 3.042 0.6671 0.110 0.023 5.907 0.231 0.227 0.266 39.03 0.180 3.042 0.668 0.113 0.023 5.774 0.231 0.270					0.041				0.170
20.00 0.136 1.559 0.731 0.050 0.019 8.692 0.173 0.185 21.02 0.140 1.637 0.727 0.055 0.018 8.569 0.180 0.193 22.02 0.144 1.715 0.722 0.059 0.018 8.384 0.184 0.199 23.02 0.148 1.793 0.720 0.061 0.020 8.236 0.189 0.205 24.02 0.151 1.872 0.709 0.073 0.022 8.055 0.193 0.213 25.02 0.154 1.950 0.711 0.070 0.023 7.876 0.196 0.216 26.02 0.155 2.027 0.708 0.073 0.024 7.669 0.199 0.220 27.02 0.158 2.105 0.706 0.076 0.024 7.494 0.202 0.224 28.02 0.160 2.183 0.703 0.078 0.024 7.311 0.204 0.231									0.178
21.02 0.140 1.637 0.727 0.055 0.018 8.569 0.180 0.193 22.02 0.144 1.715 0.722 0.059 0.018 8.384 0.184 0.199 23.02 0.148 1.793 0.720 0.061 0.020 8.236 0.189 0.205 24.02 0.151 1.872 0.709 0.073 0.022 8.055 0.193 0.213 25.02 0.154 1.950 0.711 0.070 0.023 7.876 0.196 0.216 26.02 0.155 2.027 0.708 0.073 0.024 7.669 0.199 0.220 27.02 0.158 2.105 0.706 0.076 0.024 7.494 0.202 0.224 28.02 0.160 2.183 0.703 0.078 0.024 7.311 0.204 0.227 29.02 0.161 2.261 0.697 0.085 0.026 7.098 0.205 0.230									0.185
22.02 0.144 1.715 0.722 0.059 0.018 8.384 0.184 0.199 23.02 0.148 1.793 0.720 0.061 0.020 8.236 0.189 0.205 24.02 0.151 1.872 0.709 0.073 0.022 8.055 0.193 0.213 25.02 0.154 1.950 0.711 0.070 0.023 7.876 0.196 0.216 26.02 0.155 2.027 0.708 0.073 0.024 7.669 0.199 0.220 27.02 0.158 2.105 0.706 0.076 0.024 7.494 0.202 0.224 28.02 0.160 2.183 0.703 0.078 0.024 7.311 0.204 0.227 29.02 0.161 2.261 0.697 0.085 0.026 7.098 0.205 0.230 30.02 0.168 2.418 0.691 0.091 0.023 6.932 0.214 0.243							8.569	0.180	0.193
23.02 0.148 1.793 0.720 0.061 0.020 8.236 0.189 0.205 24.02 0.151 1.872 0.709 0.073 0.022 8.055 0.193 0.213 25.02 0.154 1.950 0.711 0.070 0.023 7.876 0.196 0.216 26.02 0.155 2.027 0.708 0.073 0.024 7.669 0.199 0.220 27.02 0.158 2.105 0.706 0.076 0.024 7.494 0.202 0.224 28.02 0.160 2.183 0.703 0.078 0.024 7.311 0.204 0.227 29.02 0.161 2.261 0.697 0.085 0.026 7.098 0.205 0.230 30.02 0.165 2.339 0.698 0.084 0.026 7.051 0.211 0.236 31.02 0.168 2.418 0.691 0.091 0.023 6.932 0.214 0.243							8.384	0.184	0.199
24.02 0.151 1.872 0.709 0.073 0.022 8.055 0.193 0.213 25.02 0.154 1.950 0.711 0.070 0.023 7.876 0.196 0.216 26.02 0.155 2.027 0.708 0.073 0.024 7.669 0.199 0.220 27.02 0.158 2.105 0.706 0.076 0.024 7.494 0.202 0.224 28.02 0.160 2.183 0.703 0.078 0.024 7.311 0.204 0.227 29.02 0.161 2.261 0.697 0.085 0.026 7.098 0.205 0.230 30.02 0.165 2.339 0.698 0.084 0.026 7.051 0.211 0.236 31.02 0.168 2.418 0.691 0.091 0.023 6.932 0.214 0.243 32.02 0.170 2.495 0.691 0.091 0.025 6.794 0.217 0.245						0.020		0.189	0.205
25.02 0.154 1.950 0.711 0.070 0.023 7.876 0.196 0.216 26.02 0.155 2.027 0.708 0.073 0.024 7.669 0.199 0.220 27.02 0.158 2.105 0.706 0.076 0.024 7.494 0.202 0.224 28.02 0.160 2.183 0.703 0.078 0.024 7.311 0.204 0.227 29.02 0.161 2.261 0.697 0.085 0.026 7.098 0.205 0.230 30.02 0.165 2.339 0.698 0.084 0.026 7.051 0.211 0.236 31.02 0.168 2.418 0.691 0.091 0.023 6.932 0.214 0.243 32.02 0.170 2.495 0.691 0.091 0.025 6.794 0.217 0.245 33.02 0.171 2.574 0.687 0.094 0.024 6.650 0.219 0.249							8.055	0.193	0.213
26.02 0.155 2.027 0.708 0.073 0.024 7.669 0.199 0.220 27.02 0.158 2.105 0.706 0.076 0.024 7.494 0.202 0.224 28.02 0.160 2.183 0.703 0.078 0.024 7.311 0.204 0.227 29.02 0.161 2.261 0.697 0.085 0.026 7.098 0.205 0.230 30.02 0.165 2.339 0.698 0.084 0.026 7.051 0.211 0.236 31.02 0.168 2.418 0.691 0.091 0.023 6.932 0.214 0.243 32.02 0.170 2.495 0.691 0.091 0.025 6.794 0.217 0.245 33.02 0.171 2.574 0.687 0.094 0.024 6.650 0.219 0.249 34.02 0.173 2.652 0.684 0.097 0.023 6.518 0.221 0.253					0.070	0.023	7.876	0.196	0.216
27.02 0.158 2.105 0.706 0.076 0.024 7.494 0.202 0.224 28.02 0.160 2.183 0.703 0.078 0.024 7.311 0.204 0.227 29.02 0.161 2.261 0.697 0.085 0.026 7.098 0.205 0.230 30.02 0.165 2.339 0.698 0.084 0.026 7.051 0.211 0.236 31.02 0.168 2.418 0.691 0.091 0.023 6.932 0.214 0.243 32.02 0.170 2.495 0.691 0.091 0.025 6.794 0.217 0.245 33.02 0.171 2.574 0.687 0.094 0.024 6.650 0.219 0.249 34.02 0.173 2.652 0.684 0.097 0.023 6.518 0.221 0.253 35.03 0.174 2.730 0.679 0.103 0.024 6.381 0.223 0.257							7.669	0.199	0.220
28.02 0.160 2.183 0.703 0.078 0.024 7.311 0.204 0.227 29.02 0.161 2.261 0.697 0.085 0.026 7.098 0.205 0.230 30.02 0.165 2.339 0.698 0.084 0.026 7.051 0.211 0.236 31.02 0.168 2.418 0.691 0.091 0.023 6.932 0.214 0.243 32.02 0.170 2.495 0.691 0.091 0.025 6.794 0.217 0.245 33.02 0.171 2.574 0.687 0.094 0.024 6.650 0.219 0.249 34.02 0.173 2.652 0.684 0.097 0.023 6.518 0.221 0.253 35.03 0.174 2.730 0.679 0.103 0.024 6.381 0.223 0.257 36.03 0.175 2.808 0.676 0.105 0.024 6.235 0.224 0.259						0.024	7.494	0.202	0.224
29.02 0.161 2.261 0.697 0.085 0.026 7.098 0.205 0.230 30.02 0.165 2.339 0.698 0.084 0.026 7.051 0.211 0.236 31.02 0.168 2.418 0.691 0.091 0.023 6.932 0.214 0.243 32.02 0.170 2.495 0.691 0.091 0.025 6.794 0.217 0.245 33.02 0.171 2.574 0.687 0.094 0.024 6.650 0.219 0.249 34.02 0.173 2.652 0.684 0.097 0.023 6.518 0.221 0.253 35.03 0.174 2.730 0.679 0.103 0.024 6.381 0.223 0.257 36.03 0.175 2.808 0.676 0.105 0.024 6.235 0.224 0.259 37.03 0.177 2.886 0.676 0.105 0.022 6.137 0.227 0.262								0.204	0.227
30.02 0.165 2.339 0.698 0.084 0.026 7.051 0.211 0.236 31.02 0.168 2.418 0.691 0.091 0.023 6.932 0.214 0.243 32.02 0.170 2.495 0.691 0.091 0.025 6.794 0.217 0.245 33.02 0.171 2.574 0.687 0.094 0.024 6.650 0.219 0.249 34.02 0.173 2.652 0.684 0.097 0.023 6.518 0.221 0.253 35.03 0.174 2.730 0.679 0.103 0.024 6.381 0.223 0.257 36.03 0.175 2.808 0.676 0.105 0.024 6.235 0.224 0.259 37.03 0.177 2.886 0.676 0.105 0.022 6.137 0.227 0.262 38.03 0.177 2.964 0.674 0.107 0.024 5.983 0.227 0.263	29.02							0.205	0.230
31.02 0.168 2.418 0.691 0.091 0.023 6.932 0.214 0.243 32.02 0.170 2.495 0.691 0.091 0.025 6.794 0.217 0.245 33.02 0.171 2.574 0.687 0.094 0.024 6.650 0.219 0.249 34.02 0.173 2.652 0.684 0.097 0.023 6.518 0.221 0.253 35.03 0.174 2.730 0.679 0.103 0.024 6.381 0.223 0.257 36.03 0.175 2.808 0.676 0.105 0.024 6.235 0.224 0.259 37.03 0.177 2.886 0.676 0.105 0.022 6.137 0.227 0.262 38.03 0.177 2.964 0.674 0.107 0.024 5.983 0.227 0.263 39.03 0.180 3.042 0.671 0.110 0.023 5.907 0.230 0.268					0.084			0.211	0.236
32.02 0.170 2.495 0.691 0.091 0.025 6.794 0.217 0.245 33.02 0.171 2.574 0.687 0.094 0.024 6.650 0.219 0.249 34.02 0.173 2.652 0.684 0.097 0.023 6.518 0.221 0.253 35.03 0.174 2.730 0.679 0.103 0.024 6.381 0.223 0.257 36.03 0.175 2.808 0.676 0.105 0.024 6.235 0.224 0.259 37.03 0.177 2.886 0.676 0.105 0.022 6.137 0.227 0.262 38.03 0.177 2.964 0.674 0.107 0.024 5.983 0.227 0.263 39.03 0.180 3.042 0.671 0.110 0.023 5.907 0.230 0.268 40.03 0.180 3.120 0.668 0.113 0.023 5.774 0.231 0.270									0.243
33.02 0.171 2.574 0.687 0.094 0.024 6.650 0.219 0.249 34.02 0.173 2.652 0.684 0.097 0.023 6.518 0.221 0.253 35.03 0.174 2.730 0.679 0.103 0.024 6.381 0.223 0.257 36.03 0.175 2.808 0.676 0.105 0.024 6.235 0.224 0.259 37.03 0.177 2.886 0.676 0.105 0.022 6.137 0.227 0.262 38.03 0.177 2.964 0.674 0.107 0.024 5.983 0.227 0.263 39.03 0.180 3.042 0.671 0.110 0.023 5.907 0.230 0.268 40.03 0.180 3.120 0.668 0.113 0.023 5.774 0.231 0.270					0.091		6.794	0.217	0.245
34.02 0.173 2.652 0.684 0.097 0.023 6.518 0.221 0.253 35.03 0.174 2.730 0.679 0.103 0.024 6.381 0.223 0.257 36.03 0.175 2.808 0.676 0.105 0.024 6.235 0.224 0.259 37.03 0.177 2.886 0.676 0.105 0.022 6.137 0.227 0.262 38.03 0.177 2.964 0.674 0.107 0.024 5.983 0.227 0.263 39.03 0.180 3.042 0.671 0.110 0.023 5.907 0.230 0.268 40.03 0.180 3.120 0.668 0.113 0.023 5.774 0.231 0.270								0.219	0.249
35.03 0.174 2.730 0.679 0.103 0.024 6.381 0.223 0.257 36.03 0.175 2.808 0.676 0.105 0.024 6.235 0.224 0.259 37.03 0.177 2.886 0.676 0.105 0.022 6.137 0.227 0.262 38.03 0.177 2.964 0.674 0.107 0.024 5.983 0.227 0.263 39.03 0.180 3.042 0.671 0.110 0.023 5.907 0.230 0.268 40.03 0.180 3.120 0.668 0.113 0.023 5.774 0.231 0.270					0.097	0.023		0.221	0.253
36.03 0.175 2.808 0.676 0.105 0.024 6.235 0.224 0.259 37.03 0.177 2.886 0.676 0.105 0.022 6.137 0.227 0.262 38.03 0.177 2.964 0.674 0.107 0.024 5.983 0.227 0.263 39.03 0.180 3.042 0.671 0.110 0.023 5.907 0.230 0.268 40.03 0.180 3.120 0.668 0.113 0.023 5.774 0.231 0.270								0.223	0.257
37.03 0.177 2.886 0.676 0.105 0.022 6.137 0.227 0.262 38.03 0.177 2.964 0.674 0.107 0.024 5.983 0.227 0.263 39.03 0.180 3.042 0.671 0.110 0.023 5.907 0.230 0.268 40.03 0.180 3.120 0.668 0.113 0.023 5.774 0.231 0.270						0.024	6.235		0.259
38.03 0.177 2.964 0.674 0.107 0.024 5.983 0.227 0.263 39.03 0.180 3.042 0.671 0.110 0.023 5.907 0.230 0.268 40.03 0.180 3.120 0.668 0.113 0.023 5.774 0.231 0.270									
39.03 0.180 3.042 0.671 0.110 0.023 5.907 0.230 0.268 40.03 0.180 3.120 0.668 0.113 0.023 5.774 0.231 0.270									
40.03 0.180 3.120 0.668 0.113 0.023 5.774 0.231 0.270									
10.00									
	41.03	0.182	3.198	0.666	0.116	0.023		0.232	0.273

Elapsed Time	Shear	Shear	Effective	Pore	Axial	Shear	Normalized	Obliquity
(minutes)	Stress	Strain	Stress	Pressure	Strain	Modulus	Shear	
	(kg/cm²)	(%)	(kg/cm²)	(kg/cm²)	(%)	(kg/cm2)	Stress	
42.03	0.183	3,276	0.664	0.117	0.023	5.587	0.234	0.276
43.03	0.184	3.354	0.662	0.119	0.024	5.482	0.235	0.278
44.03	0.185	3.432	0.658	0.124	0.023	5.391	0,237	0.281
45.03	0.187	3.510	0.656	0.125	0.023	5.318	0.239	0.284
46.03	0.188	3.588	0,655	0.127	0.023	5.232	0.240	0.287
47.03	0.189	3.666	0.652	0.130	0.025	5.149	0.242	0.290
48.03	0.189	3.744	0.651	0.130	0.024	5.052	0.242	0.290
49.03	0.191	3.822	0.651	0.131	0.023	4,987	0.244	0.293
50.03	0.191	3.900	0.647	0.135	0.024	4.906	0.245	0.296
51.03	0.193	3.977	0.645	0.137	0.023	4.841	0.246	0.299
54.03	0.197	4.211	0.640	0.142	0.023	4.681	0.252	0.308
57.03	0.200	4.445	0.634	0.147	0.025	4.509	0.257	0.316
60.03	0.202	4.679	0.629	0.152	0.025	4.324	0.259	0.321
63.03	0.205	4.913	0.625	0.156	0.024	4.167	0.262	0.327
66.03	0.208	5,147	0.620	0.162	0.026	4.041	0.266	0.336
69.05	0.210	5.381	0.618	0.163	0.028	3.900	0.269	0.339
72.05	0.212	5.615	0.613	0.168	0.029	3.783	0.272	0.346
75.05	0.216	5.849	0.609	0.172	0.028	3.687	0.276	0.354
78.05	0.218	6.083	0.605	0.177	0.029	3.585	0.279	0.361
81.05	0,220 0,222	6.317	0.603	0.178	0.032 0.033	3.478	0.281 0.284	0.364
84.05 87.05	0.223	6.551 6.785	0.600 0.598	0.182 0.184	0.033	3.383 3.290	0.286	0.369 0.373
90.05	0.224	7.019	0.598	0.184	0.034	3.196	0.287	0.373
93.05	0.224	7.019	0.592	0.190	0.034	3,123	0.290	0.379
96.07	0.228	7.486	0.589	0.193	0.032	3.042	0.291	0.387
99.07	0.228	7.720	0.586	0.195	0.033	2.956	0.292	0.389
102.07	0.229	7.954	0.584	0.198	0.032	2.876	0.293	0.392
105.07	0.229	8.188	0.581	0.200	0.032	2.797	0.293	0.394
108.07	0.229	8.422	0.578	0.203	0.033	2.718	0.293	0.396
111.07	0.229	8.656	0.576	0.205	0.033	2.651	0.294	0.398
114.07	0.228	8.890	0.572	0.209	0.033	2.564	0.292	0.398
117.07	0.228	9.124	0.571	0.211	0.035	2.495	0.291	0.399
120.07	0.227	9.358	0.567	0.215	0.037	2.426	0.291	0.401
123.07	0.226	9.592	0.565	0.217	0.037	2.353	0.289	0.400
126.07	0.225	9.826	0.561	0.220	0.035	2.293	0.288	0.402
129.07	0.224	10.060	0.556	0.225	0.034	2.230	0.287	0.403
132.08	0.224	10.294	0.555	0.227	0.034	2.172	0.286	0.403
135.08	0.222	10.528	0.551	0.231	0.034	2.112	0.285	0.404
138.08	0.222	10.761	0.547	0.235	0.033	2.065	0.284	0.407
141.08	0.221	10.995	0.547	0.234	0.034	2.011	0.283	0.404
144.08	0.220	11.229	0.540	0.241	0.032	1.959	0.281	0.407
147.08	0.220	11.463	0.539	0.242	0.035	1.917	0.281	0.408
150.08	0.219	11,697	0.534	0.248	0.033	1.871	0.280	0.410
153.08	0.218	11.931	0.533	0.249	0.033	1.827	0.279	0.409
156.08	0.216	12.165	0.529	0.253	0.034	1.778	0.277	0.409
159,08	0.212	12.399	0.525	0.257	0.035	1.713	0.272	0.405
162.08	0.213	12.633	0.521	0.260	0.035	1.689	0.273	0.409
165.10	0.215	12.867	0.519	0.262	0.034	1.669	0.275	0.414
168.12	0.216	13.101	0.517	0.265	0.032	1.648	0.276	0.418
171.12	0.217	13.334	0.517	0.264	0.034	1.626	0.277	0.419
174.13	0.217	13.569	0.514	0.268	0.033	1.600	0.278	0.423
177.13	0.218	13.802	0.510	0.271	0.034	1.582	0.279	0.428
180.13	0.217	14.036	0.510	0.272	0.034	1.550	0.278	0.427
183.13	0.217	14.271	0.508	0.273	0.035	1,522	0.278	0.427
186.13	0.218	14.504	0.505	0.276	0.034	1.500	0.278	0.431
189.13	0.218	14.738	0.505	0.277	0.035	1.478	0.279	0.432
192.13	0.217	14.972	0.502	0.279	0.034	1.450	0.278	0.432
195.13	0.219	15.206	0.500	0.282	0.033	1.438	0.280	0.437
198.15	0,218	15.440	0.495	0.286	0.034	1.414	0.279	0.441
201,15	0.218	15.674	0.494	0.287	0.037	1.392	0.279	0.442
207.15	0.218	16.142	0.490	0.291	0.037	1,350	0.279	0.445
213.15	0.219	16.609	0.483	0.298	0.037	1.318	0.280	0.453
219.15	0.218	17.077	0.481	0.300	0.035	1.279	0.280	0.454
225.15	0.218	17.544	0.484	0.298	0.036	1.243	0.279	0.451
231.15	0.219	18.012	0.476	0.306	0.038	1.213	0.280	0.459

Elapsed Time (minutes)	Shear Stress	Shear Strain	Effective Stress	Pore Pressure	Axial Strain	Shear Modulus	Normalized Shear	Obliquity
(minutes)	(kg/cm ²)	(%)	(kg/cm²)	(kg/cm²)	(%)	(kg/cm2)	Stress	
237.15	0.217	18.480	0.470	0.311	0.038	1.172	0.277	0.461
243.15	0.215	18.948	0.465	0.317	0.036	1.137	0.276	0.464
249.15	0.213	19.415	0.462	0.319	0.036	1.099	0.273	0.462
255.15	0.212	19.883	0.456	0.325	0.036	1.068	0.272	0.465
261.15	0.212	20.350	0.454	0.328	0.035	1.040	0.271	0.467
267.15	0.211	20.818	0.455	0.327	0.036	1.011	0.269	0.463
273.15	0.209	21.286	0.445	0.336	0.034	0.983	0.268	0.470
279.15	0.208	21.754	0.443	0.339	0.036	0.957	0.266	0.470
284.73	0.209	22 188	0.437	0.344	0.036	0.940	0.267	0.477





File Number

12-80-3741

Project Name Sample Name

B-02 14-16

Sample Area Height (preshear) Normal Load

Displacement Rate 0.00019

Normal Stress

34.78 1.63 9.0

0.26

cm² cm Kg Kg/cm² in/min

Calibration Factors

 Horizontal Load, kgs.:
 -115721.6

 Vertical Load, kgs:
 -67588.6

 Vertical dcdt, cm:
 -219.453

 Excitation volts:
 10.000

			Normal	Shear induced				
Elapsed Time	Shear	Shear	Effective	Pore	Axial	Shear	Normalized	Obliquity
(minutes)	Stress	Strain	Stress	Pressure	Strain	Modulus	Shear	
	(kg/cm²)	(%)	(kg/cm ²)	(kg/cm²)	(%)	(kg/cm2)	Stress	
0.00	-0.001	0.000	0.258	0.000	0.000	0.000	-0.0038	-0.004
1.00	0.000	0.077	0.257	0.001	-0.001	0.026	0.000	0.000
2.00		0.156	0.259	0.000	-0.002	#VALUE!	#VALUE!	#VALUE!
3.00		0.234	0.260	-0.001	-0.004	#VALUE!	#VALUE!	#VALUE!
4.00		0.312	0.257	0.002	-0.006	#VALUE!	#VALUE!	#VALUE!
5.00		0.390	0.259	-0,001	-0.005	#VALUE!	#VALUE!	#VALUE!
6.00		0.468	0.270	-0.012	-0.007	#VALUE!	#VALUE!	#VALUE!
7.00		0.546	0.255	0.003	-0.008	#VALUE!	#VALUE!	#VALUE!
8.00		0.624	0.260	-0.001	-0.009	#VALUE!	#VALUE!	#VALUE!
9.00		0.702	0.259	-0.001	-0.008	#VALUE!	#VALUE!	#VALUE!
10.00	0.000	0.780	0.260	-0.002	-0.009	0.061	0.002	0.002
11.02	0.000	0.858	0.259	-0.001	-0.010	0.025	0.001	0.001
12.02	0.009	0.936	0.259	-0.001	-0.011	0.947	0.034	0.034
13.02	0.013	1.014	0.259	-0.001	-0.012	1.294	0.051	0.051
14.02	0.017	1.092	0.258	0.000	-0.012	1.562	0.066	0.066
15.02	0.022	1.170	0.260	-0.002	-0.009	1.896	0.086	0.085
16.02	0.030	1.248	0.261	-0.003	-0.008	2.408	0.116	0.115
17.02	0.039	1.326	0.267	-0.009	-0.004	2.918	0.150	0.145
18.02	0.048	1.404	0.265	-0.006	-0.003	3.405	0.185	0.181
19.02	0.056	1.482	0.267	-0.009	0.001	3.784	0.217	0.210
20.02	0.063	1.561	0.270	-0.012	0.003	4.057	0.245	0.234
21.02	0.070	1.639	0.273	-0.014	0.003	4.266	0.271	0.256
22.02	0.076	1.717	0.277	-0.018	0.003	4.404	0.293	0.273
23.03	0.082	1.794	0.280	-0.022	0.002	4.561	0.317	0.292
24.03	0.086	1.873	0.283	-0.025	-0.001	4.591	0.333	0.304
25.03	0.091	1.951	0.286	-0.028	-0.001	4.658	0.352	0.318
26.03	0.095	2.028	0.289	-0.031	-0.003	4.676	0.367	0.328
27.03	0.098	2.107	0.293	-0.034	-0.005	4.638	0.378	0.334
28.03	0.101	2.185	0.293	-0.035	-0.007	4.638	0.392	0.346
29.03	0.104	2.263	0.294	-0.036	-0.008	4.606	0.404	0.354
30.03	0.108	2.341	0.297	-0.039	-0.011	4.596	0.416	0.362
31.03	0.110	2.419	0.305	-0.046	-0.011	4.528	0.424	0.360
32.03	0.112	2.497	0.304	-0.045	-0.012	4.474	0.432	0.368
33.03	0.115	2.575	0.304	-0.046	-0.014	4.448	0.443	0.377
34.03	0.116	2.653	0.309	-0.050	-0.014	4.379	0.450	0.376
35.05	0.119	2.731	0.308	-0.049	-0.016	4.350	0.460	0.386
36.05	0.120	2.809	0.312	-0.053	-0.016	4.277	0.465	0.386
37.05	0.122	2.887	0.313	-0.055	-0.016	4.234	0.473	0.390
38.05	0.124	2.965	0.325	-0.067	-0.018	4,194	0.482	0.383
39.05	0.126	3.043	0.315	-0.057	-0.020	4.137	0.487	0.399
40.05	0.127	3.122	0.315	-0.057	-0.021	4.070	0.492	0.403
41.05	0.129	3.200	0.319	-0.060	-0.020	4.023	0.498	0.404
		-2			200			

	sed Time	Shear Stress	Shear Strain	Effective Stress	Pore	Axial Strain	Shear Modulus	Normalized Shear	Obliquity
(m	ninutes)				Pressure				
	40.05	(kg/cm²)	(%)	(kg/cm²)	(kg/cm²)	(%)	(kg/cm2)	Stress	0.405
	42.05	0.131	3.277	0.322	-0.064	-0.019	3.984	0.506	
	43.05	0.132	3,356	0.324	-0.065	-0.019	3.931	0.511	0.408
	44.07	0.134	3.434	0.324	-0.066	-0.021	3.894	0.518	0.412
	45.07	0.135	3.512	0.324	-0.065	-0.021	3.846	0.523	0.417
	46.07	0.136	3.590	0.326	-0.067	-0.023	3.798	0.528	0.419
	47.07	0.138	3.668	0.329	-0.070	-0.021	3.760	0,534	0.420
	48.07	0.139	3,746	0.330	-0.072	-0.020	3.721	0.540	0.422
	49.07	0.141	3.824	0.331	-0.073	-0.017	3.700	0.548	0.427
	50.07	0.143	3.902	0.331	-0.073	-0.012	3.663	0.553	0.432
	51.07	0.145	3.980	0.333	-0.074	-0.009	3.639	0.561	0.435
	54.07	0.149	4.214	0.339	-0.080	-0.004	3.533	0.576	0.440
	57.07	0.152	4.448	0,341	-0.083	-0.007	3.428	0.590	0.447
	60.07	0.155	4.682	0.344	-0.086	-0.012	3.301	0.598	0.449
	63.07	0.157	4.916	0.348	-0.090	-0.015	3.186	0.606	0.450
	66.08	0.159	5.150	0.349	-0.091	-0.018	3.084	0.615	0.455
	69.08	0.160	5,384	0.350	-0.092	-0.019	2.980	0.621	0.458
	72.08	0.163	5,617	0.352	-0.094	-0.021	2.903	0.631	0.463
	75.08	0.165	5.851	0.355	-0.096	-0.022	2.814	0.637	0.464
	78.08	0,167	6,085	0.357	-0.098	-0.022	2.742	0.646	0.468
	81.08	0.168	6.319	0.356	-0.098	-0.024	2.657	0.650	0.471
	84.08	0.170	6.553	0.359	-0.101	-0.020	2.602	0.660	0.475
	87.08	0.174	6.787	0.361	-0.102	-0.008	2.558	0.672	0.482
	90.08	0.176	7.021	0.363	-0.104	-0.001	2.500	0.679	0.484
	93.10	0.177	7.255	0.364	-0.106	-0.003	2.442	0.686	0.486
	96.10	0.177	7.489	0.365	-0.107	-0.008	2.368	0.687	0.486
	99.10	0.178	7.723	0.366	-0.108	-0.012	2.310	0.691	0.487
	102.10	0.179	7.957	0.366	-0.108	-0.016	2.247	0.692	0.488
	105.10	0.179	8.191	0.366	-0.108	-0.017	2.189	0.694	0.489
3*	108.10	0.180	8.425	0.365	-0.106	-0.018	2,135	0.696	0.493
1	111:10	0.180	8.659	0.369	-0.111	-0.021	2.074	0.695	0.487
1	114.10	0.180	8.893	0.369	-0.110	-0.022	2.020	0.696	0.488
1	117.10	0.180	9.127	0.367	-0.109	-0.018	1.968	0.695	0.490
1	120.10	0.179	9.361	0.369	-0.111	-0.006	1.911	0.693	0.485
1	123.10	0.179	9.594	0.367	-0.109	-0.002	1.870	0,695	0.489
1	126.12	0.179	9.829	0.368	-0.110	-0.005	1.823	0.694	0.487
1	129.12	0.179	10.062	0.368	-0.109	-0.009	1.776	0.692	0.486
	132.12	0.178	10.297	0.368	-0.109	-0.013	1.733	0.691	0.485
	135.12	0.178	10.530	0.366	-0.108	-0.015	1.690	0.689	0.486
	138.12	0.177	10.764	0.364	-0.105	-0.018	1.647	0.687	0.488
	141,12	0.177	10.998	0.365	-0.106	-0.019	1.613	0.687	0.486
	144.12	0.177	11.232	0.363	-0.105	-0.018	1.579	0.687	0.488
	147.12	0.177	11,466	0.360	-0.101	-0.019	1.545	0.686	0.492
1	150.12	0.165	11.700	0.352	-0.094	-0.018	1.408	0.638	0.467
1	153.12	0.165	11.934	0.351	-0.092	-0.019	1.385	0.640	0.471
	156.12	0.168	12.168	0.349	-0.091	-0.020	1.378	0.649	0.480
	159.12	0.164	12,402	0.346	-0.088	-0.016	1.324	0.636	0.475
	162.13	0.169	12.636	0.347	-0.089	-0.004	1.338	0.655	0.487
	165.13	0,180	12.870	0.352	-0.094	-0.001	1,401	0.698	0.512
	168.13	0.184	13.104	0.354	-0.096	-0.005	1.407	0.714	0.521
1	171.13	0.184	13.338	0.356	-0.098	-0.008	1.383	0.714	0.518
	174.13	0.185	13.571	0.356	-0.098	-0.011	1.365	0.717	0.520
1	177.13	0.185	13.805	0.356	-0.097	-0.013	1.337	0.714	0.519
1	180.13	0.184	14.039	0.355	-0.096	-0.016	1.309	0.711	0.518
	183.15	0.184	14.273	0.356	-0.098	-0.014	1.291	0.713	0.518
1	186.17	0.184	14.507	0.354	-0.096	-0.017	1.266	0.711	0.519
	189.17	0.184	14.741	0.353	-0.095	-0.019	1.246	0.711	0.520
	192.18	0.183	14.975	0.354	-0.096	-0.018	1.224	0.710	0.518
	195.18	0.183	15.209	0.355	-0.097	-0.020	1.203	0.708	0.516
1	198.18	0.183	15.443	0.352	-0.094	-0.021	1.183	0.708	0.519
2	201.18	0.182	15.677	0.352	-0.094	-0.021	1.163	0.706	0.518
2	207.18	0.181	16.145	0.351	-0.093	-0.020	1.123	0.702	0.516
2	213,18	0.181	16.612	0.351	-0.093	-0.021	1.088	0.699	0.514
	219.18	0.183	17.080	0.350	-0.092	-0.022	1.069	0.707	0.522
2	225.18	0.183	17.548	0.349	-0.091	-0.022	1.044	0.709	0.525
2	231.18	0.185	18.015	0.349	-0.090	-0.011	1.025	0.715	0.530

Elapsed Time	Shear	Shear	Effective	Pore	Axial	Shear	Normalized	Obliquity
(minutes)	Stress	Strain	Stress	Pressure	Strain	Modulus	Shear	
	(kg/cm²)	(%)	(kg/cm²)	(kg/cm²)	(%)	(kg/cm2)	Stress	
237.18	0.188	18.483	0.347	-0.089	-0.004	1.015	0.726	0.540
243.18	0.187	18.951	0.349	-0.090	-0.011	0.987	0.724	0.536
249.18	0.187	19.418	0.345	-0.087	-0.017	0.965	0.725	0.543
255.18	0.187	19.886	0.346	-0.087	-0.019	0.942	0.725	0.542
261.20	0.188	20.353	0.344	-0.086	-0.021	0.922	0.727	0.545
267.20	0.188	20.821	0.342	-0.083	-0.024	0.903	0.728	0.550
273.20	0.189	21.289	0.341	-0.083	-0.008	0.890	0.733	0.555
279.20	0.190	21.757	0.340	-0.082	-0.004	0.873	0.735	0.558
285.20	0.189	22.224	0.336	-0.078	-0.017	0.852	0.733	0.564
291.20	0.189	22.692	0.333	-0.075	-0.015	0.834	0.733	0.568
297.20	0.189	23.160	0.332	-0.074	0.002	0.817	0.733	0.570
303.20	0.189	23.627	0.331	-0.073	0.002	0.800	0.732	0.571
309.20	0.187	24.096	0.329	-0.071	-0.013	0.778	0.725	0.569
315.20	0.189	24.563	0.328	-0.069	-0.004	0.770	0.732	0.577
321.20	0.191	25.031	0.327	-0.069	0.010	0.764	0.740	0.584

APPENDIX F. SETTLING AND SLURRY CONSOLIDATION TEST RESULTS

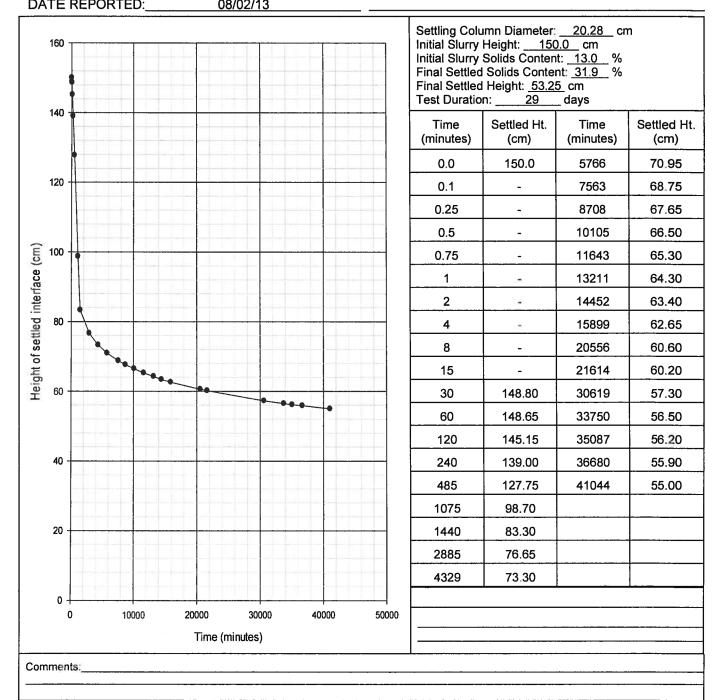
This Appendix contains the following:

- Settling Column Test Results
- Slurry Consolidation Test Results



ARDAMAN & ASSOCIATES, INC. GEOTECHNICAL TESTING LABORATORY SETTLING TEST REPORT

CLIENT: CPRA		INCOMING SAM	MPLE NO.:	Туре	1	
PROJECT: Oyster Bayou		BORING:	Borrow	SAMPLE: (Composite	
FILE NO.: 12-80-3741		DEPTH:	0 –	10 ft.] ft; □ m
-		LABORATORY	IDENTIFIC	CATION:	803741/1	_
DATE SAMPLE RECEIVED:		SAMPLE DESC	RIPTION:	Gray clay v	vith trace s	hell
DATE TEST SET-UP:	06/17/13					
DATE DEDODTED:	00/00/40	· ·			, , ,	

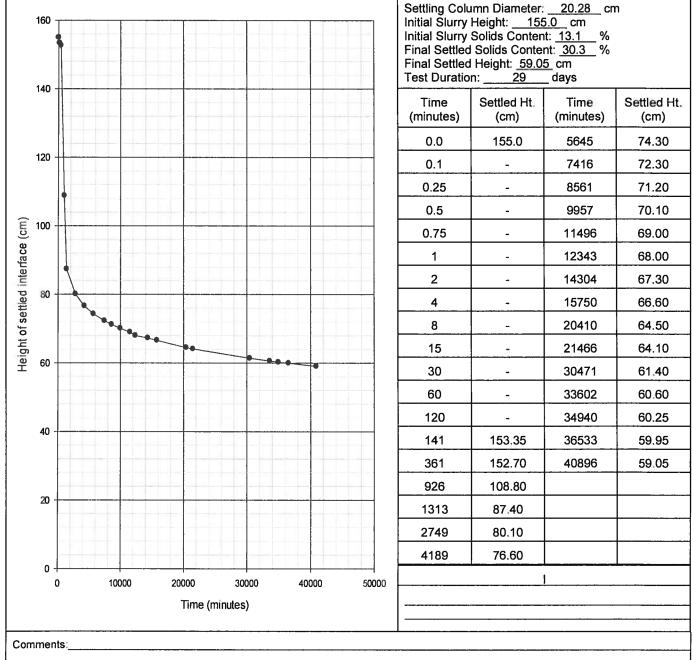


The test data and all associated project information presented hereon shall be held in confidence and disclosed to other parties only with the authorization of the Client. Physical and electronic records of each project are kept for a minimum of 7 years. Test samples are kept in storage for at least 10 working days after mailing of the test report, prior to being discarded, unless a longer storage period is requested in writing and accepted by Ardaman & Associates, Inc.



ARDAMAN & ASSOCIATES, INC. GEOTECHNICAL TESTING LABORATORY SETTLING TEST REPORT

CLIENT: CPRA	INCOMING SAMPLE NO.: Type 2
PROJECT: Oyster Bayou	BORING: Borrow SAMPLE: Composite
FILE NO.: 12-80-3741	DEPTH: <u>0 − 10 ft.</u> ☐ ft; ☐ m
DATE SAMPLE RECEIVED:	LABORATORY IDENTIFICATION: 803741/2 SAMPLE DESCRIPTION: Gray clay with trace shell
DATE TEST SET-UP: 06/17/13	
DATE REPORTED: 08/02/13	
	Settling Column Diameter:20.28 _ cm



The test data and all associated project information presented hereon shall be held in confidence and disclosed to other parties only with the authorization of the Client. Physical and electronic records of each project are kept for a minimum of 7 years. Test samples are kept in storage for at least 10 working days after mailing of the test report, prior to being discarded, unless a longer storage period is requested in writing and accepted by Ardaman & Associates, Inc.



ARDAMAN & ASSOCIATES, INC. GEOTECHNICAL TESTING LABORATORY SETTLING TEST REPORT

PROJ		CPRA Oyster Bay 12-80-374				BORIN DEPT	MING SAMPI NG: Bo H: RATORY IDE	rrow SAMI 0 - 10 ft.	PLE: Compo	🗆 ft; 🗆 m
DATE	TEST	LE RECE SET-UP:_ RTED:	IVED:	 6/17/13 8/02/13			LE DESCRIF			
180							Initial Slurry Initial Slurry Final Settled Final Settled	umn Diameter: Height: 165 Solids Content Solids Content Height: 75,7 n: 29	5.0 cm ht: 14.0 % nt: 27.6 % _ cm	n
							Time (minutes)	Settled Ht. (cm)	Time (minutes)	Settled Ht. (cm)
140							0.0	165.0	5277	98.25
							0.1	-	7047	95.80
							0.25	-	8192	94.55
120							0.5	-	9587	93.20
cm)							0.75	-	11127	91.85
) ace							1	-	11974	90.70
100	1						2	-	13936	89.85
ed ir			•				4		15381	88.95
Height of settled interface (cm)				-			8	-	20040	86.40
ht of							15	5 7 8 L	21097	85.90
Heig						+	30	-	30102	82.30
60							60	ATT (1	33233	81.20
							120	340	34571	80.70
							240	-	36163	80.20
40							480	-	40527	78.90
							555	152.40		
20							960	118.00		
20							2400	105.10		
							3856	100.90		
0	0	10000	20000	20000	40000	50000				<u>-</u>
	U	10000	20000 Time (n	30000 ninutes)	40000	50000				
Comme	nts:		`	•						
							· · · · · · · · · · · · · · · · · · ·			

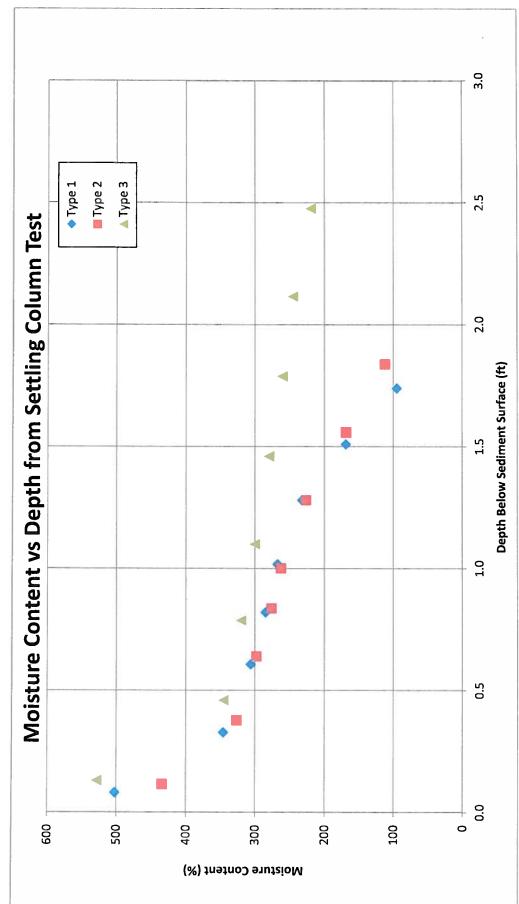
The test data and all associated project information presented hereon shall be held in confidence and disclosed to other parties only with the authorization of the Client. Physical and electronic records of each project are kept for a minimum of 7 years. Test samples are kept in storage for at least 10 working days after mailing of the test report, prior to being discarded, unless a longer storage period is requested in writing and accepted by Ardaman & Associates, Inc.

Checked By: War

Settling test	calculations		
Requested S(%)	13.5	13.5	3
Diameter of cylinder (cm)	20.28	20.36	18.97
Initial height (cm)	150	155	165
Final height (cm)	53.25	59.05	75.7
Total WDS (g)	6876	7200	7163
ιο,			
Specific gravity	2.72	2.72	2.72
Outputs:			
Ca.pa.o.			
Volume initial (cm3)	48452.60	50463.47	46634.62
Volume final (cm3)	17200.67	19224.95	21395.40
Volume solids (cm3)	2527.94	2647.06	2633.46
Volume water (cm3)i	45924.65	47816.41	44001.17
Volume water (cm3)f	14672.73	16577.90	18761. 9 4
Water content i	6.679	6.641	6.143
Solids (%)i	13.02	13.09	14.00
Concentration (g/L) i	141.9	142.7	153.6
Water content f	2.134	2.302	2.619
Solids (%)f	31.91	30.28	27.63
Concentration (g/L)f	399.8	374.5	334.8
9.000	000.0	074.0	004.0
Final water content:			
wws+tare, g	281.37	270.72	373.9
wds+tare, g	105.22	98.17	100
tare, g	21.74	21.72	0
Final water content (%)	211	226	274

TYPE 1 TYPE 2 TYPE 3





Client: CPRA Project: Oyster Bayou

AAI Project No. 12-80-3741

ARDAMAN & ASSOCIATES, INC. GEOTECHNICAL TESTING LABORATORY SLURRY CONSOLIDATION TEST REPORT

FILE NO	,,, 	ster Bayou				COMING ORING: _	SAMPLE TYPE		SA	MPLE: _	Borro)W
	.: <u>12</u> -	80-3741			DI	EPTH: _	Comp	osite (0-			ft; ⊏m	
		_			L/	AB IDENT	FICATIO	N NO.:		41 / T YP	E1	
		ECEIVED:	5/24/13		SA	MPLE DE	SCRIPTI	ON.:	Clay w	ith sand		
	AMPLE SI EPORTEI	= 1-UF										
									Te	est Method	s & Proced	dures
									⊏ C _ν [S Trimming N	nod A nod B tation Meth Log Time] Sq. Root Ti Method ing shoe	od me]	97 (cm)
6	5.0									Test C	onditions	
5	5.5					-						_
5	5.0											re Content ated
										cimen Tes dated at σ		1_ (tsf)
4	1.5	•							Inu	ndation Flu tap wat	iid: er	
4	1.0									other .		
OTFA		•								Specime	n Condition	ns
VOID RATIO	3.5		•						Paramete	er Ini	tial	Final
	3.0								D (cm)	10	.09 [.]	10.09
				•					H (cm)	9.	213	3.360
2	2.5								W _c (%)	24	46.6	67.8
2	2.0								γ _d (pcf)	2	1.0	57.6
									е	7.0	86	1.950
1	.5							\Box	S (%)	95	,	95
1	.0								G _s : 2.72	₽ /	Assumed	
	0.001	0.005	0.01	0.	05 0.1	1	0.5	1	O ₈ . 2.72	г	Measured	
		VERTIC	AL FFFFC	TIVE STRES	S.OT (ton	e/ft ²)				Index F	Properties	
			,		o, o vc (10))	3/11/				1		
									LL			
									PL			
									PI			
Particle-Siz		U.S. Standard		Gravel		Coarse Sand	Med Sa				ine and	
	422 1140-Method	Sieve Size	3/4"	3/8"	No. 4	No. 10	No. 20	No. 40	No. 60	No. 100	No. 140	No. 200
Dry Mass(g):	248.10	Soil Passing (%, dry mass basis)	100	100	100	100	99.9	99.9	98.9	94.4	88.7	83.2

The test data and all associated project information presented hereon shall be held in confidence and disclosed to other parties only with the authorization of the Client. Physical and electronic records of each project are kept for a minimum of 7 years. Test samples are kept in storage for at least 10 working days after mailing of the test report, prior to being discarded, unless a longer storage period is requested in writing and accepted by Ardaman & Associates, Inc.

Where: H=Specimen height; D = Specimen diameter; w_c = Water content (ASTM D2216); γ_d = Dry density; e = Void ratio; S = Saturation; G_s = Specific gravity; e_s = Coefficient of consolidation; and e_s = Secondary compression index.

